

Point-Mass Dynamics and Aerodynamic/Thrust Forces

Robert Stengel, Aircraft Flight Dynamics,
MAE 331, 2018

Learning Objectives

- Properties of atmosphere
- Frames of reference
- Velocity and momentum
- Newton's laws of motion
- Airplane axes
- Lift and drag
- Simplified equations for longitudinal motion
- Powerplants and thrust

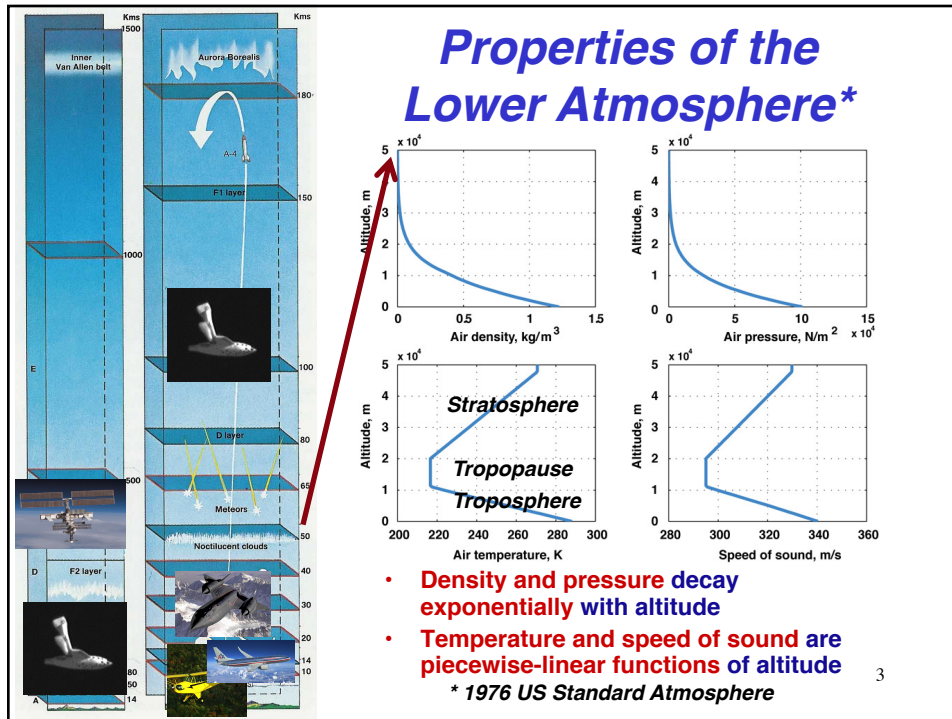
Reading:
Flight Dynamics
Introduction, 1-27
The Earth's Atmosphere, 29-34
Kinematic Equations, 38-53
Forces and Moments, 59-65
Introduction to Thrust, 103-107

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<http://www.princeton.edu/~stengel/MAE331.html>
<http://www.princeton.edu/~stengel/FlightDynamics.html>

1

The Atmosphere

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Air Density, Dynamic Pressure, and Mach Number

$\rho = \text{Air density}$, function of height

$$= \rho_{sealevel} e^{-\beta h} = \rho_{sealevel} e^{\beta z}$$

$$\rho_{sealevel} = 1.225 \text{ kg/m}^3; \quad \beta = 1/9,042 \text{ m}$$

$$V_{air} = \left[v_x^2 + v_y^2 + v_z^2 \right]_{air}^{1/2} = \left[\mathbf{v}^T \mathbf{v} \right]_{air}^{1/2} = \text{Airspeed}$$

$$\text{Dynamic pressure} = \bar{q} = \frac{1}{2} \rho(h) V_{air}^2 \triangleq \text{"qbar"}$$

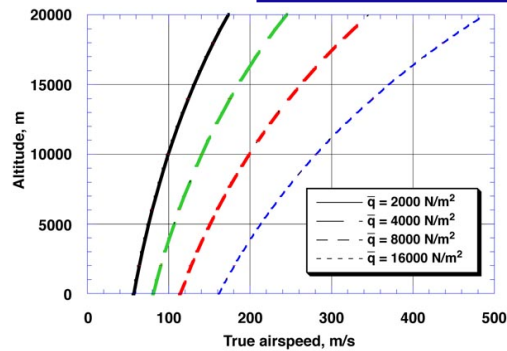
$$\text{Mach number} = \frac{V_{air}}{a(h)}; \quad a = \text{speed of sound, m/s}$$

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Contours of Constant Dynamic Pressure, \bar{q}

- In steady, cruising flight,

$$Weight = Lift = C_L \frac{1}{2} \rho V_{air}^2 S = C_L \bar{q} S$$



True airspeed must increase as altitude increases
to maintain constant dynamic pressure

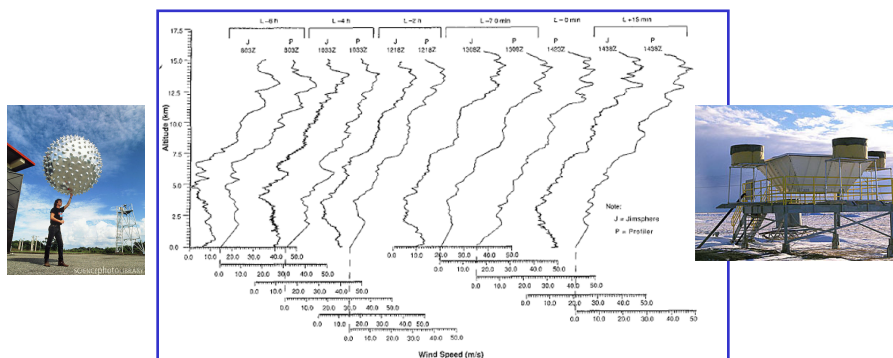
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Wind: Motion of the Atmosphere

Zero wind at Earth's surface = Rotating air mass

Wind measured with respect to Earth's rotating surface

Wind Velocity Profiles vary over Time



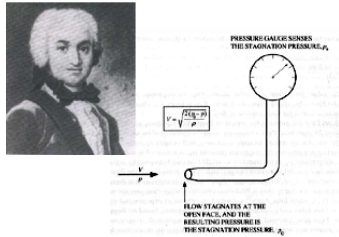
Airspeed = Airplane's speed with respect to air mass

Earth-relative velocity = Wind velocity \pm True airspeed [vector]

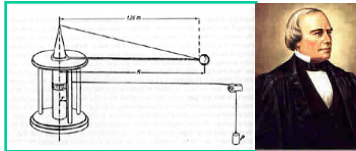
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Historical Factoids

- **Henri Pitot: Pitot tube (1732)**



- **Benjamin Robins: Whirling arm "wind tunnel" (1742)**



NASA SP-440, Wind Tunnels of NASA

Sir George Cayley

- Sketched "modern" airplane configuration (1799)
- Hand-launched glider (1804)



- Applied aerodynamics (1809-1810)
- Triplane glider carrying 10-yr-old boy (1849)
- Monoplane glider carrying coachman (1853)
 - Cayley's coachman had a steering oar with cruciform blades



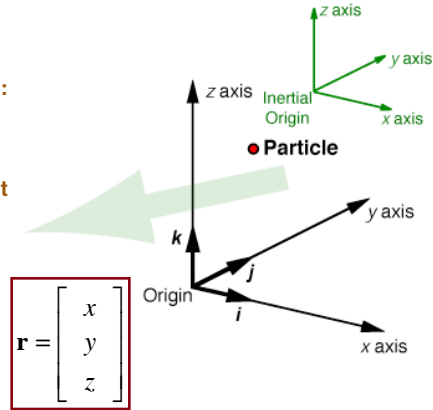
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Equations of Motion for a Particle (Point Mass)

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Newtonian Frame of Reference

- Newtonian (Inertial) Reference Frame
 - Unaccelerated Cartesian frame: origin referenced to inertial (non-moving) frame
 - Right-hand rule
 - Origin can translate at constant linear velocity
 - Frame cannot rotate with respect to inertial origin
- Position: 3 dimensions
- What is a non-moving frame?



Translation changes the position of an object

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Velocity and Momentum

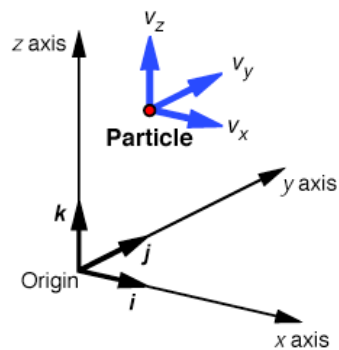
- Velocity of a particle

$$\mathbf{v} = \frac{d\mathbf{x}}{dt} = \dot{\mathbf{x}} = \begin{bmatrix} \dot{x} \\ \dot{y} \\ \dot{z} \end{bmatrix} = \begin{bmatrix} v_x \\ v_y \\ v_z \end{bmatrix}$$

- Linear momentum of a particle

$$\mathbf{p} = m\mathbf{v} = m \begin{bmatrix} v_x \\ v_y \\ v_z \end{bmatrix}$$

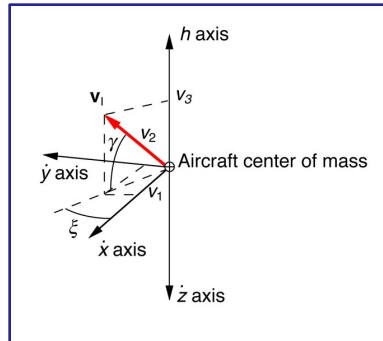
where $m = \text{mass of particle}$



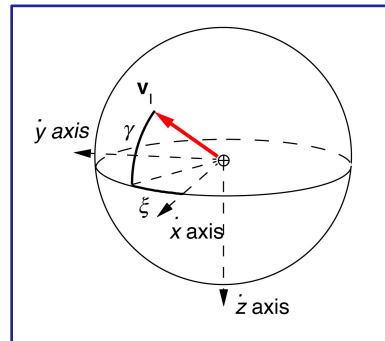
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Inertial Velocity Expressed in Polar Coordinates

Polar Coordinates



Projected on a Sphere



γ : Vertical Flight Path Angle, rad or deg
 ξ : Horizontal Flight Path Angle (Heading Angle), rad or deg

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Newton's Laws of Motion: Dynamics of a Particle

- **First Law:** If **no force** acts on a particle,
 - **it remains at rest or**
 - **continues to move in a straight line at constant velocity**, as observed in an inertial reference frame
 - **Momentum is conserved**

$$\frac{d}{dt}(m\mathbf{v}) = 0 \quad ; \quad m\mathbf{v}|_{t_1} = m\mathbf{v}|_{t_2}$$

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Newton's Laws of Motion: Dynamics of a Particle

- **Second Law:** Particle of fixed mass **acted upon by a force**
 - changes velocity with **acceleration** proportional to and in direction of force, as observed in inertial frame
 - **Mass is** ratio of force to acceleration of particle:

$$\mathbf{F} = m\mathbf{a}$$

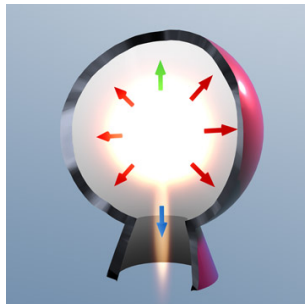
$$\frac{d}{dt}(m\mathbf{v}) = m \frac{d\mathbf{v}}{dt} = \mathbf{F} \quad ; \quad \mathbf{F} = \begin{bmatrix} f_x \\ f_y \\ f_z \end{bmatrix}$$

$$\therefore \frac{d\mathbf{v}}{dt} = \frac{1}{m}\mathbf{F} = \frac{1}{m}\mathbf{I}_3\mathbf{F} = \begin{bmatrix} 1/m & 0 & 0 \\ 0 & 1/m & 0 \\ 0 & 0 & 1/m \end{bmatrix} \begin{bmatrix} f_x \\ f_y \\ f_z \end{bmatrix}$$

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Newton's Laws of Motion: Dynamics of a Particle

- **Third Law**
 - For every **action**, there is an equal and opposite **reaction**



Force on Rocket = Force on Exhaust Gasses

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Equations of Motion for a Particle: Position and Velocity

Force vector

$$\mathbf{F}_I = \begin{bmatrix} f_x \\ f_y \\ f_z \end{bmatrix}_I = \left[\mathbf{F}_{gravity} + \mathbf{F}_{aerodynamics} + \mathbf{F}_{thrust} \right]_I$$

Rate of change of velocity

$$\frac{d\mathbf{v}}{dt} = \dot{\mathbf{v}} = \begin{bmatrix} \dot{v}_x \\ \dot{v}_y \\ \dot{v}_z \end{bmatrix}_I = \frac{1}{m} \mathbf{F} = \begin{bmatrix} 1/m & 0 & 0 \\ 0 & 1/m & 0 \\ 0 & 0 & 1/m \end{bmatrix} \begin{bmatrix} f_x \\ f_y \\ f_z \end{bmatrix}_I$$

Rate of change of position

$$\frac{d\mathbf{r}}{dt} = \dot{\mathbf{r}} = \begin{bmatrix} \dot{x} \\ \dot{y} \\ \dot{z} \end{bmatrix}_I = \mathbf{v} = \begin{bmatrix} v_x \\ v_y \\ v_z \end{bmatrix}_I$$

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Integration for Velocity with Constant Force

Differential equation

$$\frac{d\mathbf{v}(t)}{dt} = \dot{\mathbf{v}}(t) = \frac{1}{m} \mathbf{F} = \begin{bmatrix} f_x/m \\ f_y/m \\ f_z/m \end{bmatrix} = \begin{bmatrix} a_x \\ a_y \\ a_z \end{bmatrix}$$

Integral

$$\mathbf{v}(T) = \int_0^T \frac{d\mathbf{v}(t)}{dt} dt + \mathbf{v}(0) = \int_0^T \frac{1}{m} \mathbf{F} dt + \mathbf{v}(0) = \int_0^T \mathbf{a} dt + \mathbf{v}(0)$$

$$\begin{bmatrix} v_x(T) \\ v_y(T) \\ v_z(T) \end{bmatrix} = \int_0^T \begin{bmatrix} f_x/m \\ f_y/m \\ f_z/m \end{bmatrix} dt + \begin{bmatrix} v_x(0) \\ v_y(0) \\ v_z(0) \end{bmatrix} = \int_0^T \begin{bmatrix} a_x \\ a_y \\ a_z \end{bmatrix} dt + \begin{bmatrix} v_x(0) \\ v_y(0) \\ v_z(0) \end{bmatrix}$$

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Integration for Position with Varying Velocity

Differential equation

$$\frac{d\mathbf{r}(t)}{dt} = \dot{\mathbf{r}}(t) = \mathbf{v}(t) = \begin{bmatrix} \dot{x}(t) \\ \dot{y}(t) \\ \dot{z}(t) \end{bmatrix} = \begin{bmatrix} v_x(t) \\ v_y(t) \\ v_z(t) \end{bmatrix}$$

Integral

$$\mathbf{r}(T) = \int_0^T \frac{d\mathbf{r}(t)}{dt} dt + \mathbf{r}(0) = \int_0^T \mathbf{v}(t) dt + \mathbf{r}(0)$$

$$\begin{bmatrix} x(T) \\ y(T) \\ z(T) \end{bmatrix} = \int_0^T \begin{bmatrix} v_x(t) \\ v_y(t) \\ v_z(t) \end{bmatrix} dt + \begin{bmatrix} x(0) \\ y(0) \\ z(0) \end{bmatrix}$$

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Gravitational Force: Flat-Earth Approximation

- **Approximation**
 - Flat earth reference assumed to be inertial frame, *e.g.*,
 - North, East, Down
 - Range, Crossrange, Altitude (-)
- **g is gravitational acceleration**
- **mg is gravitational force**
- **Independent of position**
- **z measured down**

$$\left(\mathbf{F}_{gravity} \right)_I = \left(\mathbf{F}_{gravity} \right)_E = m\mathbf{g}_E = m \begin{bmatrix} 0 \\ 0 \\ g_o \end{bmatrix}_E$$

$$g_o \approx 9.807 \text{ m/s}^2 \text{ at earth's surface}$$

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Flight Path Dynamics, Constant Gravity, No Aerodynamics

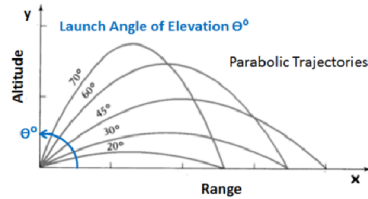
$$\begin{aligned} v_x(0) &= v_{x_0} \\ v_z(0) &= v_{z_0} \\ x(0) &= x_0 \\ z(0) &= z_0 \end{aligned}$$

Differential equation

$$\begin{aligned} \dot{v}_x(t) &= 0 \\ \dot{v}_z(t) &= -g \quad (z \text{ positive up}) \\ \dot{x}(t) &= v_x(t) \\ \dot{z}(t) &= v_z(t) \end{aligned}$$

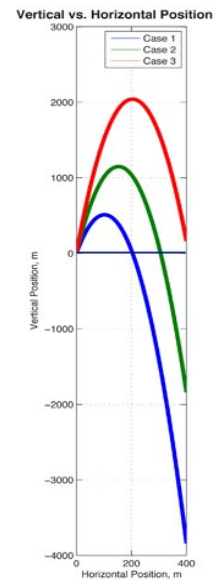
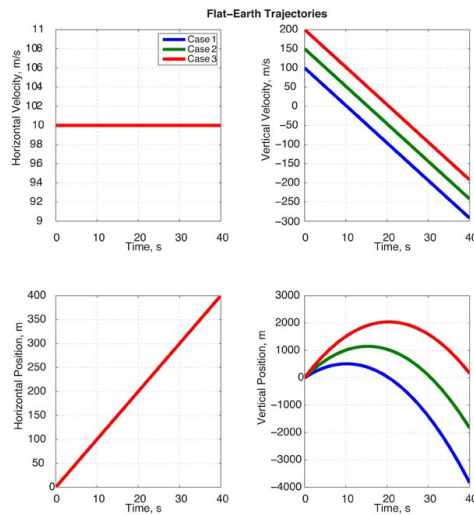
Integral

$$\begin{aligned} v_x(T) &= v_{x_0} \\ v_z(T) &= v_{z_0} - \int_0^T g dt = v_{z_0} - gT \\ x(T) &= x_0 + v_{x_0} T \\ z(T) &= z_0 + v_{z_0} T - \int_0^T gt dt = z_0 + v_{z_0} T - gT^2/2 \end{aligned}$$



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Flight Path with Constant Gravity and No Aerodynamics



Aerodynamic Force on an Airplane



Earth-Reference Frame

$$\mathbf{F}_I = \begin{bmatrix} X \\ Y \\ Z \end{bmatrix}_E = \begin{bmatrix} C_X \\ C_Y \\ C_Z \end{bmatrix}_E \frac{1}{2} \rho V_{air}^2 S$$

$$= \begin{bmatrix} C_X \\ C_Y \\ C_Z \end{bmatrix}_E \bar{q} S$$

Referenced to the Earth, not the aircraft (e.g., North, East, Down)

Body-Axis Frame

$$\mathbf{F}_B = \begin{bmatrix} C_X \\ C_Y \\ C_Z \end{bmatrix}_B \bar{q} S$$

Aligned with the aircraft axes (e.g., Nose, Wing Tip, Down)

Wind-Axis Frame

$$\mathbf{F}_V = \begin{bmatrix} C_D \\ C_Y \\ C_L \end{bmatrix} \bar{q} S$$

Aligned with and perpendicular to the velocity vector (Forward, Sideward, Down)

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Non-Dimensional Aerodynamic Coefficients

Body-Axis Frame

$$\begin{bmatrix} C_X \\ C_Y \\ C_Z \end{bmatrix}_B = \begin{bmatrix} \text{axial force coefficient} \\ \text{side force coefficient} \\ \text{normal force coefficient} \end{bmatrix}$$

Wind-Axis Frame

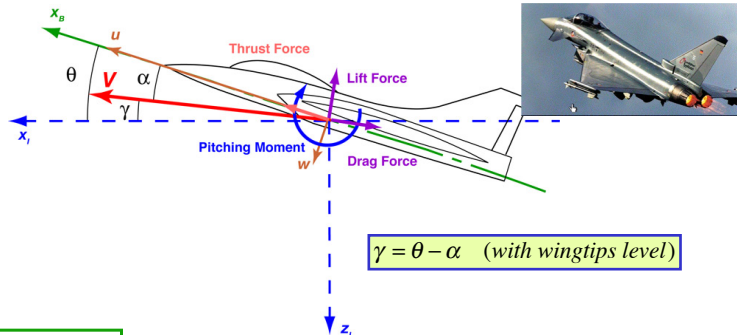
$$\begin{bmatrix} C_D \\ C_Y \\ C_L \end{bmatrix} = \begin{bmatrix} \text{drag coefficient} \\ \text{side force coefficient} \\ \text{lift coefficient} \end{bmatrix}$$

- Functions of flight condition, control settings, and disturbances, e.g., $C_L = C_L(\delta, M, \delta E)$
- Non-dimensional coefficients allow application of sub-scale model wind tunnel data to full-scale airplane



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Longitudinal Variables



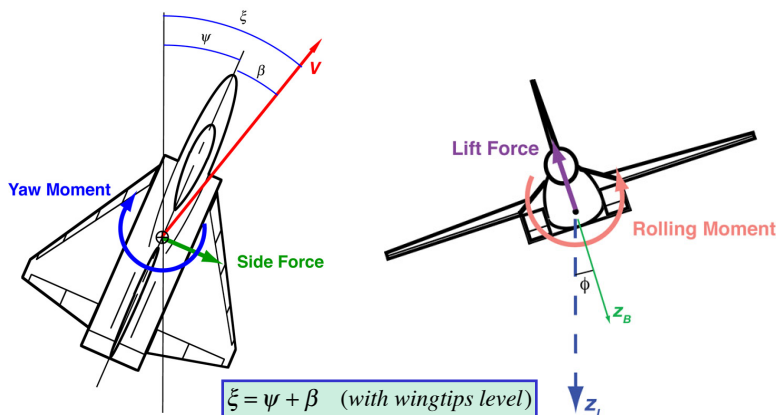
$$\gamma = \theta - \alpha \quad (\text{with wingtips level})$$

$u(t)$: axial velocity
 $w(t)$: normal velocity
 $V(t)$: velocity magnitude
 $\alpha(t)$: angle of attack
 $\gamma(t)$: flight path angle
 $\theta(t)$: pitch angle

- along vehicle centerline
- perpendicular to centerline
- along net direction of flight
- angle between centerline and direction of flight
- angle between direction of flight and local horizontal
- angle between centerline and local horizontal

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Lateral-Directional Variables



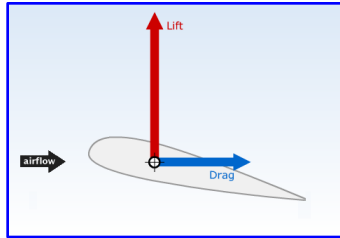
$$\xi = \psi + \beta \quad (\text{with wingtips level})$$

$\beta(t)$: sideslip angle
 $\psi(t)$: yaw angle
 $\xi(t)$: heading angle
 $\phi(t)$: roll angle

- angle between centerline and direction of flight
- angle between centerline and local horizontal
- angle between direction of flight and compass reference (e.g., north)
- angle between true vertical and body z axis

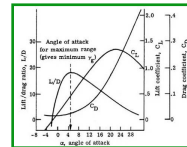
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Introduction to Lift and Drag



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Lift and Drag are Referenced to Velocity Vector



$$Lift = C_L \frac{1}{2} \rho V_{air}^2 S \approx \left[C_{L_0} + \frac{\partial C_L}{\partial \alpha} \alpha \right] \frac{1}{2} \rho V_{air}^2 S$$

- Lift components sum to produce total lift
 - **Perpendicular** to velocity vector
 - Pressure differential between upper and lower surfaces

$$Drag = C_D \frac{1}{2} \rho V_{air}^2 S \approx \left[C_{D_0} + \epsilon C_L^2 \right] \frac{1}{2} \rho V_{air}^2 S$$

- Drag components sum to produce total drag
 - **Parallel** and **opposed** to velocity vector
 - Skin friction, pressure differentials

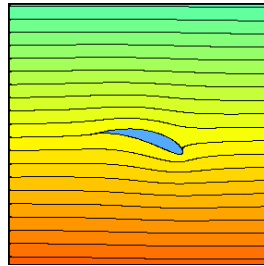
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2-D Aerodynamic Lift

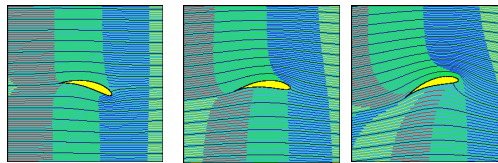
$$Lift = C_L \frac{1}{2} \rho V_{air}^2 S \approx (C_{L_{wing}} + C_{L_{fuselage}} + C_{L_{tail}}) \frac{1}{2} \rho V_{air}^2 S \approx \left[C_{L_0} + \frac{\partial C_L}{\partial \alpha} \alpha \right] \bar{q} S$$

- Upper/lower speed difference proportional to angle of attack
- Stagnation points at leading and trailing edges
 - **Kutta condition:** Aft stagnation point at sharp trailing edge

Streamlines
Instantaneous tangent to velocity vector



Streaklines
Locus of particles passing through points
Dye injected at fixed points

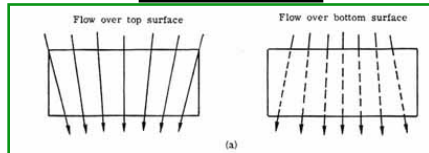


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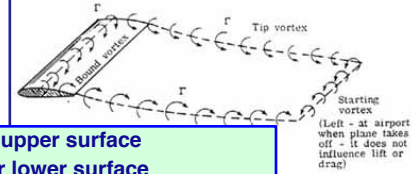
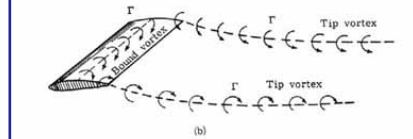
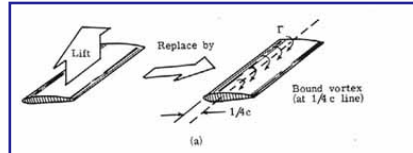
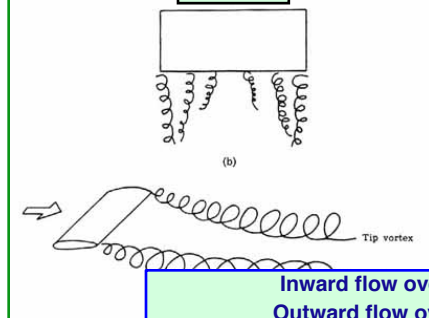
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3-D Lift

Inward-Outward Flow



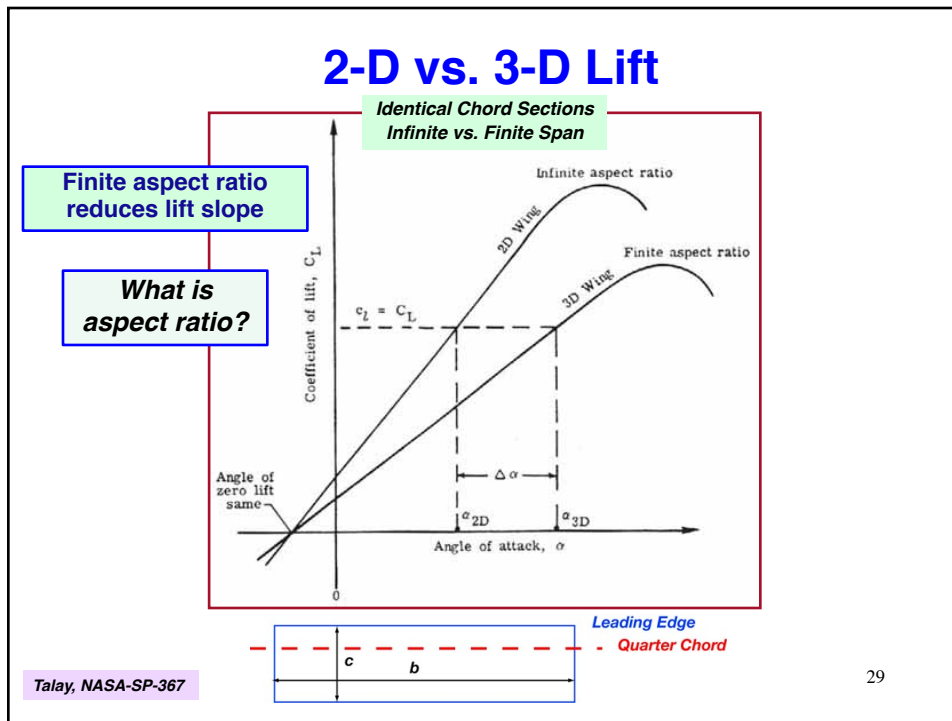
Tip Vortices



Inward flow over upper surface
Outward flow over lower surface
Bound vorticity of wing produces tip vortices

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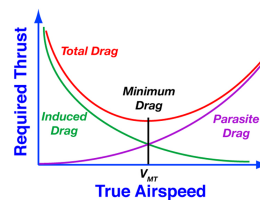
2-D vs. 3-D Lift



Aerodynamic Drag

$$Drag = C_D \frac{1}{2} \rho V_{air}^2 S \approx (C_{D_p} + C_{D_w} + C_{D_i}) \frac{1}{2} \rho V_{air}^2 S \approx [C_{D_0} + \epsilon C_L^2] \bar{q} S$$

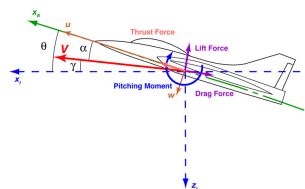
- **Drag components**
 - Parasite drag (friction, interference, base pressure differential)
 - Wave drag (shock-induced pressure differential)
 - Induced drag (drag due to lift generation)
- **In steady, subsonic flight**
 - Parasite (form) drag increases as V^2
 - Induced drag (due to lift) proportional to $1/V^2$
 - Total drag minimized at one particular airspeed



2-D Equations of Motion with Aerodynamics and Thrust

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2-D Equations of Motion for a Point Mass



- Motions restricted to vertical plane
- Inertial frame, wind = 0
- z positive down, flat-earth assumption
- Point-mass location coincides with aircraft's center of mass

$$\begin{bmatrix} \dot{x} \\ \dot{z} \\ \dot{v}_x \\ \dot{v}_z \end{bmatrix} = \begin{bmatrix} v_x \\ v_z \\ f_x/m \\ f_z/m \end{bmatrix}$$

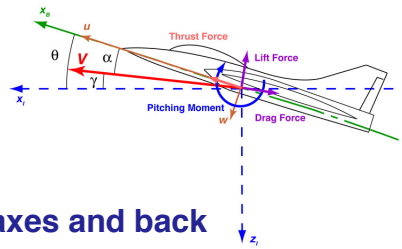
$$= \begin{bmatrix} 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} x \\ z \\ v_x \\ v_z \end{bmatrix} + \begin{bmatrix} 0 & 0 \\ 0 & 0 \\ 1/m & 0 \\ 0 & 1/m \end{bmatrix} \begin{bmatrix} (C_T \cos \theta + C_{x_i}) \bar{q} S \\ (-C_T \sin \theta + C_{z_i}) \bar{q} S + mg_o \end{bmatrix}$$

$$\bar{q} = \frac{1}{2} \rho(z) (v_x^2 + v_z^2)$$

C_T = Thrust coefficient
 θ = Pitch angle

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Transform Velocity from Cartesian to Polar Coordinates



Inertial axes -> wind axes and back

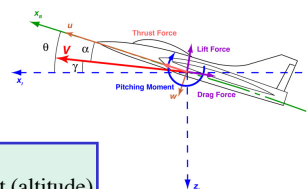
$$\begin{bmatrix} \dot{x} \\ \dot{z} \end{bmatrix} = \begin{bmatrix} v_x \\ v_z \end{bmatrix} = \begin{bmatrix} V \cos \gamma \\ -V \sin \gamma \end{bmatrix} \Rightarrow \begin{bmatrix} V \\ \gamma \end{bmatrix} = \begin{bmatrix} \sqrt{\dot{x}^2 + \dot{z}^2} \\ -\sin^{-1}\left(\frac{\dot{z}}{V}\right) \end{bmatrix} = \begin{bmatrix} \sqrt{v_x^2 + v_z^2} \\ -\sin^{-1}\left(\frac{v_z}{V}\right) \end{bmatrix}$$

Rates of change of velocity and flight path angle

$$\begin{bmatrix} \dot{V} \\ \dot{\gamma} \end{bmatrix} = \begin{bmatrix} \frac{d}{dt} \sqrt{v_x^2 + v_z^2} \\ -\frac{d}{dt} \sin^{-1}\left(\frac{v_z}{V}\right) \end{bmatrix}$$

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Longitudinal Point-Mass Equations of Motion



$$\dot{x}(t) = v_x = V(t) \cos \gamma(t)$$

$$\dot{z}(t) = v_z = -V(t) \sin \gamma(t)$$

x : range
 z : -height (altitude)
 V : velocity
 γ : flight path angle

$$\dot{V}(t) = \frac{(C_T \cos \alpha - C_D) \frac{1}{2} \rho(z) V^2(t) S - mg_o \sin \gamma(t)}{m}$$

$$\dot{\gamma}(t) = \frac{(C_T \sin \alpha + C_L) \frac{1}{2} \rho(z) V^2(t) S - mg_o \cos \gamma(t)}{mV(t)}$$

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Steady, Level (*i.e.*, Cruising) Flight

In steady, level flight with $\cos \alpha \sim 1$, $\sin \alpha \sim 0$
Thrust = Drag, Lift = Weight

$$V_{cruise} = \dot{x}(t) = v_x$$

$$0 = \dot{z}(t) = v_z$$

$$0 = \frac{(C_T - C_D) \frac{1}{2} \rho(z) V_{cruise}^2 S}{m}$$

$$0 = \frac{C_L \frac{1}{2} \rho(z) V_{cruise}^2 S - mg(z)}{mV_{cruise}}$$

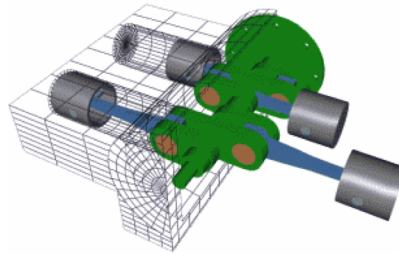
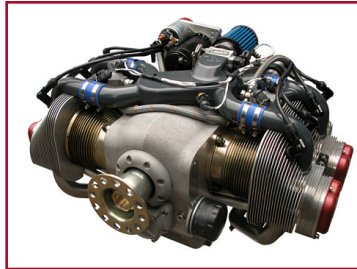
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Introduction to Aeronautical Propulsion

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Internal Combustion Reciprocating Engine

Linear motion of pistons converted to rotary motion to drive propeller

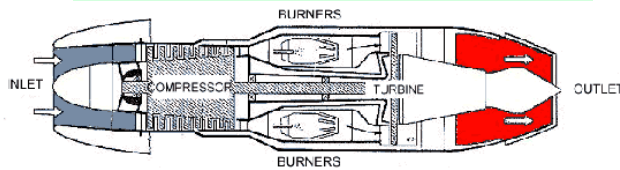


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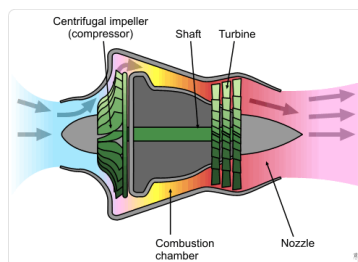
Turbojet Engines (1930s)

Thrust produced directly by exhaust gas

Axial-flow Turbojet (von Ohain, Germany)



Centrifugal-flow Turbojet (Whittle, UK)



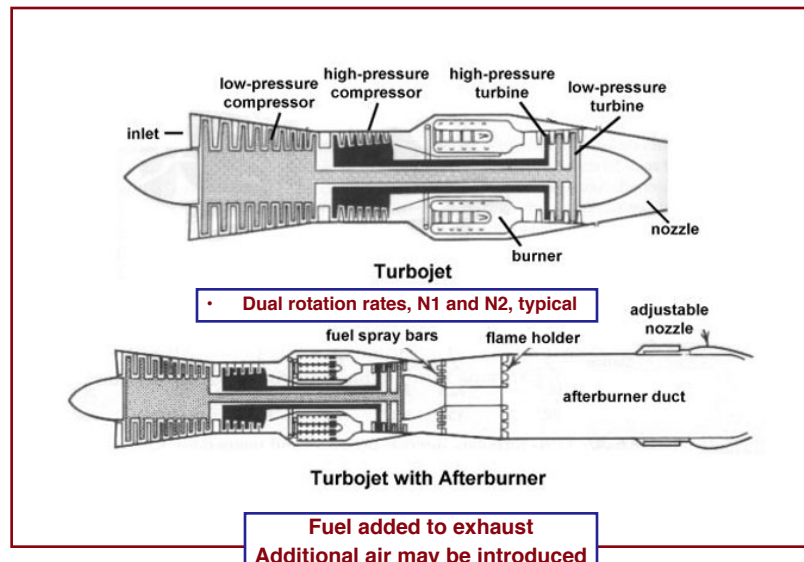
38

Birth of the Jet Airplane



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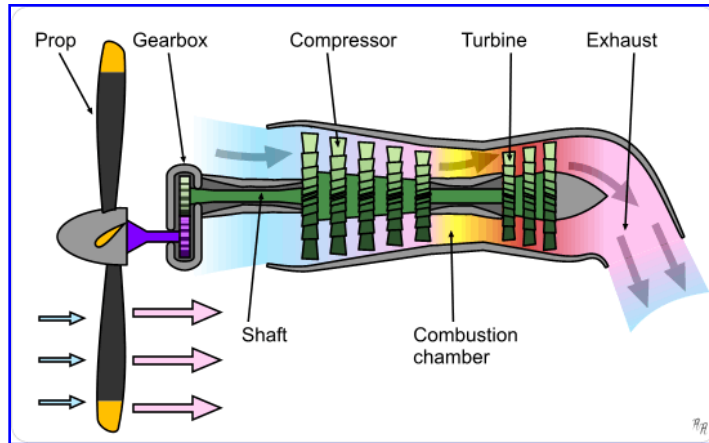
Turbojet + Afterburner (1950s)



40

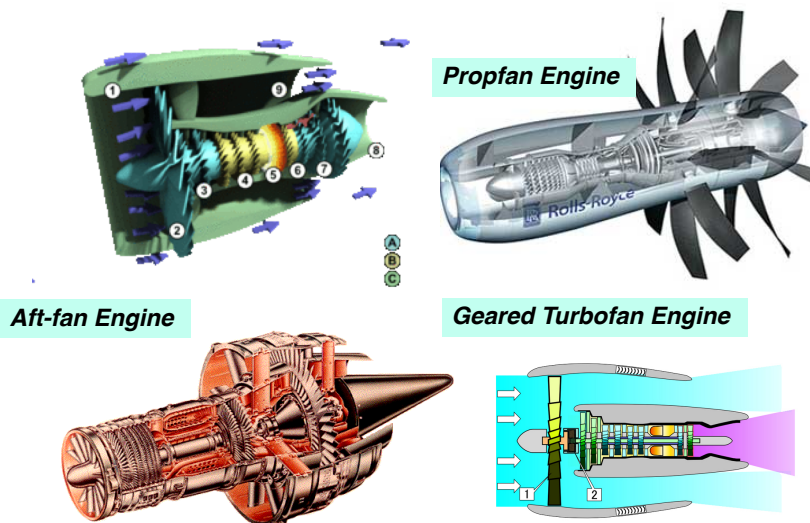
Turboprop Engines (1940s)

Exhaust gas drives propeller to produce thrust



41

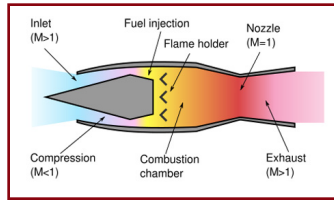
High Bypass Ratio Turbofan



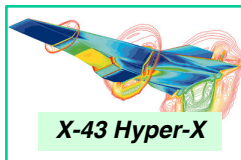
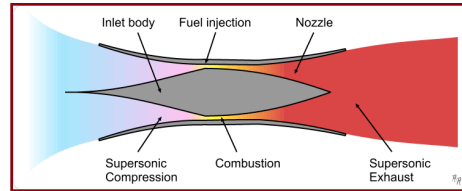
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Ramjet and Scramjet

Ramjet (1940s)

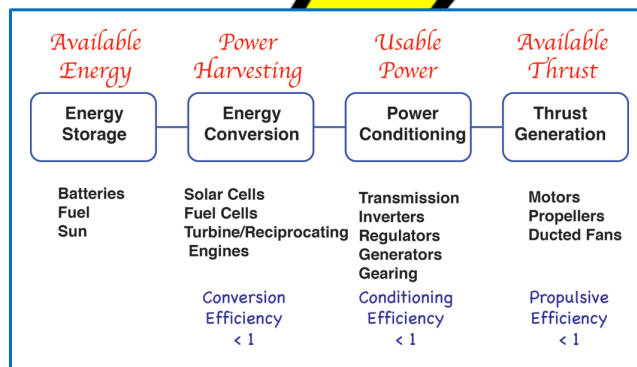


Scramjet (1950s)



43

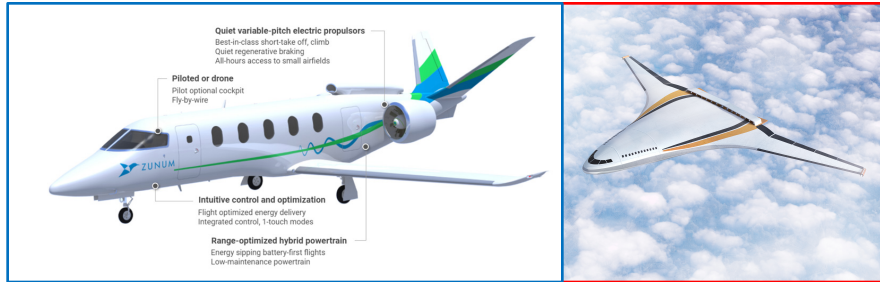
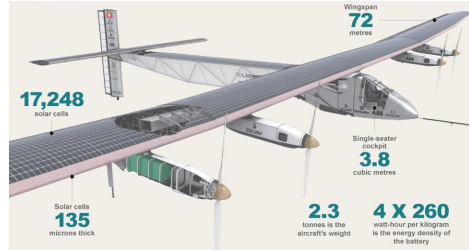
Electric Propulsion



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Electric Aircraft

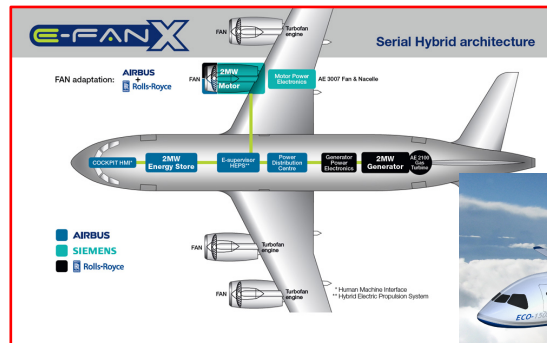
- Solar cells/batteries
- Fuel cells
- Batteries



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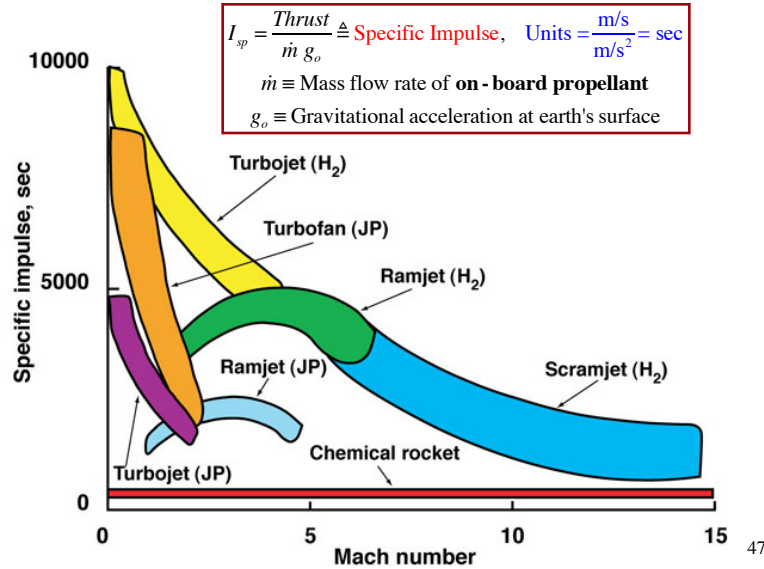
Hybrid-Electric Aircraft

- Turbine engines
- Generators
- Thrust
- Drag reduction



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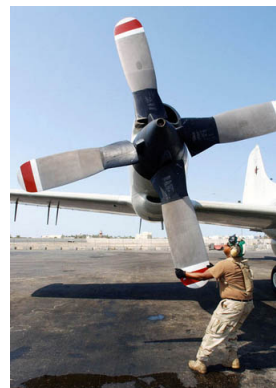
Thrust and Specific Impulse



Thrust and Thrust Coefficient

$$Thrust \equiv C_T \frac{1}{2} \rho V^2 S$$

- Non-dimensional thrust coefficient, C_T
 - C_T is a function of power/throttle setting, fuel flow rate, blade angle, Mach number, ...
- Reference area, S , may be
 - aircraft wing area,
 - propeller disk area, or
 - jet exhaust area



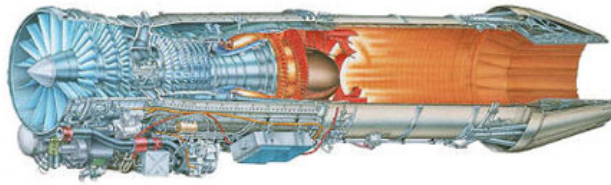
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Sensitivity of Thrust to Airspeed

$$\text{Nominal Thrust} = T_N \equiv C_{T_N} \frac{1}{2} \rho V_N^2 S$$

$(\cdot)_N$ = Nominal (or reference) value

Turbojet thrust is ~independent of airspeed over wide range



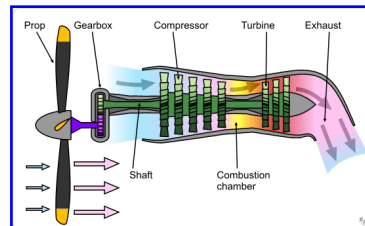
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Power

Assuming thrust is aligned with airspeed vector

$$\text{Power} = P = \text{Thrust} \times \text{Velocity} \equiv C_T \frac{1}{2} \rho V^3 S$$

Propeller-driven power is ~independent of (subsonic) airspeed over a wide range
(reciprocating or turbine engine, with constant RPM or variable-pitch prop)



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Next Time: Low-Speed Aerodynamics

*Reading:
Flight Dynamics
Aerodynamic Coefficients, 65-84*

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Supplementary Material

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MATLAB Scripts for Flat-Earth Trajectory, No Aerodynamics

Analytical Solution

```
g = 9.8;
t = 0:0.1:40;

vx0 = 10;
vz0 = 100;
x0 = 0;
z0 = 0;

vx1 = vx0;
vz1 = vz0 - g*t;
x1 = x0 + vx0*t;
z1 = z0 + vz0*t - 0.5*g*t.* t;
```

Numerical Solution

Calling Routine

```
tspan = 40;
xo = [10;100;0;0];
[t1,x1] = ode45('FlatEarth',tspan,xo);
```

Equations of Motion

```
function xdot = FlatEarth(t,x)
% x(1) = vx
% x(2) = vz
% x(3) = x
% x(4) = z
g = 9.8;
xdot(1) = 0;
xdot(2) = -g;
xdot(3) = x(1);
xdot(4) = x(2);
xdot = xdot';
end
```

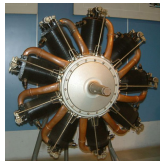
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Early Reciprocating Engines

- **Rotary Engine:**
 - Air-cooled
 - Crankshaft fixed
 - Cylinders turn with propeller
 - On/off control: No throttle

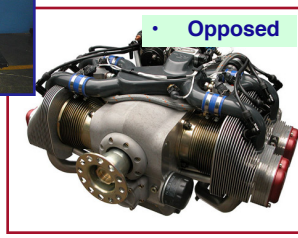
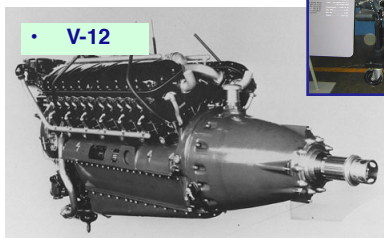
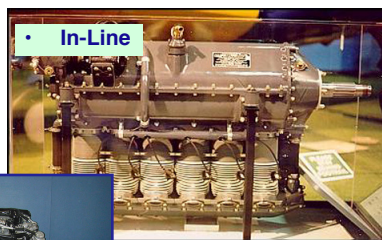
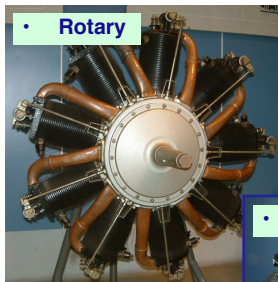


- **V-8 Engine:**
 - Water-cooled
 - Crankshaft turns with propeller



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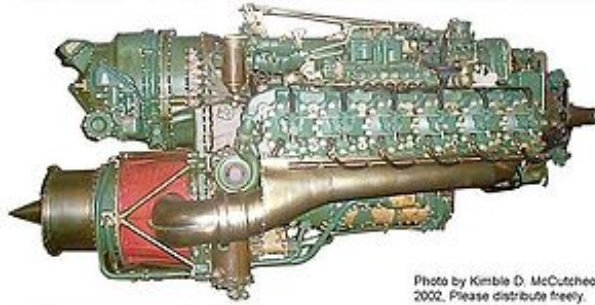
Reciprocating Engines



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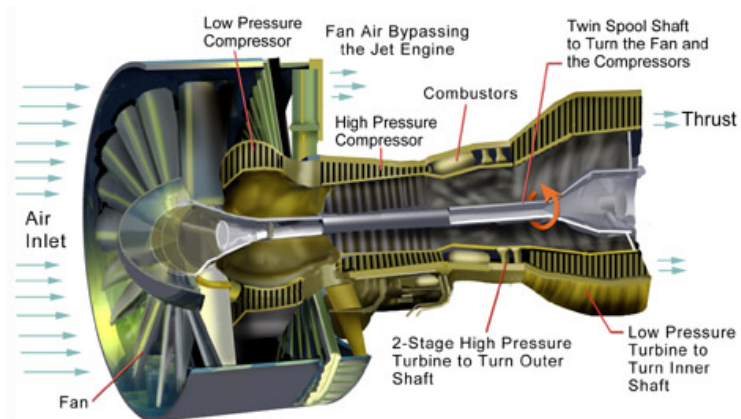
Turbo-compound Reciprocating Engine

- Exhaust gas drives the turbo-compressor
- Napier Nomad II shown (1949)



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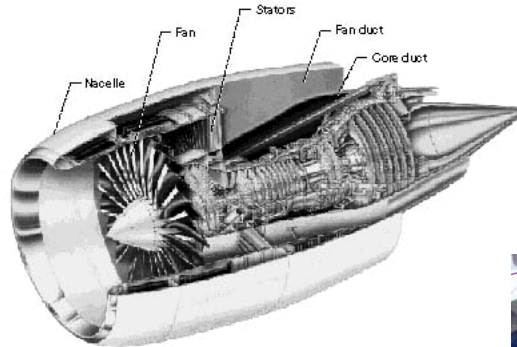
Turbofan Engine (1960s)



- Dual or triple rotation rates

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Jet Engine Nacelles



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Propeller-Driven Aircraft of the 1950s

Reciprocating Engines



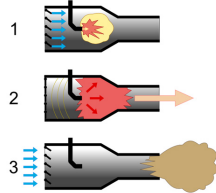
Turboprop Engines



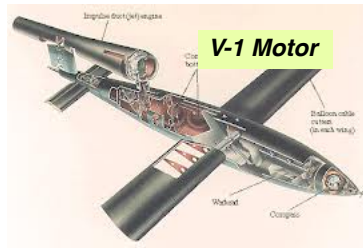
60

Pulsejet

Flapper-valved motor (1940s)



Dynajet Red Head (1950s)



Pulse Detonation Engine on Long EZ (1981)



<http://airplanesandrocks.com/motors/dynajet-engine.htm>

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Jet Transports of the 2000s



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SR-71: P&W J58 Variable-Cycle Engine (Late 1950s)

Hybrid
Turbojet/Ramjet

