

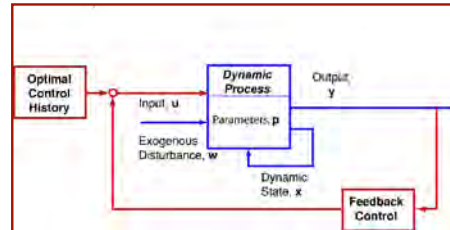
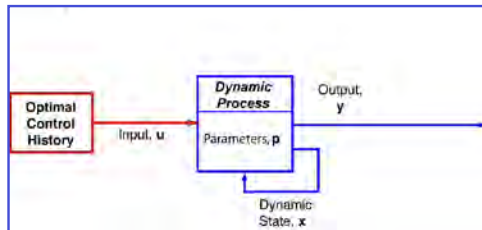
Dynamic Optimal Control

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Robotics and Intelligent Systems MAE 345, Princeton University, 2017

Learning Objectives

- Examples of cost functions
- Necessary conditions for optimality
- Calculation of optimal trajectories
- Design of optimal feedback control laws



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<http://www.princeton.edu/~stengel/MAE345.html>

1

Integrated Effect can be a Scalar "Cost"



Time

$$J = \int_0^{\text{final time}} (1) dt$$

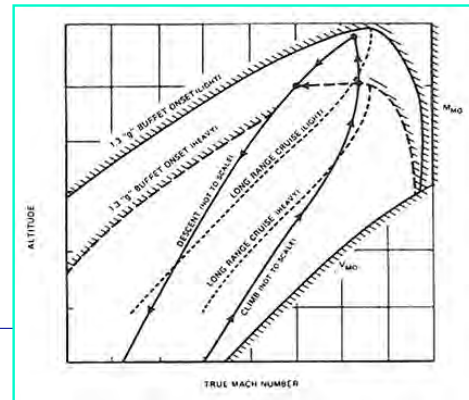
Fuel

$$J = \int_0^{\text{final range}} (\text{fuel use per kilometer}) dR$$

Financial cost of time and fuel

$$J = \int_0^{\text{final time}} (\text{cost per hour}) dt$$

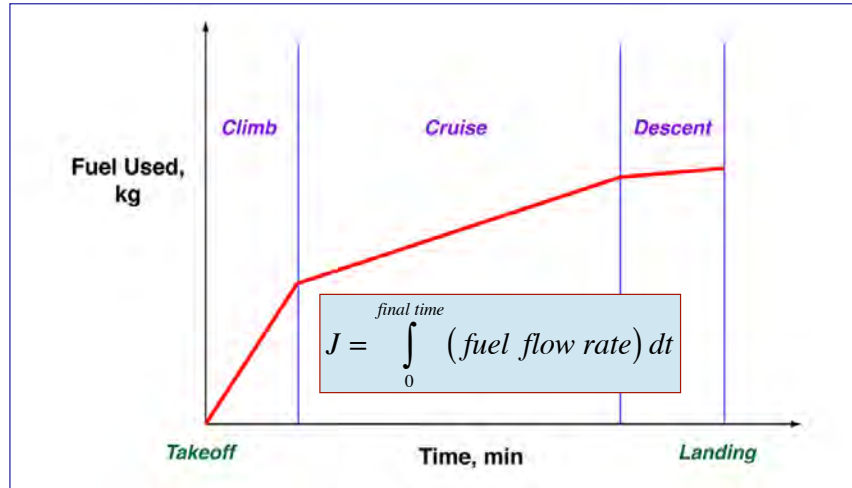
$$= \int_0^{\text{final time}} \left[\left(\frac{\text{cost}}{\text{hour}} \right) + \left(\frac{\text{cost}}{\text{liter}} \right) \left(\frac{\text{liter}}{\text{kilometer}} \right) \frac{dR}{dt} \right] dt$$



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Cost Accumulates from Start to Finish



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Optimal System Regulation

Cost functions that penalize state deviations over a time interval:

Quadratic scalar variation

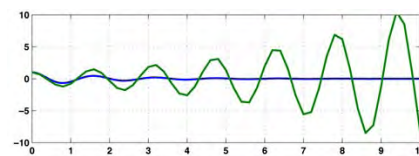
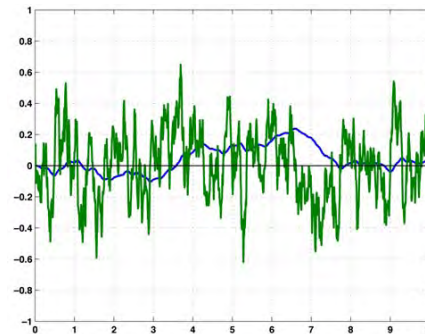
$$J = \lim_{T \rightarrow \infty} \frac{1}{T} \int_0^T (\Delta x^2) dt < \infty$$

Vector variation

$$J = \lim_{T \rightarrow \infty} \frac{1}{T} \int_0^T (\Delta \mathbf{x}^T \Delta \mathbf{x}) dt < \infty$$

Weighted vector variation

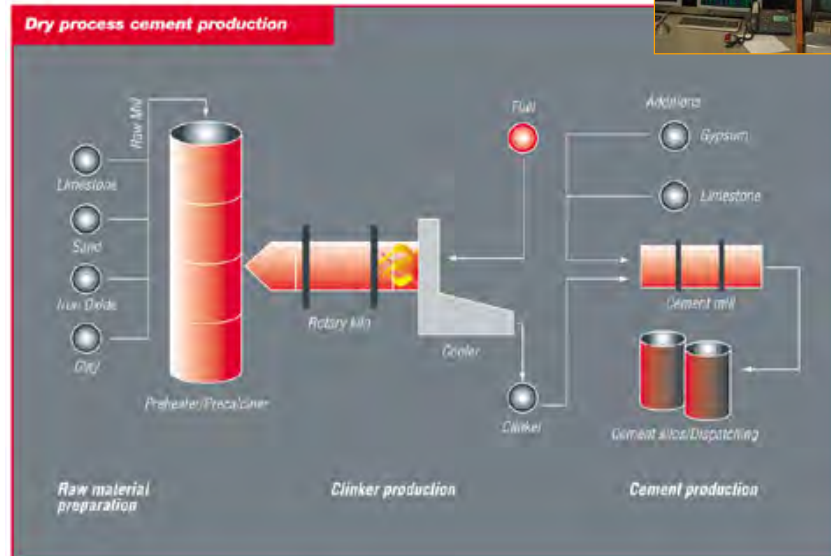
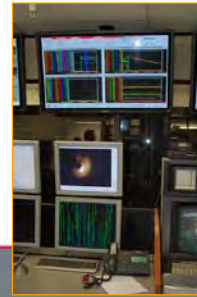
$$J = \lim_{T \rightarrow \infty} \frac{1}{T} \int_0^T (\Delta \mathbf{x}^T \mathbf{Q} \Delta \mathbf{x}) dt < \infty$$



- **No penalty for control use**
- **Why not use infinite control?**

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Cement Kiln

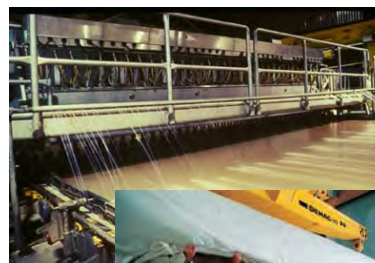


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Pulp & Paper Machines



- Machine length: ~ 2 football fields
- Paper speed $\leq 2,200$ m/min = 80 mph
- Maintain 3-D paper quality
- Avoid paper breaks at all cost!



Paper-Making Machine Operation
<https://www.youtube.com/watch?v=6BhEXBAak24>

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Hazardous Waste Generated by Large Industrial Plants

- Cement dust
- Coal fly ash
- Metal emissions
- Dioxin
- “Electroscrap” and other hazardous waste
- Waste chemicals
- Ground water contamination
- Ancillary mining and logging issues
- “Greenhouse” gasses
- **Need to optimize total “cost”-benefit of production processes (including health/environmental/regulatory cost)**

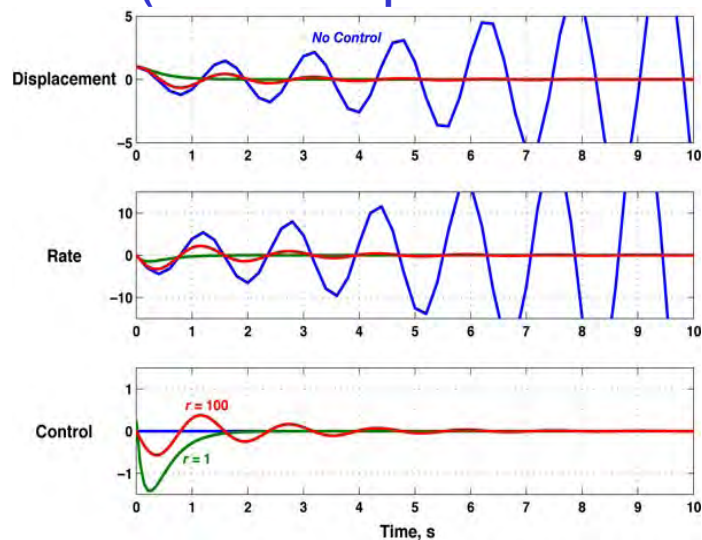


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Tradeoffs Between Performance and Control in Integrated Cost Function

Trade performance against control usage

Minimize a cost function that contains state and control (r : relative importance of the two)



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Dynamic Optimization: The Optimal Control Problem

Minimize a scalar function, J , of
terminal and integral costs

$$\min_{\mathbf{u}(t)} J = \min_{\mathbf{u}(t)} \left\{ \phi[\mathbf{x}(t_f)] + \int_{t_o}^{t_f} L[\mathbf{x}(t), \mathbf{u}(t)] dt \right\}$$

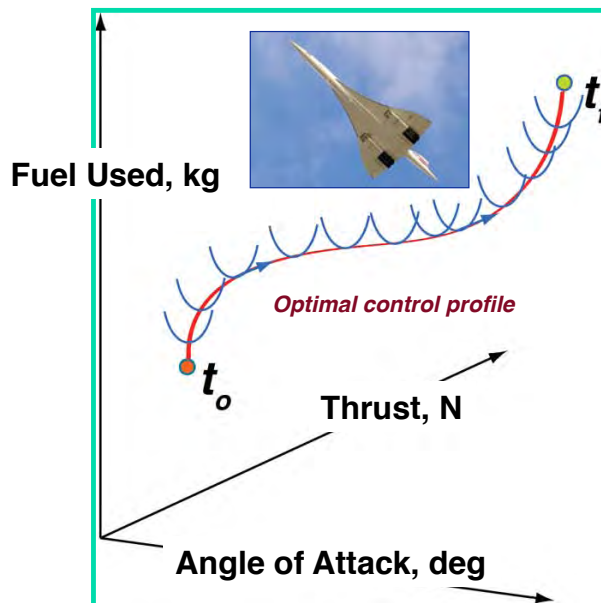
with respect to the control, $\mathbf{u}(t)$, in (t_o, t_f) ,
subject to a dynamic constraint

$$\frac{d\mathbf{x}(t)}{dt} = \mathbf{f}[\mathbf{x}(t), \mathbf{u}(t)], \quad \mathbf{x}(t_o) \text{ given}$$

$$\begin{aligned} \dim(\mathbf{x}) &= n \times 1 \\ \dim(\mathbf{f}) &= n \times 1 \\ \dim(\mathbf{u}) &= m \times 1 \end{aligned}$$

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Example of Dynamic Optimization



Any deviation from optimal thrust and angle-of-attack profiles would increase total fuel used

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Components of the Cost Function

Integral cost is a function of the state and control from start to finish

$$\int_{t_o}^{t_f} L[\mathbf{x}(t), \mathbf{u}(t)] dt \quad \text{positive scalar function of two vectors}$$

$L[\mathbf{x}(t), \mathbf{u}(t)]$: **Lagrangian** of the cost function

Terminal cost is a function of the state at the final time

$\phi[\mathbf{x}(t_f)]$ **positive scalar function of a vector**

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Components of the Cost Function

Lagrangian examples

$$L[\mathbf{x}(t), \mathbf{u}(t)] = \begin{cases} 1 \\ dm/dt \\ d\$/dt \\ \frac{1}{2}[\mathbf{x}^T(t)\mathbf{Q}\mathbf{x}(t) + \mathbf{u}(t)\mathbf{R}\mathbf{u}(t)] \end{cases}$$

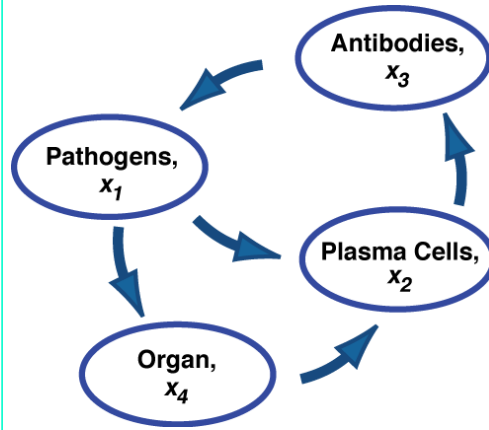
Terminal cost examples

$$\phi[\mathbf{x}(t_f)] = \begin{cases} |\mathbf{x}(t_f) - \mathbf{x}_{Goal}| \\ \frac{1}{2}[\mathbf{x}(t_f) - \mathbf{x}_{Goal}]^2 \end{cases}$$

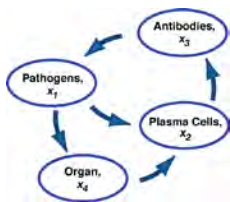
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Example: Dynamic Model of Infection and Immune Response

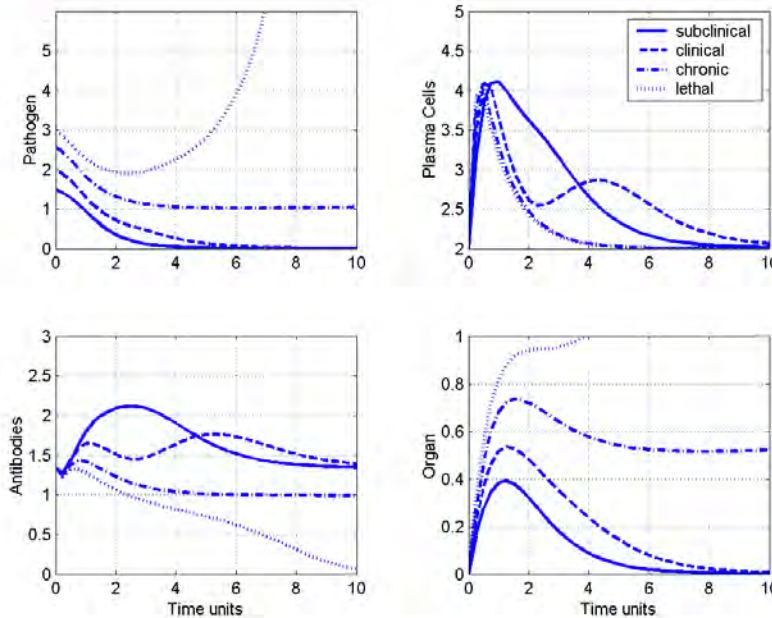
- x_1 = Concentration of a **pathogen**, which displays antigen
- x_2 = Concentration of **plasma cells**, which are carriers and producers of antibodies
- x_3 = Concentration of **antibodies**, which recognize antigen and kill pathogen
- x_4 = Relative characteristic of a **damaged organ** [0 = healthy, 1 = dead]



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Natural Response to Pathogen Assault (No Therapy)



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Cost Function Considers Infection, Organ Health, and Drug Usage

$$\min_{\mathbf{u}(t)} J = \min_{\mathbf{u}(t)} \left\{ \phi[\mathbf{x}(t_f)] + \int_{t_o}^{t_f} L[\mathbf{x}(t), \mathbf{u}(t)] dt \right\}$$

$$= \min_u \left[\frac{1}{2} (s_{11}x_{1_f}^2 + s_{44}x_{4_f}^2) + \frac{1}{2} \int_{t_o}^{t_f} (q_{11}x_1^2 + q_{44}x_4^2 + ru^2) dt \right]$$

- Tradeoffs between final values, integral values over a fixed time interval, state, and control
- Cost function includes weighted square values of
 - Final concentration of the pathogen
 - Final health of the damaged organ (0 is good, 1 is bad)
 - Integral of pathogen concentration
 - Integral health of the damaged organ (0 is good, 1 is bad)
 - Integral of drug usage
- Drug cost may reflect physiological or financial cost

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*Necessary Conditions
for Optimal Control*

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Augment the Cost Function

- Must express sensitivity of the cost to the dynamic response
- Adjoin *dynamic constraint* to *integrand* using **Lagrange multiplier, $\lambda(t)$**
 - Same dimension as the dynamic constraint, $[n \times 1]$
 - Constraint = 0 when the dynamic equation is satisfied

$$J = \phi[\mathbf{x}(t_f)] + \int_{t_o}^{t_f} \left\{ L[\mathbf{x}(t), \mathbf{u}(t)] + \boldsymbol{\lambda}^T(t) \left[\mathbf{f}[\mathbf{x}(t), \mathbf{u}(t)] - \frac{d\mathbf{x}(t)}{dt} \right] \right\} dt$$

- Optimization goal is to minimize J with respect to $\mathbf{u}(t)$ in (t_o, t_f) ,

$$\min_{\mathbf{u}(t)} J = J^* = \phi[\mathbf{x}^*(t_f)] + \int_{t_o}^{t_f} \left\{ L[\mathbf{x}^*(t), \mathbf{u}^*(t)] + \boldsymbol{\lambda}^{*T}(t) \left[\mathbf{f}[\mathbf{x}^*(t), \mathbf{u}^*(t)] - \frac{d\mathbf{x}^*(t)}{dt} \right] \right\} dt$$

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Substitute the Hamiltonian in the Cost Function

Define **Hamiltonian, $H[\cdot]$**

$$H(\mathbf{x}, \mathbf{u}, \boldsymbol{\lambda}) \triangleq L(\mathbf{x}, \mathbf{u}) + \boldsymbol{\lambda}^T \mathbf{f}(\mathbf{x}, \mathbf{u})$$

Substitute the Hamiltonian in the cost function

$$J = \phi[\mathbf{x}(t_f)] + \int_{t_o}^{t_f} \left\{ H[\mathbf{x}(t), \mathbf{u}(t), \boldsymbol{\lambda}(t)] - \boldsymbol{\lambda}^T(t) \frac{d\mathbf{x}(t)}{dt} \right\} dt$$

The optimal cost, J^* , is produced by the optimal histories of state, control, and Lagrange multiplier

$$\min_{\mathbf{u}(t)} J = J^* = \phi[\mathbf{x}^*(t_f)] + \int_{t_o}^{t_f} \left\{ H[\mathbf{x}^*(t), \mathbf{u}^*(t), \boldsymbol{\lambda}^*(t)] - \boldsymbol{\lambda}^{*T}(t) \frac{d\mathbf{x}^*(t)}{dt} \right\} dt$$

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Integration by Parts

- Scalar indefinite integral

$$\int u dv = uv - \int v du$$

- Vector definite integral

$$u = \boldsymbol{\lambda}^T(t)$$

$$dv = \dot{\mathbf{x}}(t)dt = d\mathbf{x}$$

$$\int_{t_0}^{t_f} \boldsymbol{\lambda}^T(t) \frac{d\mathbf{x}(t)}{dt} dt = \boldsymbol{\lambda}^T(t) \mathbf{x}(t) \Big|_{t_0}^{t_f} - \int_{t_0}^{t_f} \frac{d\boldsymbol{\lambda}^T(t)}{dt} \mathbf{x}(t) dt$$

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The Optimal Control Solution

- Along the optimal trajectory, the cost, J^* , should be **insensitive to small variations in control policy**
 - To first order,

$$\Delta J^* = \left\{ \left[\frac{\partial \phi}{\partial \mathbf{x}} - \boldsymbol{\lambda}^T \right] \right\} \Delta \mathbf{x}(\Delta \mathbf{u}) \Big|_{t=t_f} + \left[\boldsymbol{\lambda}^T \Delta \mathbf{x}(\Delta \mathbf{u}) \right] \Big|_{t=t_0}$$

$$+ \int_{t_0}^{t_f} \left\{ \frac{\partial H}{\partial \mathbf{u}} \Delta \mathbf{u} + \left[\frac{\partial H}{\partial \mathbf{x}} + \frac{d\boldsymbol{\lambda}^T}{dt} \right] \Delta \mathbf{x}(\Delta \mathbf{u}) \right\} dt = 0$$

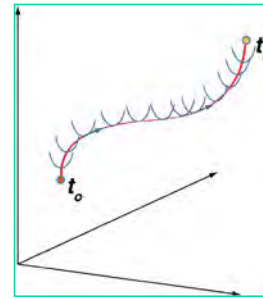
$\Delta \mathbf{x}(\Delta \mathbf{u})$ is arbitrary perturbation in state due to perturbation in control over the time interval, (t_0, t_f) .

Setting $\Delta J^* = 0$ leads to three necessary conditions for optimality

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Three Conditions for Optimality

Individual terms should remain zero for arbitrary variations in $\Delta \mathbf{x}(t)$ and $\Delta \mathbf{u}(t)$



Solution for Lagrange Multiplier

$$1) \left[\frac{\partial \phi}{\partial \mathbf{x}} - \boldsymbol{\lambda}^T \right]_{t=t_f} = \mathbf{0}$$

$$2) \left[\frac{\partial H}{\partial \mathbf{x}} + \frac{d\boldsymbol{\lambda}^T}{dt} \right] = \mathbf{0} \quad \text{in } (t_0, t_f)$$

$$\left. \begin{array}{l} \\ \\ \end{array} \right\} \Rightarrow \boldsymbol{\lambda}^*(t) \text{ in } (t_0, t_f)$$

Insensitivity to Control Variation

$$3) \frac{\partial H}{\partial \mathbf{u}} = \mathbf{0} \quad \text{in } (t_0, t_f)$$

$$\left. \begin{array}{l} \\ \\ \end{array} \right\} \Rightarrow \mathbf{u}^*(t) \text{ in } (t_0, t_f)$$

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Iterative Numerical Optimization Using Steepest-Descent

- Forward solution to find the state, $\mathbf{x}(t)$
- Backward solution to find the Lagrange multiplier, $\boldsymbol{\lambda}(t)$
- Steepest-descent adjustment of control history, $\mathbf{u}(t)$
- Iterate to find the optimal solution

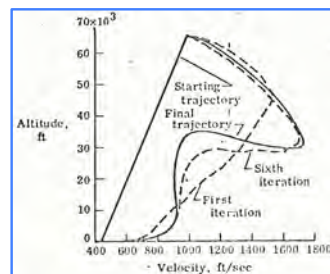
$$\dot{\mathbf{x}}_k(t) = \mathbf{f}[\mathbf{x}_k(t), \mathbf{u}_{k-1}(t)],$$

with

$\mathbf{x}(t_0)$ given

$\mathbf{u}_{k-1}(t)$ prescribed in (t_0, t_f)

$k =$ Iteration index



Use educated guess for $\mathbf{u}(t)$ on first iteration

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Numerical Optimization Using Steepest-Descent

- Forward solution to find the state, $\mathbf{x}(t)$
- **Backward solution to find the Lagrange multiplier, $\lambda(t)$**
- Steepest-descent adjustment of control history, $\mathbf{u}(t)$
- Iterate to optimal solution

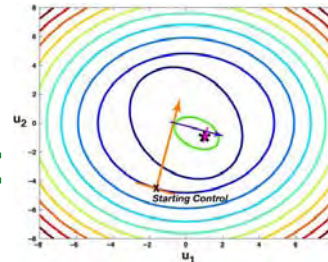
$$\lambda_k(t_f) = \left\{ \frac{\partial \phi[\mathbf{x}_k(t_f)]}{\partial \mathbf{x}} \right\}^T \left[\begin{array}{l} \text{Boundary condition at final time} \\ \text{Calculated from terminal value of the state} \end{array} \right]$$

$$\frac{d\lambda_k(t)}{dt} = - \left[\frac{\partial H(\mathbf{x}_k, \mathbf{u}_k, \lambda_k)}{\partial \mathbf{x}} \right]_k^T$$

$$= - \left[\frac{\partial L(\mathbf{x}, \mathbf{u})}{\partial \mathbf{x}} \Big|_{\substack{\mathbf{x}(t)=\mathbf{x}_k(t) \\ \mathbf{u}(t)=\mathbf{u}_{k-1}(t)}}} + \lambda_k^T(t) \frac{\partial \mathbf{f}(\mathbf{x}, \mathbf{u})}{\partial \mathbf{x}} \Big|_{\substack{\mathbf{x}(t)=\mathbf{x}_k(t) \\ \mathbf{u}(t)=\mathbf{u}_{k-1}(t)}}} \right]_k^T$$

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Numerical Optimization Using Steepest-Descent



- Forward solution to find the state, $\mathbf{x}(t)$
- Backward solution to find the Lagrange multiplier, $\lambda(t)$
- **Steepest-descent adjustment of control history, $\mathbf{u}(t)$**
- Iterate to optimal solution

$$\mathbf{u}_k(t) = \mathbf{u}_{k-1}(t) - \varepsilon \left[\frac{\partial H}{\partial \mathbf{u}} \right]_k^T$$

$$= \mathbf{u}_{k-1}(t) - \varepsilon \left[\frac{\partial L}{\partial \mathbf{u}} \Big|_{\substack{\mathbf{x}(t)=\mathbf{x}_k(t) \\ \mathbf{u}(t)=\mathbf{u}_{k-1}(t)}}} + \lambda_k^T(t) \frac{\partial \mathbf{f}}{\partial \mathbf{u}} \Big|_{\substack{\mathbf{x}(t)=\mathbf{x}_k(t) \\ \mathbf{u}(t)=\mathbf{u}_{k-1}(t)}}} \right]_k^T$$

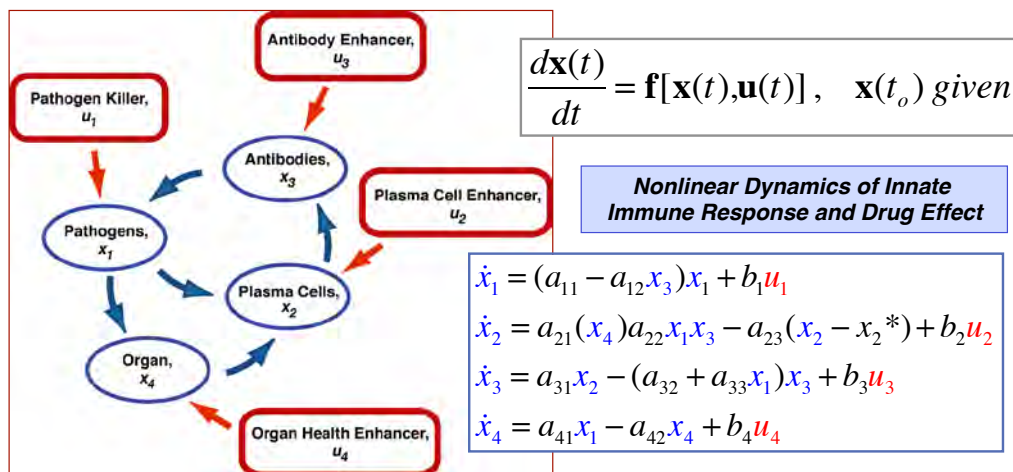
ε : Steepest-descent gain

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Optimal Treatment of an Infection

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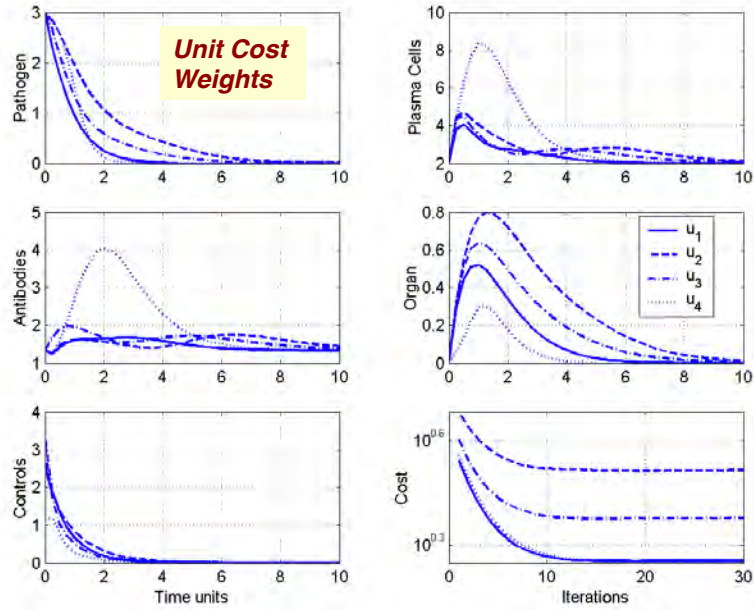
Dynamic Model for the Infection Treatment Problem



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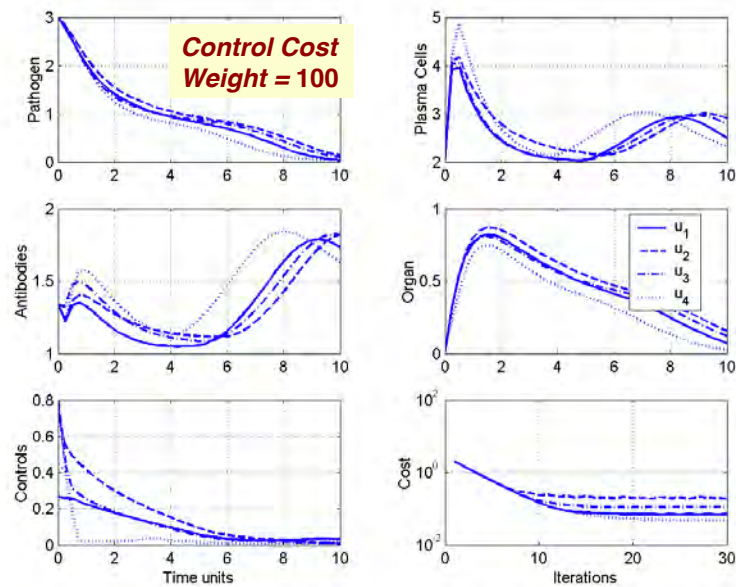


Optimal Treatment with Four Drugs (separately)



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Increased Cost of Drug Use



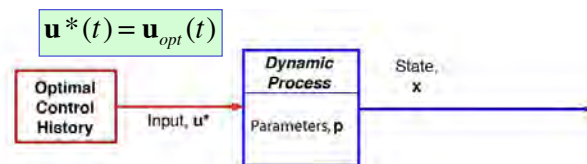
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Accounting for Uncertainty in Initial Condition

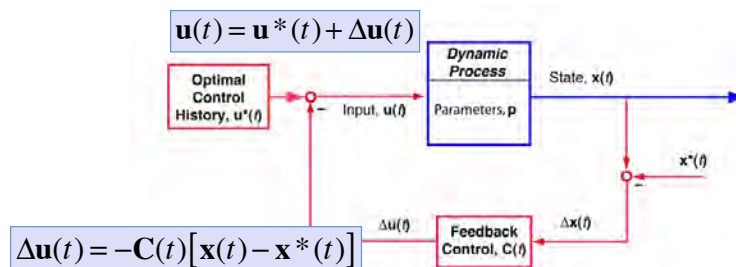
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Account for Uncertainty in Initial Condition and Unknown Disturbances

Nominal, Open-Loop Optimal Control



Neighboring-Optimal (*Feedback*) Control



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Neighboring-Optimal Control

Linearize dynamic equation

$$\begin{aligned} \dot{\mathbf{x}}(t) &= \dot{\mathbf{x}}^*(t) + \Delta\dot{\mathbf{x}}(t) \\ &= \mathbf{f}\{\mathbf{x}^*(t) + \Delta\mathbf{x}(t), [\mathbf{u}^*(t) + \Delta\mathbf{u}(t)]\} \\ &\approx \mathbf{f}[\mathbf{x}^*(t), \mathbf{u}^*(t)] + \mathbf{F}(t)\Delta\mathbf{x}(t) + \mathbf{G}(t)\Delta\mathbf{u}(t) \end{aligned}$$

- Nominal optimal control history
- Optimal perturbation control
- Sum the two for neighboring-optimal control

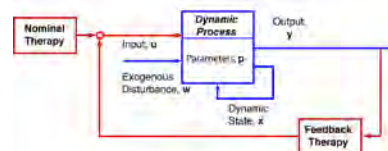
$$\mathbf{u}^*(t) = \mathbf{u}_{opt}(t)$$

$$\Delta\mathbf{u}(t) = -\mathbf{C}(t)[\mathbf{x}(t) - \mathbf{x}_{opt}(t)]$$

$$\mathbf{u}(t) = \mathbf{u}_{opt}(t) + \Delta\mathbf{u}(t)$$

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Optimal Feedback Gain, $\mathbf{C}(t)$



- Solution of Euler-Lagrange equations for
 - Linear dynamic system
 - Quadratic cost function
- leads to linear, time-varying (LTV) optimal feedback controller

$$\Delta\mathbf{u}^*(t) = -\mathbf{C}^*(t) \Delta\mathbf{x}(t)$$

where

$$\mathbf{C}^*(t) = \mathbf{R}^{-1}\mathbf{G}^T(t)\mathbf{S}(t)$$

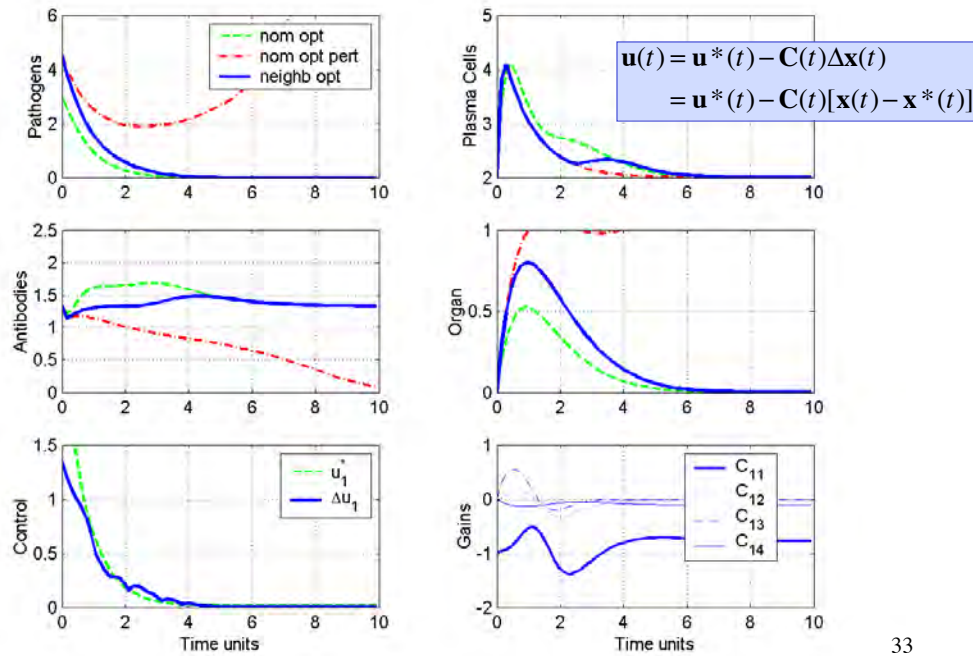
$$\dot{\mathbf{S}}(t) = -\mathbf{F}^T(t)\mathbf{S}(t) - \mathbf{S}(t)\mathbf{F}(t) + \mathbf{S}(t)\mathbf{G}(t)\mathbf{R}^{-1}\mathbf{G}^T(t)\mathbf{S}(t) - \mathbf{Q}$$

$$\mathbf{S}(t_f) = \mathbf{S}_f$$

Matrix Riccati equation (see Supplemental Material for derivation)

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50% Increased Initial Infection and Scalar Neighboring-Optimal Control (u_1)



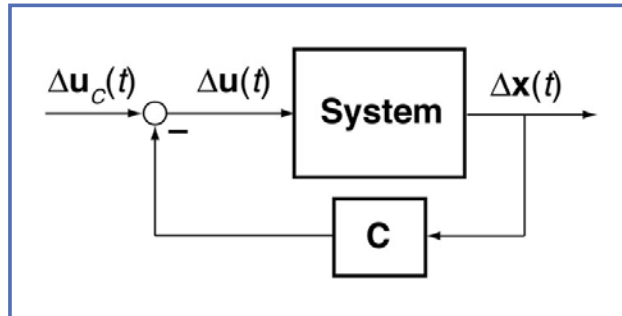
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*Optimal, Constant Gain
Feedback Control for Linear,
Time-Invariant Systems*

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Linear-Quadratic (LQ) Optimal Control Law

$$\Delta \dot{\mathbf{x}}(t) = \mathbf{F}(t) \Delta \mathbf{x}(t) + \mathbf{G}(t) \Delta \mathbf{u}(t)$$



$$\Delta \dot{\mathbf{x}}(t) = \mathbf{F}(t) \Delta \mathbf{x}(t) + \mathbf{G}(t) [\Delta \mathbf{u}_c(t) - \mathbf{C}^*(t) \Delta \mathbf{x}(t)]$$

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Optimal Control for Linear, Time-Invariant Dynamic Process

Original system is linear and time-invariant (LTI)

$$\Delta \dot{\mathbf{x}}(t) = \mathbf{F} \Delta \mathbf{x}(t) + \mathbf{G} \Delta \mathbf{u}(t), \quad \Delta \mathbf{x}(0) \text{ given}$$

Minimize quadratic cost function for $t_f \rightarrow \infty$
Terminal cost is of no concern

$$\min_u J = J^* = \lim_{t_f \rightarrow \infty} \frac{1}{2} \int_0^{t_f} [\Delta \mathbf{x}^{*T}(t) \mathbf{Q} \Delta \mathbf{x}^*(t) + \Delta \mathbf{u}^{*T}(t) \mathbf{R} \Delta \mathbf{u}^*(t)] dt$$

Dynamic constraint is the linear, time-invariant (LTI) plant

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Linear-Quadratic (LQ) Optimal Control for LTI System, and $t_f \rightarrow \infty$

$$\dot{\mathbf{S}}^*(0) \rightarrow \mathbf{0} \quad t_f \rightarrow \infty$$

Steady-state solution of the matrix Riccati equation = **Algebraic Riccati Equation**

$$-\mathbf{F}^T \mathbf{S}^* - \mathbf{S}^* \mathbf{F} + \mathbf{S}^* \mathbf{G} \mathbf{R}^{-1} \mathbf{G}^T \mathbf{S}^* - \mathbf{Q} = \mathbf{0}$$

Optimal control gain matrix

$$\mathbf{C}^* = \mathbf{R}^{-1} \mathbf{G}^T \mathbf{S}^*$$

$$(m \times n) = (m \times m)(m \times n)(n \times n)$$

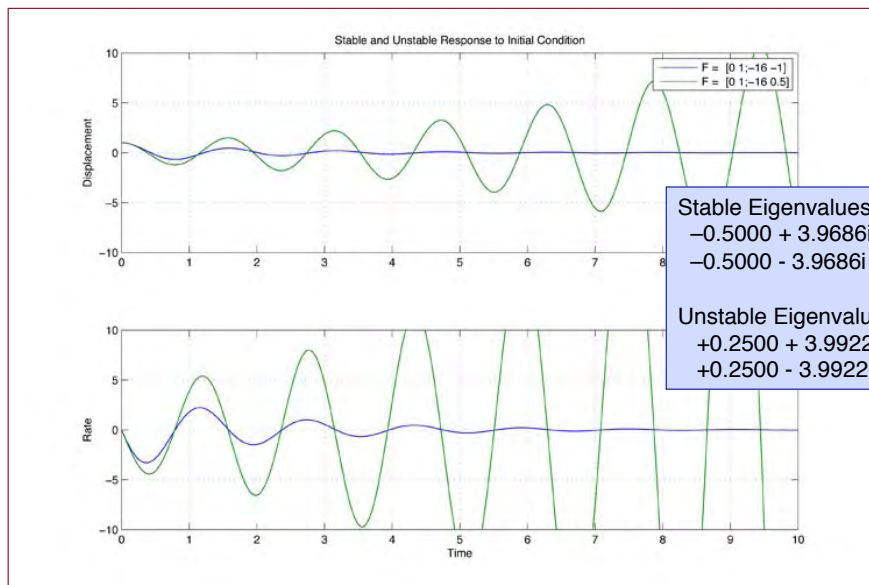
Optimal control

$$\Delta \mathbf{u}(t) = -\mathbf{C}^* \Delta \mathbf{x}(t)$$

MATLAB function: *lqr*

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Example: Open-Loop Stable and Unstable Second-Order System Response to Initial Condition



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Example: LQ Regulator Stabilizes Unstable System, $r = 1$ and 100

$$\min_{\Delta u} J = \min_{\Delta u} \left[\frac{1}{2} \int_0^{\infty} (\Delta x_1^2 + \Delta x_2^2 + r \Delta u^2) dt \right]$$

$$\Delta u(t) = - \begin{bmatrix} c_1 & c_2 \end{bmatrix} \begin{bmatrix} \Delta x_1(t) \\ \Delta x_2(t) \end{bmatrix} = -c_1 \Delta x_1(t) - c_2 \Delta x_2(t)$$

$r = 1$

Control Gain (\mathbf{C}^*) =
0.2620 1.0857

Riccati Matrix (\mathbf{S}^*) =
 2.2001 0.0291
 0.0291 0.1206

Closed-Loop Eigenvalues =
-6.4061
-2.8656

$r = 100$

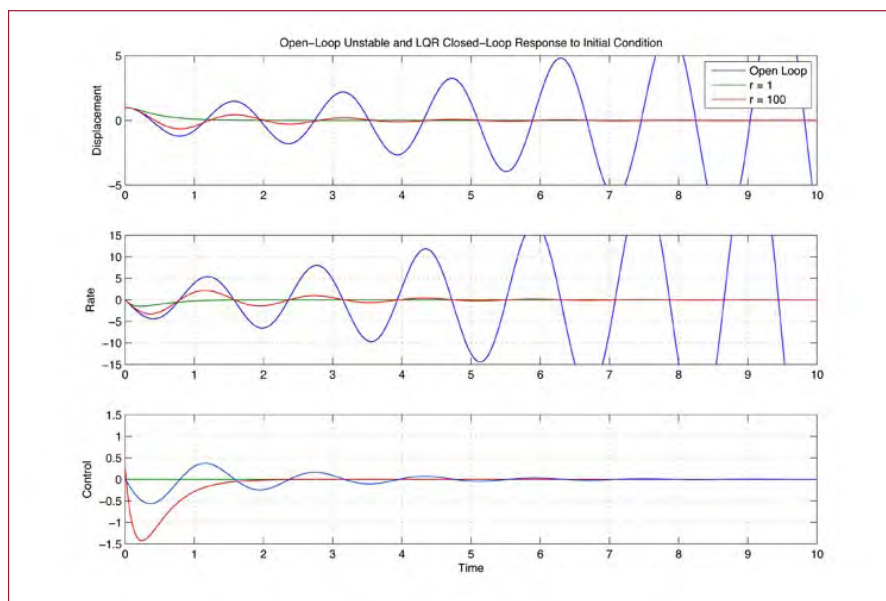
Control Gain (\mathbf{C}^*) =
0.0028 0.1726

Riccati Matrix (\mathbf{S}^*) =
 30.7261 0.0312
 0.0312 1.9183

Closed-Loop Eigenvalues =
-0.5269 + 3.9683j
-0.5269 - 3.9683j

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Example: LQ Regulator Stabilizes Unstable System, $r = 1$ and 100



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Requirements for Guaranteeing Stability of the LQ Regulator

$$\Delta \dot{\mathbf{x}}(t) = \mathbf{F}\Delta \mathbf{x}(t) + \mathbf{G}\Delta \mathbf{u}(t) = [\mathbf{F} - \mathbf{G}\mathbf{C}]\Delta \mathbf{x}(t)$$

Closed-loop system is stable whether or not open-loop system is stable if ...

$$\begin{array}{l} \mathbf{Q} > \mathbf{0} \\ \mathbf{R} > \mathbf{0} \end{array}$$

... and (\mathbf{F}, \mathbf{G}) is a controllable pair

$$\text{Rank} \begin{bmatrix} \mathbf{G} & \mathbf{F}\mathbf{G} & \dots & \mathbf{F}^{n-1}\mathbf{G} \end{bmatrix} = n$$

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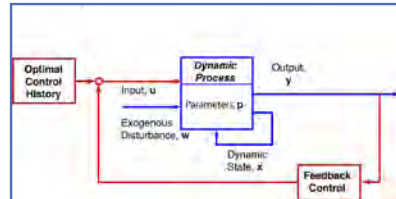
*Next Time:
Formal Logic, Algorithms,
and Incompleteness*

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Supplementary Material

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Linearized Model of Infection Dynamics



Locally linearized (time-varying) dynamic equation

$$\begin{bmatrix} \Delta \dot{x}_1 \\ \Delta \dot{x}_2 \\ \Delta \dot{x}_3 \\ \Delta \dot{x}_4 \end{bmatrix} = \begin{bmatrix} (a_{11} - a_{12}x_3^*) & 0 & -a_{12}x_1^* & 0 \\ a_{21}(x_4^*)a_{22}x_3^* & a_{23} & a_{21}(x_4^*)a_{22}x_1^* & \frac{\partial a_{21}}{\partial x_4} a_{22}x_1^* x_3^* \\ -a_{33}x_3^* & a_{31} & a_{31}x_1^* & 0 \\ a_{41} & 0 & 0 & -a_{42} \end{bmatrix} \begin{bmatrix} \Delta x_1 \\ \Delta x_2 \\ \Delta x_3 \\ \Delta x_4 \end{bmatrix} + \begin{bmatrix} b_1 & 0 & 0 & 0 \\ 0 & b_2 & 0 & 0 \\ 0 & 0 & b_3 & 0 \\ 0 & 0 & 0 & b_4 \end{bmatrix} \begin{bmatrix} \Delta u_1 \\ \Delta u_2 \\ \Delta u_3 \\ \Delta u_4 \end{bmatrix} + \begin{bmatrix} \Delta w_1 \\ \Delta w_2 \\ \Delta w_3 \\ \Delta w_4 \end{bmatrix}$$

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Expand Optimal Control Function

- Expand optimized cost function to second degree

$$J\left\{\left[\mathbf{x}^*(t_o) + \Delta\mathbf{x}(t_o)\right], \left[\mathbf{x}^*(t_f) + \Delta\mathbf{x}(t_f)\right]\right\} \simeq$$

$$J^*\left[\mathbf{x}^*(t_o), \mathbf{x}^*(t_f)\right] + \cancel{\Delta J\left[\Delta\mathbf{x}(t_o), \Delta\mathbf{x}(t_f)\right]} + \Delta^2 J\left[\Delta\mathbf{x}(t_o), \Delta\mathbf{x}(t_f)\right]$$

$$= J^*\left[\mathbf{x}^*(t_o), \mathbf{x}^*(t_f)\right] + \Delta^2 J\left[\Delta\mathbf{x}(t_o), \Delta\mathbf{x}(t_f)\right]$$

as **First Variation**, $\Delta J\left[\Delta\mathbf{x}(t_o), \Delta\mathbf{x}(t_f)\right] = 0$

- Nominal optimized cost, plus nonlinear dynamic constraint

$$J^*\left[\mathbf{x}^*(t_o), \mathbf{x}^*(t_f)\right] = \phi\left[\mathbf{x}^*(t_f)\right] + \int_{t_o}^{t_f} L\left[\mathbf{x}^*(t), \mathbf{u}^*(t)\right] dt$$

subject to nonlinear dynamic equation

$$\dot{\mathbf{x}}^*(t) = \mathbf{f}\left[\mathbf{x}^*(t), \mathbf{u}^*(t)\right], \mathbf{x}(t_o) = \mathbf{x}_o$$

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Second Variation of the Cost Function

Objective: Minimize second-variational cost subject to linear dynamic constraint

$$\min_{\Delta\mathbf{u}} \Delta^2 J = \frac{1}{2} \Delta\mathbf{x}^T(t_f) \phi_{\mathbf{xx}}(t_f) \Delta\mathbf{x}(t_f) + \frac{1}{2} \int_{t_o}^{t_f} \begin{bmatrix} \Delta\mathbf{x}^T(t) & \Delta\mathbf{u}^T(t) \end{bmatrix} \begin{bmatrix} L_{\mathbf{xx}}(t) & L_{\mathbf{xu}}(t) \\ L_{\mathbf{ux}}(t) & L_{\mathbf{uu}}(t) \end{bmatrix} \begin{bmatrix} \Delta\mathbf{x}(t) \\ \Delta\mathbf{u}(t) \end{bmatrix} dt$$

subject to perturbation dynamics

$$\Delta\dot{\mathbf{x}}(t) = \mathbf{F}(t)\Delta\mathbf{x}(t) + \mathbf{G}(t)\Delta\mathbf{u}(t), \Delta\mathbf{x}(t_o) = \Delta\mathbf{x}_o$$

Cost weighting matrices expressed as

$$\mathbf{S}(t_f) \triangleq \phi_{\mathbf{xx}}(t_f) = \frac{\partial^2 \phi}{\partial \mathbf{x}^2}(t_f)$$

$$\begin{bmatrix} \mathbf{Q}(t) & \mathbf{M}(t) \\ \mathbf{M}^T(t) & \mathbf{R}(t) \end{bmatrix} \triangleq \begin{bmatrix} L_{\mathbf{xx}}(t) & L_{\mathbf{xu}}(t) \\ L_{\mathbf{ux}}(t) & L_{\mathbf{uu}}(t) \end{bmatrix}$$

$$\dim[\mathbf{S}(t_f)] = \dim[\mathbf{Q}(t)] = n \times n$$

$$\dim[\mathbf{R}(t)] = m \times m$$

$$\dim[\mathbf{M}(t)] = n \times m$$

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Second Variational Hamiltonian

Variational cost function

$$\Delta^2 J = \frac{1}{2} \Delta \mathbf{x}^T(t_f) \mathbf{S}(t_f) \Delta \mathbf{x}(t_f) + \frac{1}{2} \left\{ \int_{t_0}^{t_f} \begin{bmatrix} \Delta \mathbf{x}^T(t) & \Delta \mathbf{u}^T(t) \end{bmatrix} \begin{bmatrix} \mathbf{Q}(t) & \mathbf{M}(t) \\ \mathbf{M}^T(t) & \mathbf{R}(t) \end{bmatrix} \begin{bmatrix} \Delta \mathbf{x}(t) \\ \Delta \mathbf{u}(t) \end{bmatrix} dt \right\}$$

$$= \frac{1}{2} \Delta \mathbf{x}^T(t_f) \mathbf{S}(t_f) \Delta \mathbf{x}(t_f) + \frac{1}{2} \left\{ \int_{t_0}^{t_f} \left[\Delta \mathbf{x}^T(t) \mathbf{Q}(t) \Delta \mathbf{x}(t) + 2 \Delta \mathbf{x}^T(t) \mathbf{M}(t) \Delta \mathbf{u}(t) + \Delta \mathbf{u}^T(t) \mathbf{R}(t) \Delta \mathbf{u}(t) \right] dt \right\}$$

Variational Lagrangian plus adjoined dynamic constraint

$$\begin{aligned} H[\Delta \mathbf{x}(t), \Delta \mathbf{u}(t), \Delta \boldsymbol{\lambda}(t)] &= L[\Delta \mathbf{x}(t), \Delta \mathbf{u}(t)] + \Delta \boldsymbol{\lambda}^T(t) \mathbf{f}[\Delta \mathbf{x}(t), \Delta \mathbf{u}(t)] \\ &= \frac{1}{2} \left[\Delta \mathbf{x}^T(t) \mathbf{Q}(t) \Delta \mathbf{x}(t) + 2 \Delta \mathbf{x}^T(t) \mathbf{M}(t) \Delta \mathbf{u}(t) + \Delta \mathbf{u}^T(t) \mathbf{R}(t) \Delta \mathbf{u}(t) \right] \\ &\quad + \Delta \boldsymbol{\lambda}^T(t) [\mathbf{F}(t) \Delta \mathbf{x}(t) + \mathbf{G}(t) \Delta \mathbf{u}(t)] \end{aligned}$$

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Second Variational Euler-Lagrange Equations

$$\begin{aligned} H &= \frac{1}{2} \left[\Delta \mathbf{x}^T(t) \mathbf{Q}(t) \Delta \mathbf{x}(t) + 2 \Delta \mathbf{x}^T(t) \mathbf{M}(t) \Delta \mathbf{u}(t) + \Delta \mathbf{u}^T(t) \mathbf{R}(t) \Delta \mathbf{u}(t) \right] \\ &\quad + \Delta \boldsymbol{\lambda}^T(t) [\mathbf{F}(t) \Delta \mathbf{x}(t) + \mathbf{G}(t) \Delta \mathbf{u}(t)] \end{aligned}$$

Terminal condition, solution for adjoint vector, and optimality condition

$$\Delta \boldsymbol{\lambda}(t_f) = \phi_{\mathbf{xx}}(t_f) \Delta \mathbf{x}(t_f) = \mathbf{S}(t_f) \Delta \mathbf{x}(t_f)$$

$$\Delta \dot{\boldsymbol{\lambda}}(t) = - \left\{ \frac{\partial H[\Delta \mathbf{x}(t), \Delta \mathbf{u}(t), \Delta \boldsymbol{\lambda}(t)]}{\partial \mathbf{x}} \right\}^T = -\mathbf{Q}(t) \Delta \mathbf{x}(t) - \mathbf{M}(t) \Delta \mathbf{u}(t) - \mathbf{F}^T(t) \Delta \boldsymbol{\lambda}(t)$$

$$\left\{ \frac{\partial H[\Delta \mathbf{x}(t), \Delta \mathbf{u}(t), \Delta \boldsymbol{\lambda}(t)]}{\partial \mathbf{u}} \right\}^T = \mathbf{M}^T(t) \Delta \mathbf{x}(t) + \mathbf{R}(t) \Delta \mathbf{u}(t) - \mathbf{G}^T(t) \Delta \boldsymbol{\lambda}(t) = \mathbf{0}$$

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Use Control Law to Solve the Two-Point Boundary-Value Problem

From $H_u = 0$ $\Delta \mathbf{u}(t) = -\mathbf{R}^{-1}(t) [\mathbf{M}^T(t) \Delta \mathbf{x}(t) + \mathbf{G}^T(t) \Delta \boldsymbol{\lambda}(t)]$

Substitute for control in system and adjoint equations
Two-point boundary-value problem

$$\begin{bmatrix} \Delta \dot{\mathbf{x}}(t) \\ \Delta \dot{\boldsymbol{\lambda}}(t) \end{bmatrix} = \begin{bmatrix} [\mathbf{F}(t) - \mathbf{G}(t)\mathbf{R}^{-1}(t)\mathbf{M}^T(t)] & -\mathbf{G}(t)\mathbf{R}^{-1}(t)\mathbf{G}^T(t) \\ [-\mathbf{Q}(t) + \mathbf{M}(t)\mathbf{R}^{-1}(t)\mathbf{M}^T(t)] & -[\mathbf{F}(t) - \mathbf{G}(t)\mathbf{R}^{-1}(t)\mathbf{M}^T(t)]^T \end{bmatrix} \begin{bmatrix} \Delta \mathbf{x}(t) \\ \Delta \boldsymbol{\lambda}(t) \end{bmatrix}$$

Boundary conditions at initial and final times

$$\begin{bmatrix} \Delta \mathbf{x}(t_o) \\ \Delta \boldsymbol{\lambda}(t_f) \end{bmatrix} = \begin{bmatrix} \Delta \mathbf{x}_o \\ \mathbf{S}_f \Delta \mathbf{x}_f \end{bmatrix} \quad \begin{array}{l} \text{Perturbation state vector} \\ \text{Perturbation adjoint vector} \end{array}$$

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Use Control Law to Solve the Two-Point Boundary-Value Problem

Suppose that the terminal adjoint relationship applies
over the entire interval

$$\Delta \boldsymbol{\lambda}(t) = \mathbf{S}(t) \Delta \mathbf{x}(t)$$

Feedback control law becomes

$$\begin{aligned} \Delta \mathbf{u}(t) &= -\mathbf{R}^{-1}(t) [\mathbf{M}^T(t) \Delta \mathbf{x}(t) + \mathbf{G}^T(t) \mathbf{S}(t) \Delta \mathbf{x}(t)] \\ &= -\mathbf{R}^{-1}(t) [\mathbf{M}^T(t) + \mathbf{G}^T(t) \mathbf{S}(t)] \Delta \mathbf{x}(t) \\ &\triangleq -\mathbf{C}(t) \Delta \mathbf{x}(t) \end{aligned} \quad \dim(\mathbf{C}) = m \times n$$

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Linear-Quadratic (LQ) Optimal Control Gain Matrix

$$\Delta \mathbf{u}(t) = -\mathbf{C}(t)\Delta \mathbf{x}(t)$$

- Optimal feedback gain matrix

$$\mathbf{C}(t) = \mathbf{R}^{-1}(t) \left[\mathbf{G}^T(t)\mathbf{S}(t) + \mathbf{M}^T(t) \right]$$

- Properties of feedback gain matrix
 - Full state feedback ($m \times n$)
 - Time-varying matrix
 - \mathbf{R} , \mathbf{G} , and \mathbf{M} given
 - Control weighting matrix, \mathbf{R}
 - State-control weighting matrix, \mathbf{M}
 - Control effect matrix, \mathbf{G}
 - $\mathbf{S}(t)$ remains to be determined

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Solution for the Adjoining Matrix, $\mathbf{S}(t)$

Time-derivative of adjoint vector

$$\Delta \dot{\boldsymbol{\lambda}}(t) = \dot{\mathbf{S}}(t)\Delta \mathbf{x}(t) + \mathbf{S}(t)\Delta \dot{\mathbf{x}}(t)$$

Rearrange

$$\dot{\mathbf{S}}(t)\Delta \mathbf{x}(t) = \Delta \dot{\boldsymbol{\lambda}}(t) - \mathbf{S}(t)\Delta \dot{\mathbf{x}}(t)$$

Recall

$$\begin{bmatrix} \Delta \dot{\mathbf{x}}(t) \\ \Delta \dot{\boldsymbol{\lambda}}(t) \end{bmatrix} = \begin{bmatrix} [\mathbf{F}(t) - \mathbf{G}(t)\mathbf{R}^{-1}(t)\mathbf{M}^T(t)] & -\mathbf{G}(t)\mathbf{R}^{-1}(t)\mathbf{G}^T(t) \\ [-\mathbf{Q}(t) + \mathbf{M}(t)\mathbf{R}^{-1}(t)\mathbf{M}^T(t)] & -[\mathbf{F}(t) - \mathbf{G}(t)\mathbf{R}^{-1}(t)\mathbf{M}^T(t)]^T \end{bmatrix} \begin{bmatrix} \Delta \mathbf{x}(t) \\ \Delta \boldsymbol{\lambda}(t) \end{bmatrix}$$

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Solution for the Adjoining Matrix, $\mathbf{S}(t)$

Substitute

$$\dot{\mathbf{S}}(t)\Delta\mathbf{x}(t) = \left[-\mathbf{Q}(t) + \mathbf{M}(t)\mathbf{R}^{-1}(t)\mathbf{M}^T(t) \right] \Delta\mathbf{x}(t) - \left[\mathbf{F}(t) - \mathbf{G}(t)\mathbf{R}^{-1}(t)\mathbf{M}^T(t) \right]^T \Delta\boldsymbol{\lambda}(t) - \mathbf{S}(t) \left\{ \left[\mathbf{F}(t) - \mathbf{G}(t)\mathbf{R}^{-1}(t)\mathbf{M}^T(t) \right] \Delta\mathbf{x}(t) - \mathbf{G}(t)\mathbf{R}^{-1}(t)\mathbf{G}^T(t)\Delta\boldsymbol{\lambda}(t) \right\}$$

Substitute

$$\Delta\boldsymbol{\lambda}(t) = \mathbf{S}(t)\Delta\mathbf{x}(t)$$

$$\dot{\mathbf{S}}(t)\underline{\Delta\mathbf{x}(t)} = \left[-\mathbf{Q}(t) + \mathbf{M}(t)\mathbf{R}^{-1}(t)\mathbf{M}^T(t) \right] \underline{\Delta\mathbf{x}(t)} - \left[\mathbf{F}(t) - \mathbf{G}(t)\mathbf{R}^{-1}(t)\mathbf{M}^T(t) \right]^T \mathbf{S}(t)\underline{\Delta\mathbf{x}(t)} - \mathbf{S}(t) \left\{ \left[\mathbf{F}(t) - \mathbf{G}(t)\mathbf{R}^{-1}(t)\mathbf{M}^T(t) \right] \underline{\Delta\mathbf{x}(t)} - \mathbf{G}(t)\mathbf{R}^{-1}(t)\mathbf{G}^T(t)\mathbf{S}(t)\underline{\Delta\mathbf{x}(t)} \right\}$$

$\Delta\mathbf{x}(t)$ can be eliminated

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Matrix Riccati Equation for $\mathbf{S}(t)$

The result is a nonlinear, ordinary differential equation for $\mathbf{S}(t)$, with terminal boundary conditions

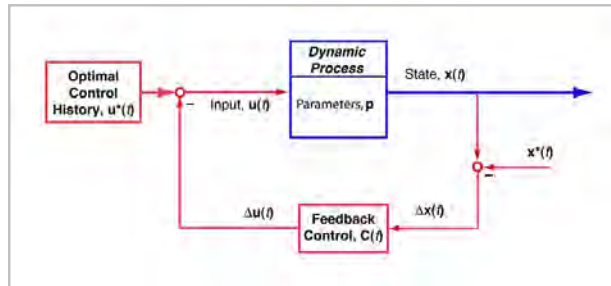
$$\dot{\mathbf{S}}(t) = \left[-\mathbf{Q}(t) + \mathbf{M}(t)\mathbf{R}^{-1}(t)\mathbf{M}^T(t) \right] - \left[\mathbf{F}(t) - \mathbf{G}(t)\mathbf{R}^{-1}(t)\mathbf{M}^T(t) \right]^T \mathbf{S}(t) - \mathbf{S}(t) \left[\mathbf{F}(t) - \mathbf{G}(t)\mathbf{R}^{-1}(t)\mathbf{M}^T(t) \right] + \mathbf{S}(t)\mathbf{G}(t)\mathbf{R}^{-1}(t)\mathbf{G}^T(t)\mathbf{S}(t)$$

$$\mathbf{S}(t_f) = \phi_{\mathbf{xx}}(t_f)$$

- **Characteristics of the Riccati matrix, $\mathbf{S}(t)$**
 - $\mathbf{S}(t)$ is symmetric, $n \times n$, and typically positive semi-definite
 - Matrix Riccati equation is symmetric
 - Therefore, $\mathbf{S}(t)$ is symmetric and positive semi-definite throughout
- Once $\mathbf{S}(t)$ has been determined, optimal feedback control gain matrix, $\mathbf{C}(t)$ can be calculated

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Neighboring-Optimal (LQ) Feedback Control Law



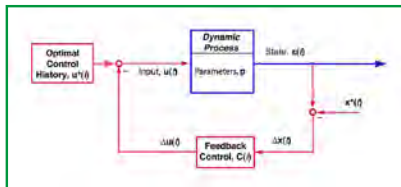
Full state is fed back to all available controls

$$\Delta \mathbf{u}(t) = -\mathbf{R}^{-1}(t) [\mathbf{M}^T(t) + \mathbf{G}^T(t)\mathbf{S}(t)] \Delta \mathbf{x}(t) = -\mathbf{C}(t) \Delta \mathbf{x}(t)$$

Optimal control history plus feedback correction

$$\mathbf{u}(t) = \mathbf{u}^*(t) - \mathbf{C}(t) \Delta \mathbf{x}(t) = \mathbf{u}^*(t) - \mathbf{C}(t) [\mathbf{x}(t) - \mathbf{x}^*(t)]$$

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Nonlinear System with Neighboring-Optimal Feedback Control

Nonlinear dynamic system

$$\dot{\mathbf{x}}(t) = \mathbf{f}[\mathbf{x}(t), \mathbf{u}(t)]$$

Neighboring-optimal control law

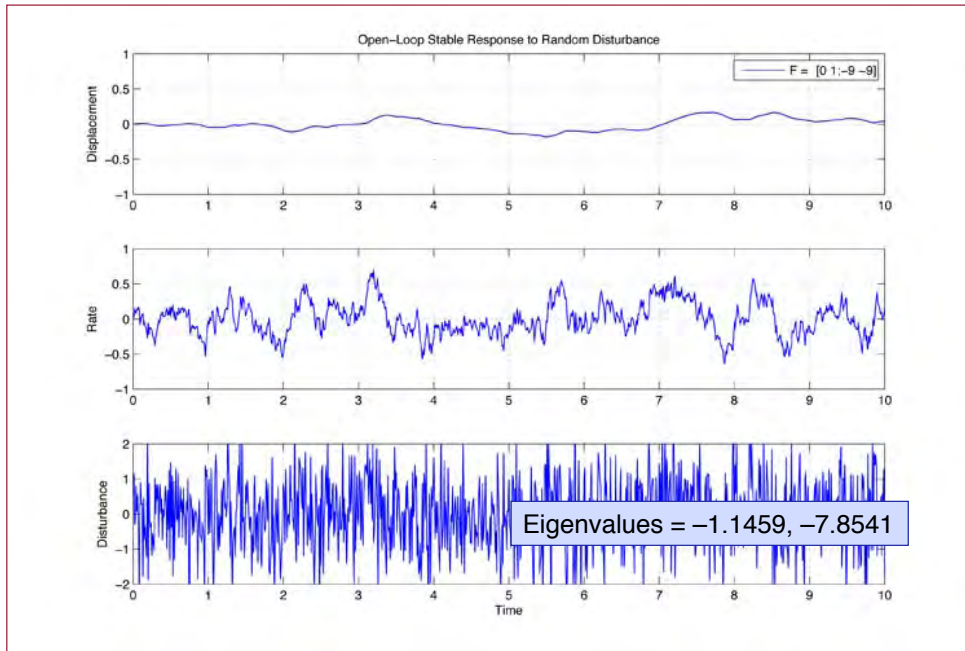
$$\mathbf{u}(t) = \mathbf{u}^*(t) - \mathbf{C}(t) \Delta \mathbf{x}(t) = \mathbf{u}^*(t) - \mathbf{C}(t) [\mathbf{x}(t) - \mathbf{x}^*(t)]$$

Nonlinear dynamic system with neighboring-optimal feedback control

$$\dot{\mathbf{x}}(t) = \mathbf{f} \left\{ \mathbf{x}(t), [\mathbf{u}^*(t) - \mathbf{C}(t) [\mathbf{x}(t) - \mathbf{x}^*(t)]] \right\}$$

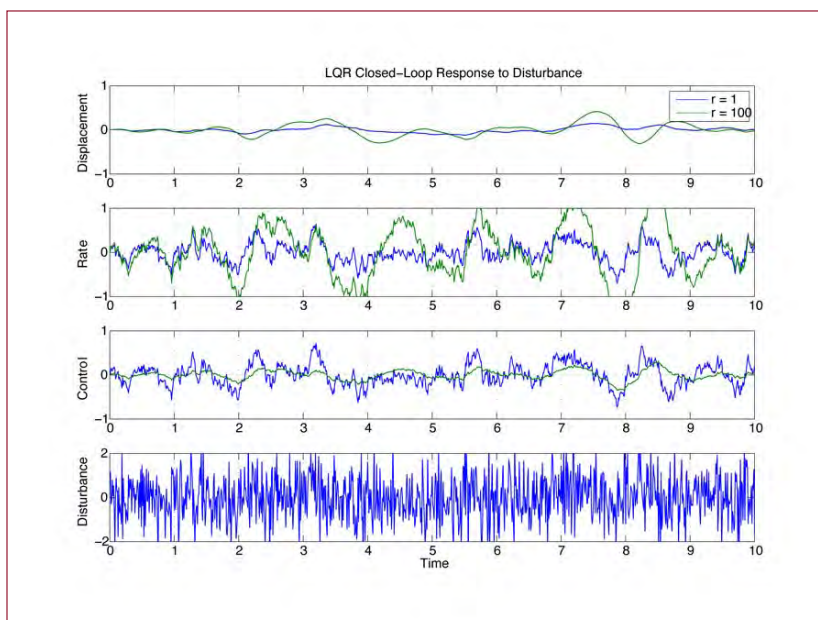
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Example: Response of Stable Second-Order System to Random Disturbance



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Example: Disturbance Response of Unstable System with LQ Regulators, $r = 1$ and 100



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Equilibrium Response to a Command Input

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Steady-State Response to Commands

$$\Delta \dot{\mathbf{x}}(t) = \mathbf{F}\Delta \mathbf{x}(t) + \mathbf{G}\Delta \mathbf{u}(t) + \mathbf{L}\Delta \mathbf{w}(t),$$

$\Delta \mathbf{x}(t_0)$ given

$$\Delta \mathbf{y}(t) = \mathbf{H}_x \Delta \mathbf{x}(t) + \mathbf{H}_u \Delta \mathbf{u}(t) + \mathbf{H}_w \Delta \mathbf{w}(t)$$

State equilibrium with constant inputs ...

$$\mathbf{0} = \mathbf{F}\Delta \mathbf{x}^* + \mathbf{G}\Delta \mathbf{u}^* + \mathbf{L}\Delta \mathbf{w}^*$$

$$\Delta \mathbf{x}^* = -\mathbf{F}^{-1}(\mathbf{G}\Delta \mathbf{u}^* + \mathbf{L}\Delta \mathbf{w}^*)$$

... constrained by requirement to satisfy command input

$$\Delta \mathbf{y}^* = \mathbf{H}_x \Delta \mathbf{x}^* + \mathbf{H}_u \Delta \mathbf{u}^* + \mathbf{H}_w \Delta \mathbf{w}^*$$

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Steady-State Response to Commands

Equilibrium that satisfies a commanded input, Δy_C

$$\begin{aligned} \mathbf{0} &= \mathbf{F}\Delta\mathbf{x}^* + \mathbf{G}\Delta\mathbf{u}^* + \mathbf{L}\Delta\mathbf{w}^* \\ \Delta\mathbf{y}^* &= \mathbf{H}_x\Delta\mathbf{x}^* + \mathbf{H}_u\Delta\mathbf{u}^* + \mathbf{H}_w\Delta\mathbf{w}^* \end{aligned}$$

Combine equations

$$\begin{bmatrix} \mathbf{0} \\ \Delta\mathbf{y}_C \end{bmatrix} = \begin{bmatrix} \mathbf{F} & \mathbf{G} \\ \mathbf{H}_x & \mathbf{H}_u \end{bmatrix} \begin{bmatrix} \Delta\mathbf{x}^* \\ \Delta\mathbf{u}^* \end{bmatrix} + \begin{bmatrix} \mathbf{L} \\ \mathbf{H}_w \end{bmatrix} \Delta\mathbf{w}^*$$

$(n+r) \times (n+m)$

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Equilibrium Values of State and Control to Satisfy Commanded Input

Equilibrium that satisfies a commanded input, Δy_C

$$\begin{aligned} \begin{bmatrix} \Delta\mathbf{x}^* \\ \Delta\mathbf{u}^* \end{bmatrix} &= \begin{bmatrix} \mathbf{F} & \mathbf{G} \\ \mathbf{H}_x & \mathbf{H}_u \end{bmatrix}^{-1} \begin{bmatrix} -\mathbf{L}\Delta\mathbf{w}^* \\ \Delta\mathbf{y}_C - \mathbf{H}_w\Delta\mathbf{w}^* \end{bmatrix} \\ &\triangleq \mathbf{A}^{-1} \begin{bmatrix} -\mathbf{L}\Delta\mathbf{w}^* \\ \Delta\mathbf{y}_C - \mathbf{H}_w\Delta\mathbf{w}^* \end{bmatrix} \end{aligned}$$

A must be square for inverse to exist

Then, number of commands = number of controls

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Inverse of the Matrix

$$\begin{bmatrix} \mathbf{F} & \mathbf{G} \\ \mathbf{H}_x & \mathbf{H}_u \end{bmatrix}^{-1} \triangleq \mathbf{A}^{-1} = \mathbf{B} = \begin{bmatrix} \mathbf{B}_{11} & \mathbf{B}_{12} \\ \mathbf{B}_{21} & \mathbf{B}_{22} \end{bmatrix}$$

$$\begin{bmatrix} \Delta \mathbf{x}^* \\ \Delta \mathbf{u}^* \end{bmatrix} = \begin{bmatrix} \mathbf{B}_{11} & \mathbf{B}_{12} \\ \mathbf{B}_{21} & \mathbf{B}_{22} \end{bmatrix} \begin{bmatrix} -\mathbf{L}\Delta \mathbf{w}^* \\ \Delta \mathbf{y}_C - \mathbf{H}_w \Delta \mathbf{w}^* \end{bmatrix}$$

\mathbf{B}_{ij} have same dimensions as equivalent blocks of \mathbf{A}
Equilibrium that satisfies a commanded input, $\Delta \mathbf{y}_C$

$$\begin{aligned} \Delta \mathbf{x}^* &= -\mathbf{B}_{11} \mathbf{L} \Delta \mathbf{w}^* + \mathbf{B}_{12} (\Delta \mathbf{y}_C - \mathbf{H}_w \Delta \mathbf{w}^*) \\ \Delta \mathbf{u}^* &= -\mathbf{B}_{21} \mathbf{L} \Delta \mathbf{w}^* + \mathbf{B}_{22} (\Delta \mathbf{y}_C - \mathbf{H}_w \Delta \mathbf{w}^*) \end{aligned}$$

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Elements of Matrix Inverse and Solutions for Open-Loop Equilibrium

Substitution and elimination (*see Supplement*)

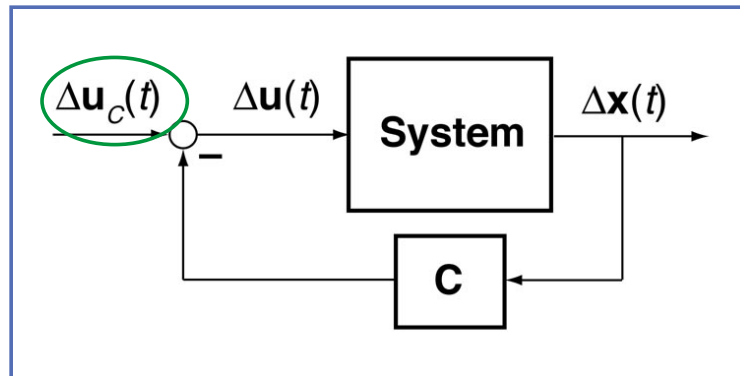
$$\begin{bmatrix} \mathbf{B}_{11} & \mathbf{B}_{12} \\ \mathbf{B}_{21} & \mathbf{B}_{22} \end{bmatrix} = \begin{bmatrix} \mathbf{F}^{-1}(-\mathbf{G}\mathbf{B}_{21} + \mathbf{I}_n) & -\mathbf{F}^{-1}\mathbf{G}\mathbf{B}_{22} \\ -\mathbf{B}_{22}\mathbf{H}_x\mathbf{F}^{-1} & (-\mathbf{H}_x\mathbf{F}^{-1}\mathbf{G} + \mathbf{H}_u)^{-1} \end{bmatrix}$$

Solve for \mathbf{B}_{22} , then \mathbf{B}_{12} and \mathbf{B}_{21} , then \mathbf{B}_{11}

$$\begin{aligned} \Delta \mathbf{x}^* &= \mathbf{B}_{12} \Delta \mathbf{y}_C - (\mathbf{B}_{11} \mathbf{L} + \mathbf{B}_{12} \mathbf{H}_w) \Delta \mathbf{w}^* \\ \Delta \mathbf{u}^* &= \mathbf{B}_{22} \Delta \mathbf{y}_C - (\mathbf{B}_{21} \mathbf{L} + \mathbf{B}_{22} \mathbf{H}_w) \Delta \mathbf{w}^* \end{aligned}$$

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LQ Regulator with Command Input (Proportional Control Law)



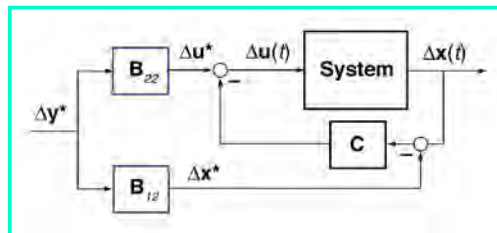
$$\Delta \mathbf{u}(t) = \Delta \mathbf{u}_c(t) - \mathbf{C} \Delta \mathbf{x}(t)$$

How do we define $\Delta \mathbf{u}_c(t)$?

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Non-Zero Steady-State Regulation with LQ Regulator

Command input provides equivalent state and control values for the LQ regulator



Control law with command input

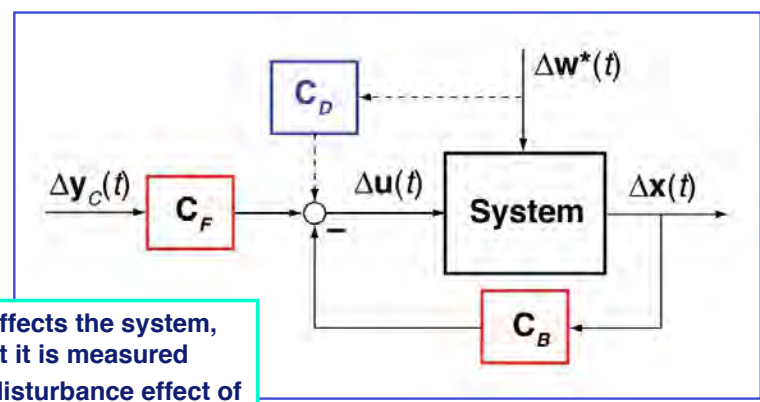
$$\begin{aligned} \Delta \mathbf{u}(t) &= \Delta \mathbf{u}^*(t) - \mathbf{C} [\Delta \mathbf{x}(t) - \Delta \mathbf{x}^*(t)] \\ &= \mathbf{B}_{22} \Delta \mathbf{y}^* - \mathbf{C} [\Delta \mathbf{x}(t) - \mathbf{B}_{12} \Delta \mathbf{y}^*] \\ &= (\mathbf{B}_{22} + \mathbf{C} \mathbf{B}_{12}) \Delta \mathbf{y}^* - \mathbf{C} \Delta \mathbf{x}(t) \end{aligned}$$

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LQ Regulator with Forward Gain Matrix

$$\begin{aligned} \Delta \mathbf{u}(t) &= \Delta \mathbf{u}^*(t) - \mathbf{C} [\Delta \mathbf{x}(t) - \Delta \mathbf{x}^*(t)] \\ &= \mathbf{C}_F \Delta \mathbf{y}^* - \mathbf{C}_B \Delta \mathbf{x}(t) \end{aligned}$$

$$\begin{aligned} \mathbf{C}_F &\triangleq \mathbf{B}_{22} + \mathbf{C} \mathbf{B}_{12} \\ \mathbf{C}_B &\triangleq \mathbf{C} \end{aligned}$$



- Disturbance affects the system, whether or not it is measured
- If measured, disturbance effect of can be countered by \mathbf{C}_D (analogous to \mathbf{C}_F)