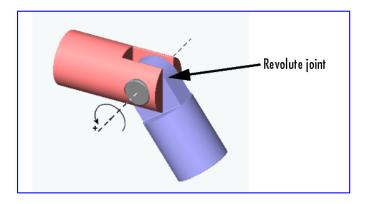
Articulated Robots

Robert Stengel Robotics and Intelligent Systems MAE 345, Princeton University, 2017



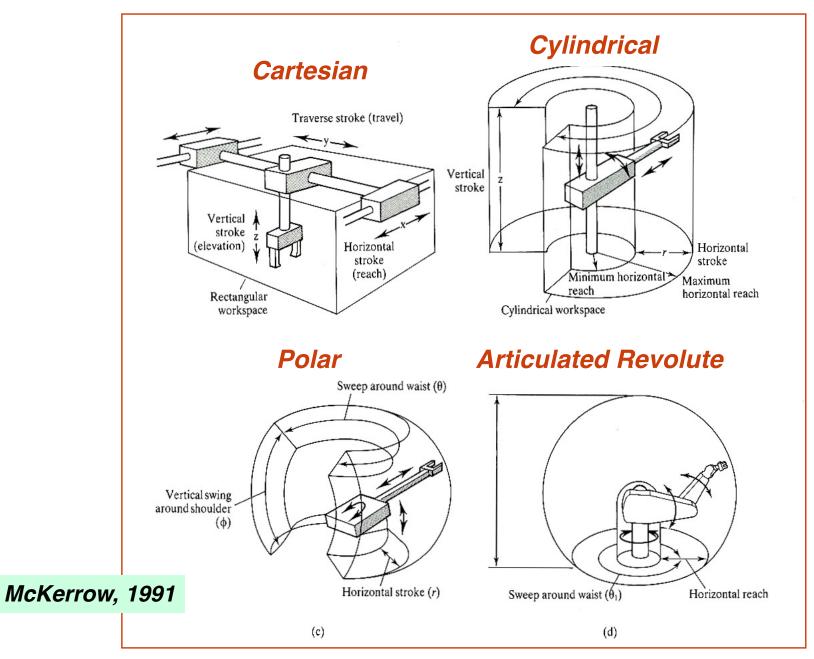




- Robot configurations
- Joints and links
- Joint-link-joint transformations
 - Denavit-Hartenberg representation

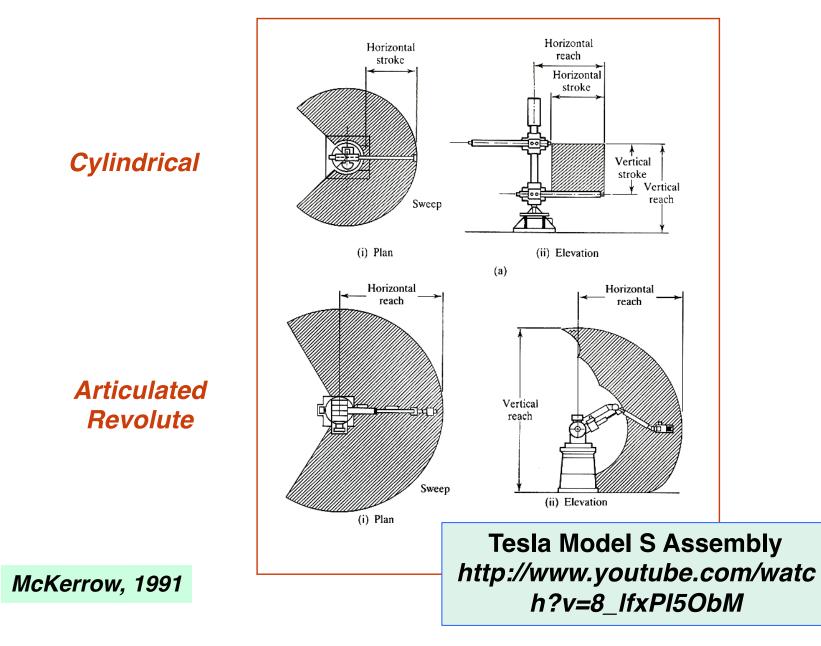
Copyright 2017 by Robert Stengel. All rights reserved. For educational use only. http://www.princeton.edu/~stengel/MAE345.html

Assembly Robot Configurations



2

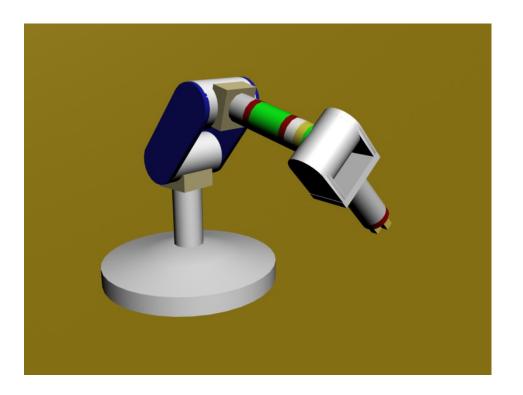
Assembly Robot Workspaces



Serial Robotic Manipulators

Proximal link: closer to the base **Distal link:** farther from the base

- Serial chain of robotic links and joints
 - Large workspace
 - Low stiffness
 - Cumulative errors from link to link
 - Proximal links carry the weight and load of distal links
 - Actuation of proximal joints affects distal links
 - Limited load-carrying capability at end effecter



Humanoid Robots







NASA/GM Robonaut



Disney Audio-Animatronics, 1967

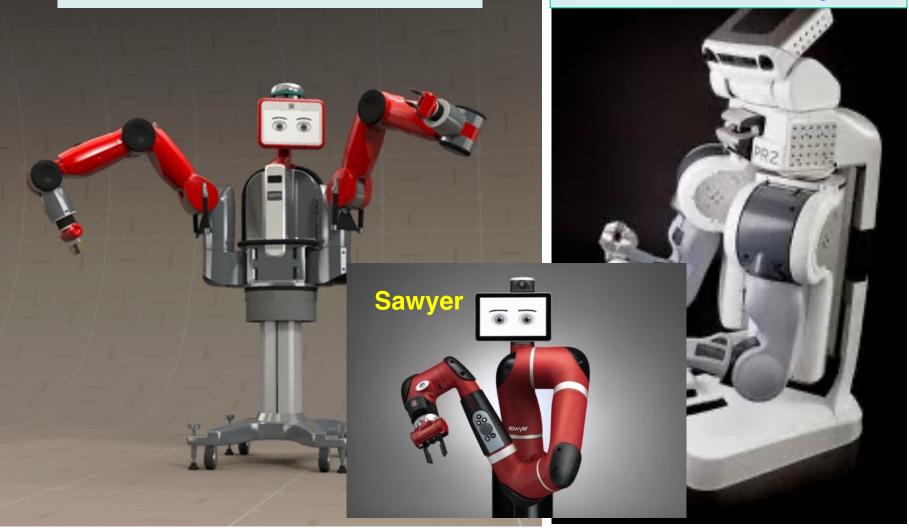






Baxter, Sawyer, and the PR2

Baxter <u>http://www.youtube.com/watch?v=Q</u> <u>HAMsalhIv8</u> PR2 <u>http://www.youtube.com/watch</u> <u>?v=HMx1xW2E4Gg</u>

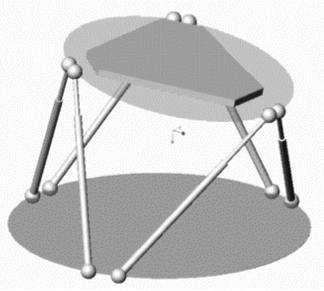


Parallel Robotic Mechanisms

- End plate is directly actuated by multiple links and joints (*kinematic chains*)
 - Restricted workspace
 - Common link-joint configuration
 - Light construction
 - Stiffness
 - High load-carrying capacity

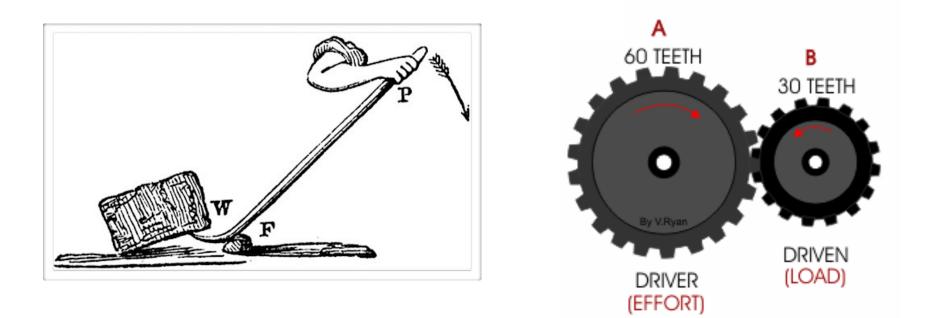
Stewart Platform http://www.youtube.com/watch?v=QdK o9PYwGaU

Pick-and-Place Rob*ot* http://www.youtube.com/watch?v=i4oB Exl2KiQ



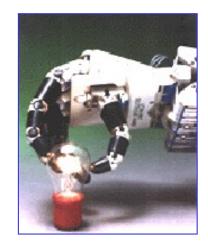


Gearing and Leverage Force multiplication Displacement ratios

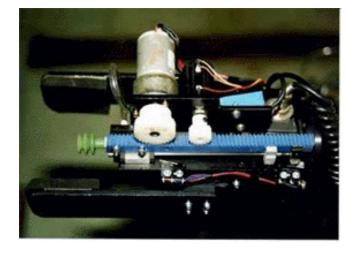


- Machine tools
 - Grinding, sanding
 - Inserting screws
 - Drilling
 - Hammering
- Paint sprayer
- Gripper, clamp
- Multi-digit hand

End Effecters

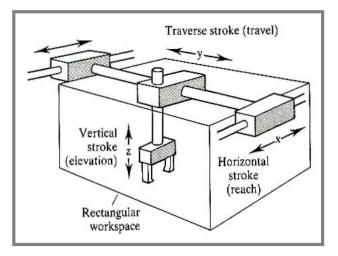


DARPA Prosthetic Hand http://www.youtube.com/watch?v=QJg 9igTnjlo&feature=related

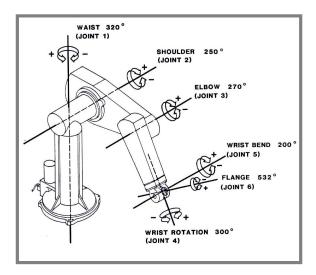






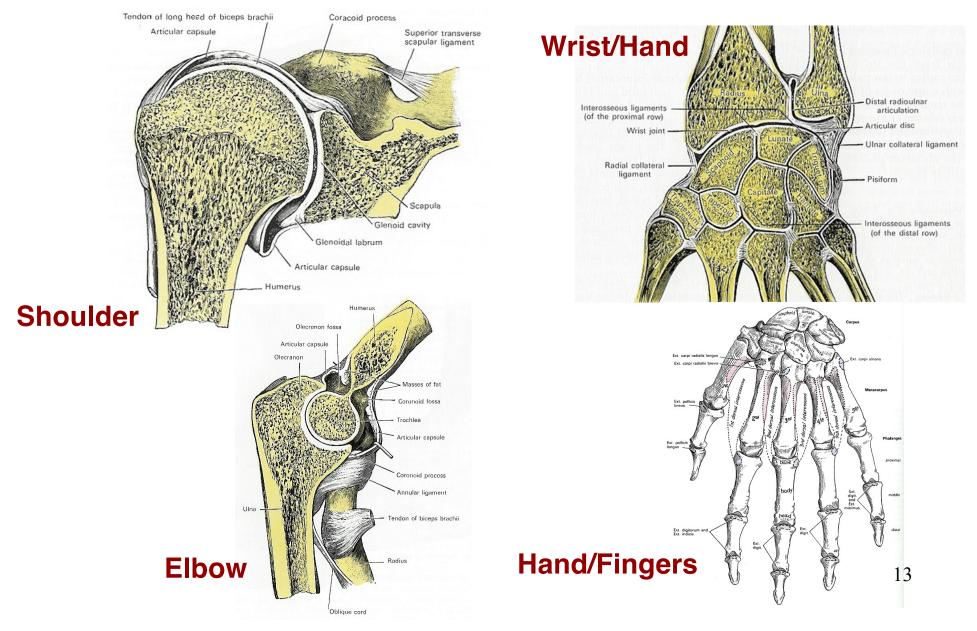


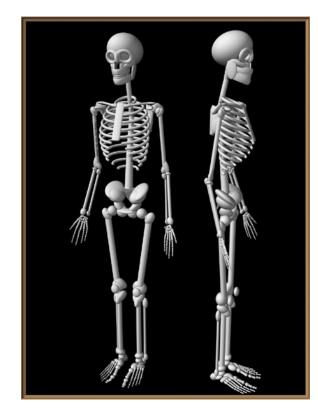
Links and Joints



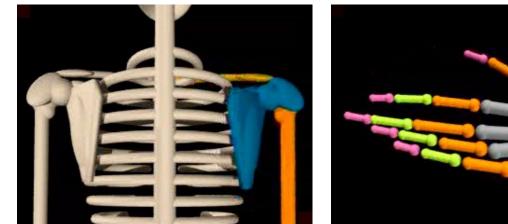


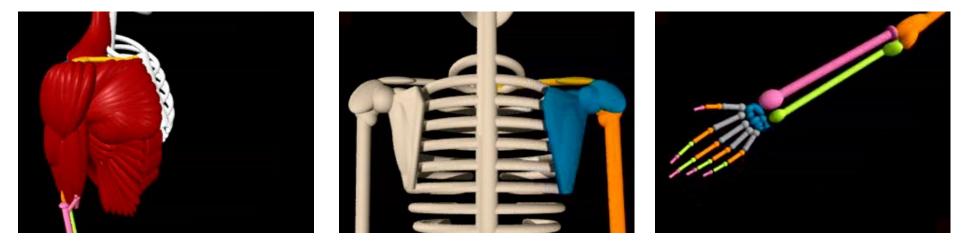
Human Joints Gray's Anatomy, 1858

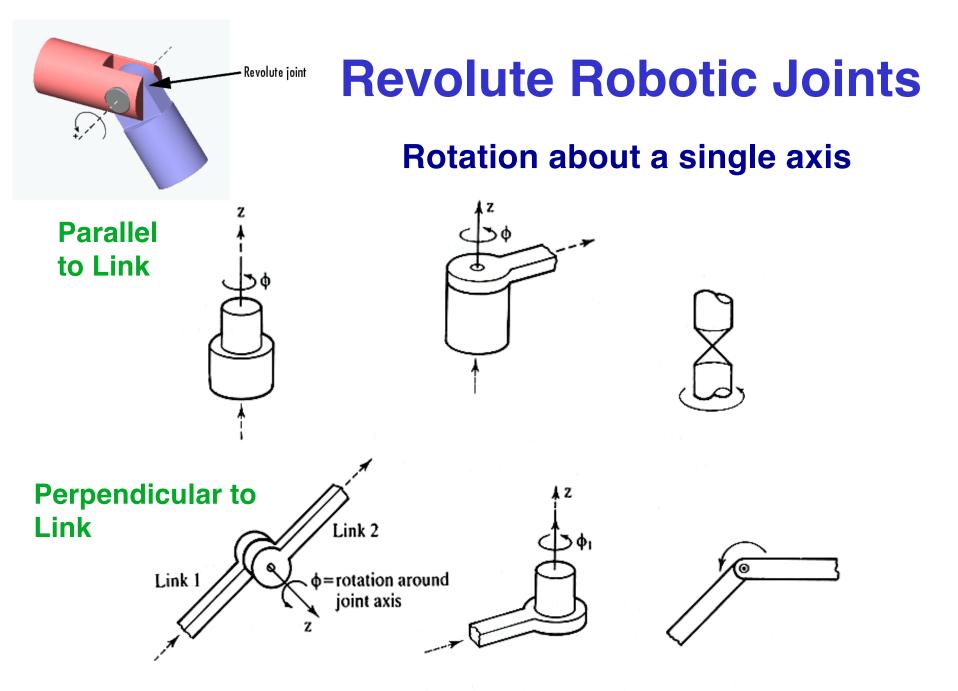




Skeleton and Muscle-Induced Motion

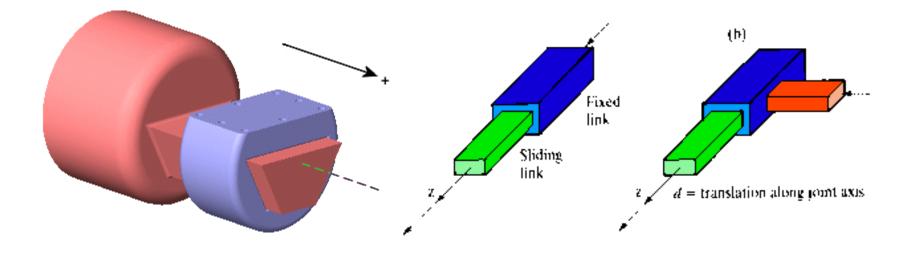






Prismatic Robotic Joints

Sliding along a single axis



Universal



Other Robotic Joints

Flexible

Spherical (or ball)





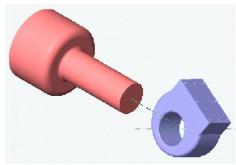
Constant-Velocity



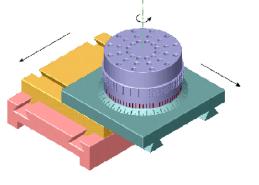
Roller Screw



Cylindrical (sliding and turning composite)



Planar (sliding and turning composite)

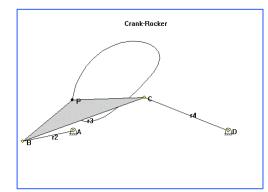


Construction Cranes

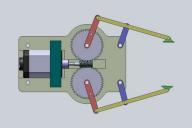




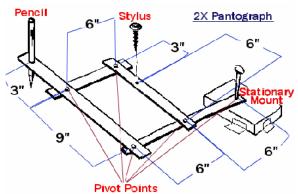




Four-Bar Linkage



- Closed-loop structure
- Rotational joints
- Planar motion
- Proportions of link lengths determine pattern of motion
- Examples
 - Double wishbone suspension
 - Pantograph
 - Scissor lift
 - Gripper

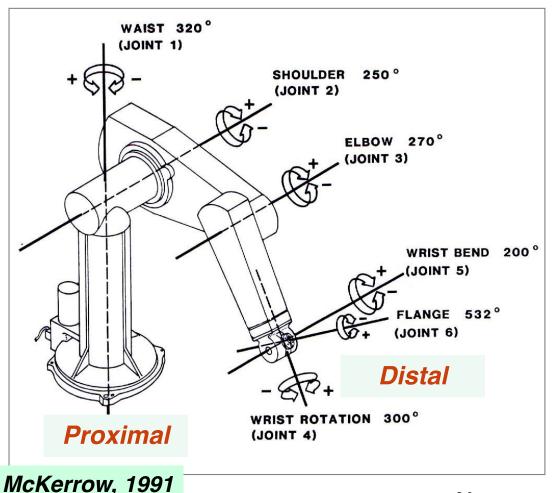




Characteristic Transformation of a Link

Link: solid structure between two joints

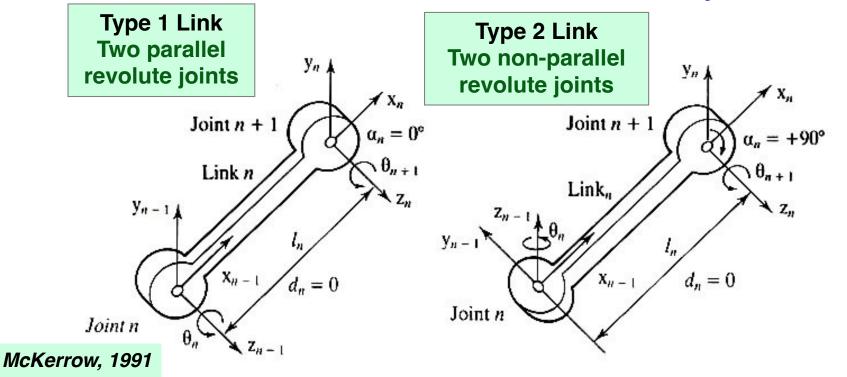
- Each link type has a characteristic transformation matrix relating the proximal joint to the distal joint
- Link n has
 - <u>Proximal end</u>: Joint *n*, coordinate frame *n* 1
 - <u>Distal end</u>: Joint *n* + 1, coordinate frame *n*



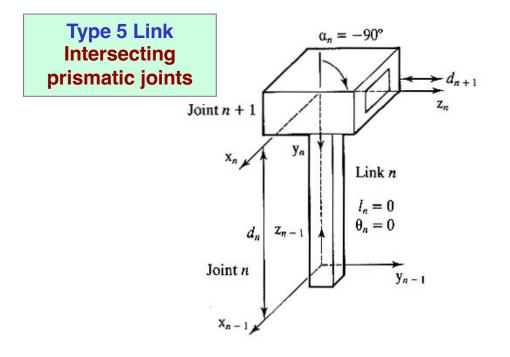
Links Between Revolute Joints

- Link: solid structure between two joints
 - Proximal end: closer to the base
 - Distal end: farther from the base

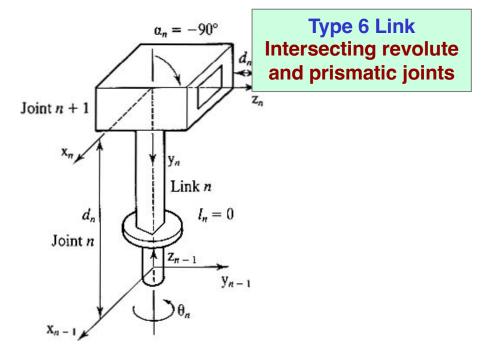
- 4 Link Parameters
 - Length of the link between rotational axes, *I*, along the common normal
 - Twist angle between axes, α
 - Angle between 2 links, θ (revolute)
 - Offset between links, *d* (prismatic)
- Joint Variable: single link parameter that is free to vary



Links Involving Prismatic Joints



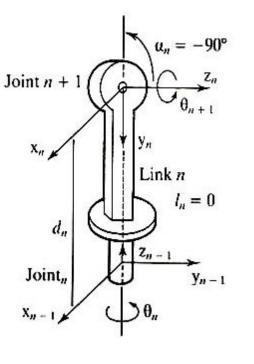
- Link *n* extends along z_{n-1} axis
 - $I_n = 0$, along x_{n-1}
 - $d_n = \text{length}, \text{ along } z_{n-1}$ (variable)
 - $\theta_n = 0$, about z_{n-1}
 - a_n = fixed orientation of n + 1prismatic axis about x_{n-1}



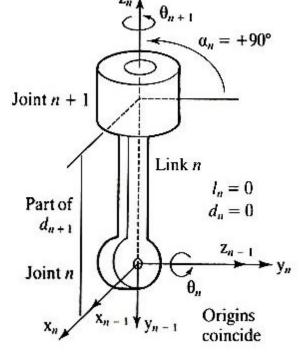
- Link *n* extends along z_{n-1} axis
 - $I_n = 0, \text{ along } x_{n-1}$
 - $d_n = \text{length}, \text{ along } z_{n-1}$ (fixed)
 - θ_n = variable joint angle *n* about z_{n-1}
 - *a_n* = fixed orientation of *n* + 1
 prismatic axis about *x_{n-1}*

Links Between Revolute Joints - 2

Type 3 Link Two revolute joints with intersecting rotational axes (e.g., shoulder)



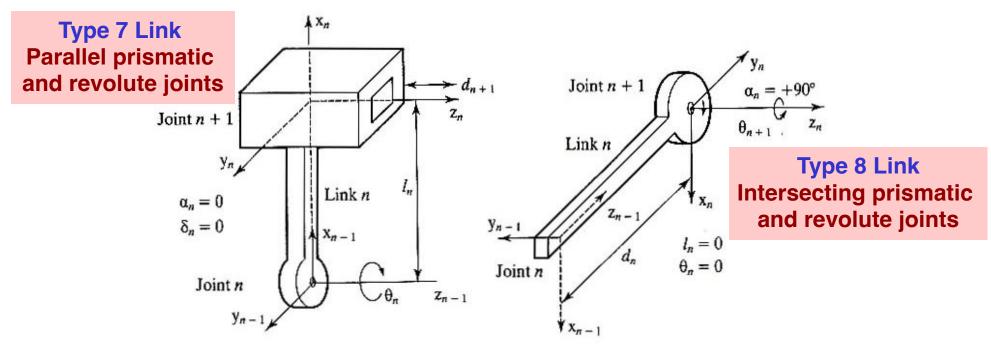
- Link *n* extends along z_{n-1} axis
 - $I_n = 0$, along x_{n-1}
 - $d_n = \text{length}, \text{ along } z_{n-1}$ (fixed)
 - θ_n = variable joint angle *n* about z_{n-1}
 - *a_n* = fixed orientation of *n* + 1 rotational axis about *x_{n-1}*



Type 4 Link Two perpendicular revolute joints with common origin (e.g., elbow-wrist)

- Link *n* extends along -*z_n* axis
 - $I_n = 0$, along x_{n-1}
 - $d_n = 0$, along z_{n-1}
 - θ_n = variable joint angle *n* about z_{n-1}
 - a_n = fixed orientation of n + 1rotational axis about x_{n-23}

Links Involving Prismatic Joints - 2



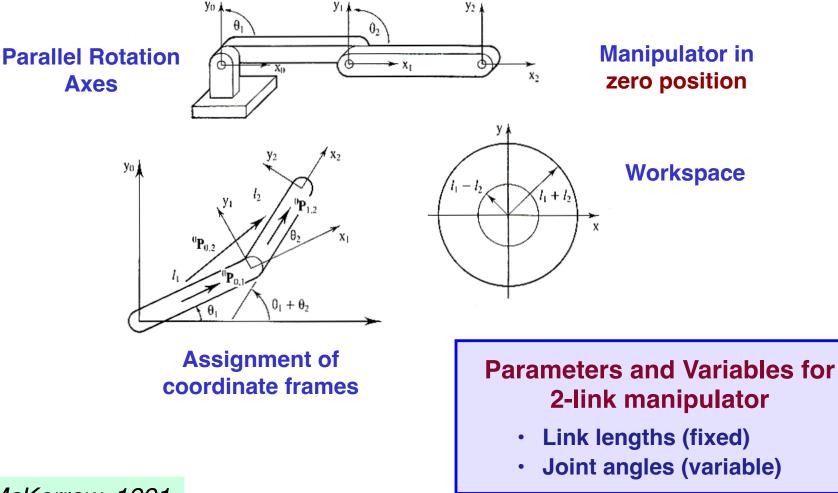
- Link *n* extends along x_{n-1} axis
 - $I_n = \text{length along } x_{n-1}$
 - $d_n = 0$, along z_{n-1}
 - θ_n = variable joint angle *n* about z_{n-1}
 - $a_n = 0$, orientation of n + 1prismatic axis about x_{n-1}

McKerrow, 1991

- Link *n* extends along *z_{n-1}* axis
 - $I_n = 0$, along x_{n-1}
 - *d_n* = length, along *z_{n-1}* (variable)
 - $\theta_n = 0$, about z_{n-1}
 - $a_n = fixed orientation of <math>n + 1$ rotational axis about x_{n-1} 24



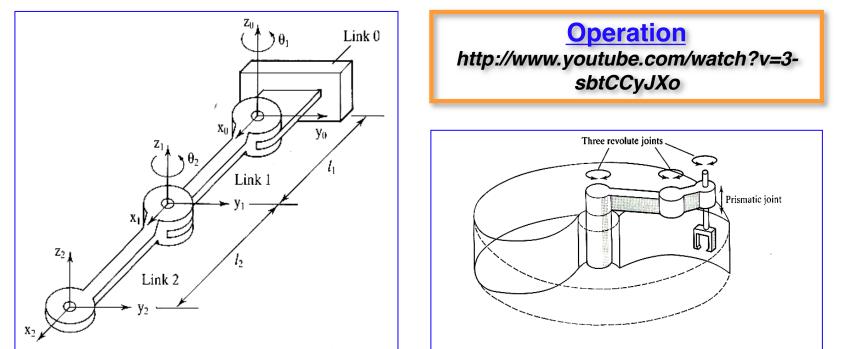
Two-Link/Three-Joint Manipulator



Four-Joint (SCARA*) Manipulator

Arm with Three Revolute Link Variables (Joint Angles)





McKerrow, 1991

*Selective Compliant Articulated Robot Arm

Joint Variables Must Be Actuated and Observed for Control



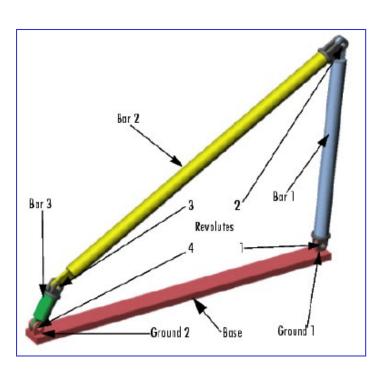
•Frames of Reference for Actuation and Control

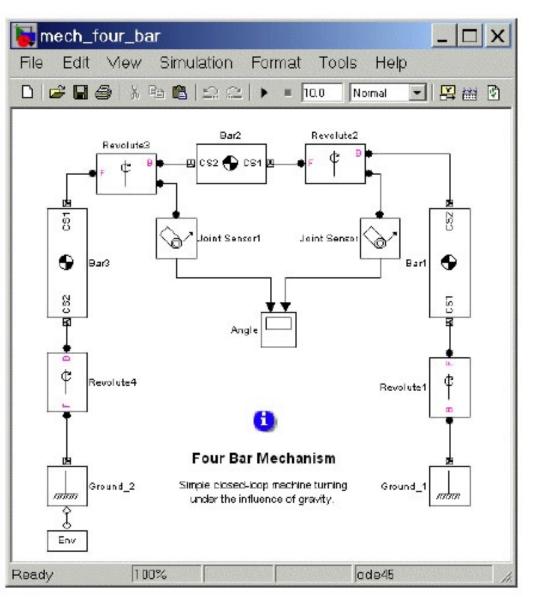
- World coordinates
- Actuator coordinates
- Joint coordinates
- Tool coordinates

Three revolute joint Prismatic joint

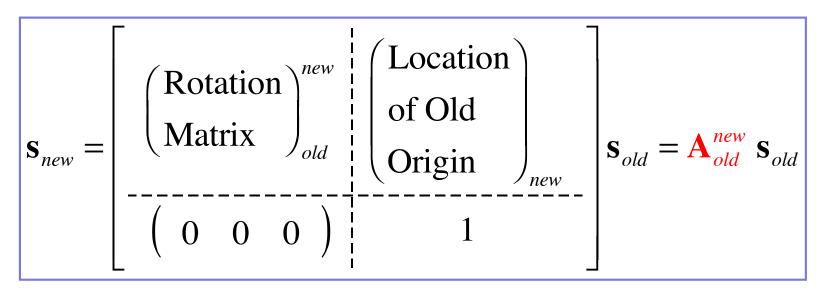
Sensors May Observe Joints Directly, Indirectly, or Not At All **Linear Actuator**

Simulink/SimMechanics Representation of Four-Bar Linkage

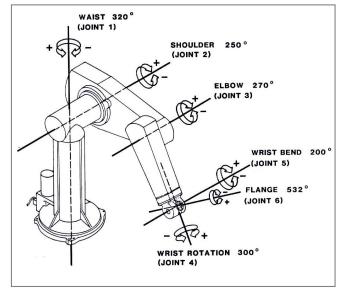




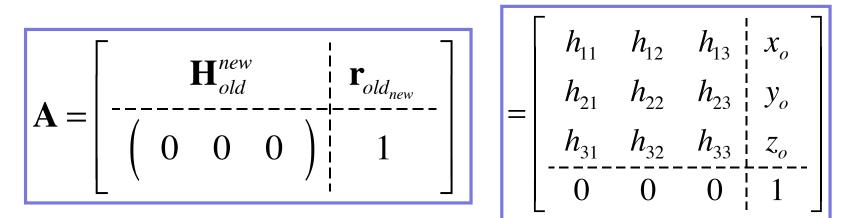
Recall: Homogeneous Transformation



Transform from one joint to the next



Rotation Matrix can be Derived from Euler Angles or Quaternions





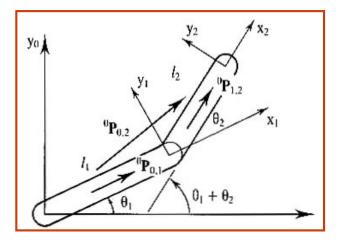
Series of Homogeneous Transformations

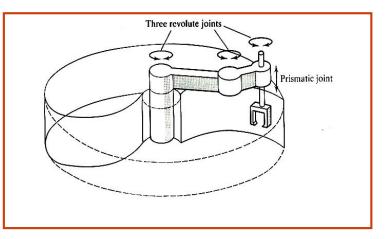
Two serial transformations can be combined in a single transformation

$$\mathbf{s}_2 = \mathbf{A}_1^2 \mathbf{A}_0^1 \ \mathbf{s}_0 = \mathbf{A}_0^2 \ \mathbf{s}_0$$

Four transformations for SCARA robot

$$\mathbf{s}_4 = \mathbf{A}_3^4 \mathbf{A}_2^3 \mathbf{A}_1^2 \mathbf{A}_0^1 \ \mathbf{s}_0 = \mathbf{A}_0^4 \ \mathbf{s}_0$$

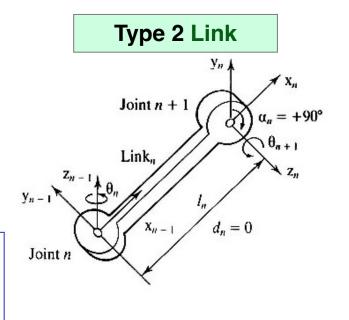




Transformation for a Single Robotic Joint-Link

- <u>Each joint-link</u> requires four <u>sequential</u> transformations:
 - Rotation about α
 - Translation along *d*
 - Translation along *I*
 - Rotation about θ

Ath



$$\mathbf{s}_{n+1} = \mathbf{A}_3^{n+1} \mathbf{A}_2^3 \mathbf{A}_1^2 \mathbf{A}_n^1 \mathbf{s}_n = \mathbf{A}_n^{n+1} \mathbf{s}_n$$
$$= \mathbf{A}_{\theta} \mathbf{A}_d \mathbf{A}_l \mathbf{A}_{\alpha} \mathbf{s}_n = \mathbf{A}_n^{n+1} \mathbf{s}_n$$

Ord

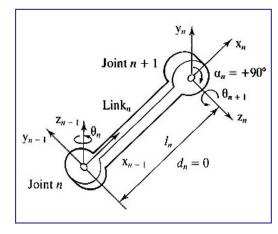
… axes for each transformation (along or around) must be specified

ond

-l et

$$\mathbf{s}_{n+1} = \mathbf{A}(z_{n-1}, \theta_n) \mathbf{A}(z_{n-1}, d_n) \mathbf{A}(x_{n-1}, l_n) \mathbf{A}(x_{n-1}, \alpha_n) \mathbf{s}_n = \mathbf{A}_n^{n+1} \mathbf{s}_n$$

Denavit-Hartenberg Representation of Joint-Link-Joint Transformation



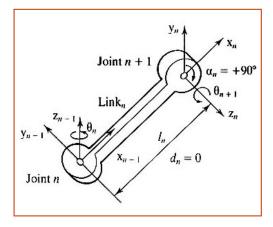
Denavit-Hartenberg Representation of Joint-Link-Joint Transformation

- Like Euler angle rotation, transformational effects of the 4 link parameters are defined in a specific application sequence (right to left): {θ, d, l, α}
- <u>4 link parameters</u>
 - Angle between 2 links, *θ* (revolute)
 - Distance (offset) between links, *d* (prismatic)
 - Length of the link between rotational axes, *I*, along the common normal (prismatic)
 - Twist angle between axes, α (revolute)

$$\mathbf{A}_{n} = \mathbf{A}(z_{n-1}, \theta_{n}) \mathbf{A}(z_{n-1}, d_{n}) \mathbf{A}(x_{n-1}, l_{n}) \mathbf{A}(x_{n-1}, \alpha_{n})$$

= Rot(z_{n-1}, \theta_{n}) Trans(z_{n-1}, d_{n}) Trans(x_{n-1}, l_{n}) Rot(x_{n-1}, \alpha_{n})
$$\triangleq {}^{n}\mathbf{T}_{n+1} \text{ in some references (e.g., McKerrow, 1991)}$$

Denavit-Hartenberg Demo <u>http://www.youtube.com/watch?v=10mUtjfGmzw</u>



Four Transformations from One Joint to the Next (Single Link)

Rotation of θ_n about the z_{n-1} axis

$\mathbf{D}_{ot}(\mathbf{z} = 0)$	$\cos\theta_n$	$-\sin\theta_n$	0	0
	sinA	_	0	0
$\operatorname{Rot}(z_{n-1}, \theta_n) =$	0	0	1	0
	0	0	0	1

Translation of I_n along the x_{n-1} axis

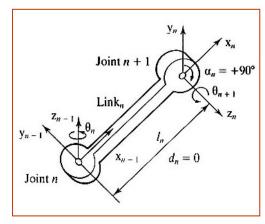
Trans
$$(x_{n-1}, l_n) = \begin{bmatrix} 1 & 0 & 0 & l_n \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

Translation of d_n along the z_{n-1} axis

$$\operatorname{Trans}(z_{n-1}, d_n) = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & d_n \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

Rotation of α_n about the x_{n-1} axis

$$\operatorname{Rot}(x_{n-1},\alpha_n) = \begin{vmatrix} 1 & 0 & 0 & 0 \\ 0 & \cos\alpha_n & -\sin\alpha_n & 0 \\ 0 & \sin\alpha_n & \cos\alpha_n & 0 \\ 0 & 0 & 0 & 1 \end{vmatrix}$$



Denavit-Hartenberg Representation of Joint-Link-Joint Transformation

Then

Then

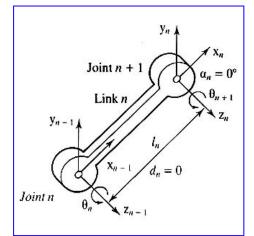
$\mathbf{A}_{n}^{n-1} = \begin{bmatrix} \cos\theta_{n} & -\sin\theta_{n} & 0 & 0\\ \sin\theta_{n} & \cos\theta_{n} & 0 & 0\\ 0 & 0 & 1 & 0\\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0\\ 0 & 1\\ 0 & 0\\ 0 & 0 \end{bmatrix}$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{bmatrix} 0 & l_n \\ 0 & 0 \\ 1 & 0 \\ 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 \\ 0 & \cos \alpha_n \\ 0 & \sin \alpha_n \\ 0 & 0 \end{bmatrix}$	$ \begin{array}{cccc} 0 & 0 \\ -\sin \alpha_n & 0 \\ \cos \alpha_n & 0 \\ 0 & 1 \end{array} $
---	--	---	---

Then

$$\mathbf{A}_{n}^{n-1} = \begin{bmatrix} \cos\theta_{n} & -\sin\theta_{n}\cos\alpha_{n} & \sin\theta_{n}\sin\alpha_{n} & l_{n}\cos\theta_{n} \\ \sin\theta_{n} & \cos\theta_{n}\cos\alpha_{n} & -\cos\theta_{n}\sin\alpha_{n} & l_{n}\sin\theta_{n} \\ 0 & \sin\alpha_{n} & \cos\alpha_{n} & d_{n} \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

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First



Example: Joint-Link-Joint Transformation, Type 1 Link

Joint Variable = θ_n

θ = variable
d = 0 m
l = 0.25 m
α = 90 deg

$$\theta \triangleq 30 \text{ deg}$$

 $d = 0 \text{ m}$
 $l = 0.25 \text{ m}$
 $\alpha = 90 \text{ deg}$

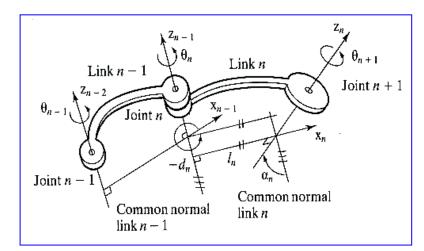
	$\cos \theta_n$	$-\sin\theta_n\cos\alpha_n$	$\sin \theta_n \sin \alpha_n$	$l_n \cos \theta_n$
A ^{<i>n</i>-1} -	$\sin \theta_n$	$\cos \theta_n \cos \alpha_n$	$-\cos\theta_n\sin\alpha_n$	$l_n \sin \theta_n$
\mathbf{A}_n –	0	$\sin \alpha_n$	$\cos \alpha_n$	d_n
	0	0	0	1

г

	$\int \cos \theta_n$	0	$\sin \theta_n$	$0.25\cos\theta_n$
$A^{n-1} =$	$\sin \theta_n$	0	$-\cos\theta_n$	$0.25\sin\theta_n$
- n	0	1	0	0
	0	0	0	1

$\mathbf{A}_{n}^{n-1} =$	0.866			0.217]
	0.5	0	-0.866	0.125	
	0	1	0	0	
	0	0	0	1	

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Forward and Inverse Transformations

Forward transformation: proximal to distal frame (Expression of proximal frame in distal frame)

$$\mathbf{s}_1 = \mathbf{A}_0^1 \mathbf{s}_0$$
; $s_2 = \mathbf{A}_1^2 \mathbf{s}_1 = \mathbf{A}_1^2 \mathbf{A}_0^1 \mathbf{s}_0 = \mathbf{A}_0^2 \mathbf{s}_0$

<u>Reverse transformation</u>: distal to proximal frame = inverse of forward transformation

$$\mathbf{s}_0 = \left(\mathbf{A}_0^2\right)^{-1} \mathbf{s}_2 = \mathbf{A}_2^0 \mathbf{s}_2 = \mathbf{A}_1^0 \mathbf{A}_2^1 \mathbf{s}_2$$

Homogeneous Transformation Matrix is not Orthonormal

$$\mathbf{A}_{2}^{0} = \left(\mathbf{A}_{0}^{2}\right)^{-1} \neq \left(\mathbf{A}_{0}^{2}\right)^{T}$$

...but a useful identity makes inversion simple

Matrix Inverse Identity

Given: a square matrix, **A**, and its inverse, **B**

$$\mathbf{A} = \begin{bmatrix} \mathbf{A}_1 & \mathbf{A}_2 \\ -\frac{m \times m}{\mathbf{A}_3} & \frac{m \times n}{n \times n} \end{bmatrix} ; \quad \mathbf{B} \triangleq \mathbf{A}^{-1} = \begin{bmatrix} \mathbf{B}_1 & \mathbf{B}_2 \\ \mathbf{B}_3 & \mathbf{B}_4 \end{bmatrix}$$

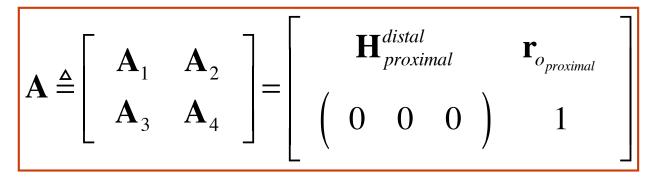
Then
$$\begin{vmatrix} \mathbf{A}\mathbf{B} = \mathbf{A}\mathbf{A}^{-1} = \mathbf{I}_{m+n} \\ = \begin{bmatrix} \mathbf{I}_m & \mathbf{0} \\ \mathbf{0} & \mathbf{I}_n \end{bmatrix} = \begin{bmatrix} (\mathbf{A}_1\mathbf{B}_1 + \mathbf{A}_2\mathbf{B}_3) & (\mathbf{A}_1\mathbf{B}_2 + \mathbf{A}_2\mathbf{B}_4) \\ (\mathbf{A}_3\mathbf{B}_1 + \mathbf{A}_4\mathbf{B}_3) & (\mathbf{A}_3\mathbf{B}_2 + \mathbf{A}_4\mathbf{B}_4) \end{bmatrix}$$

Equating like parts, and solving for B_i

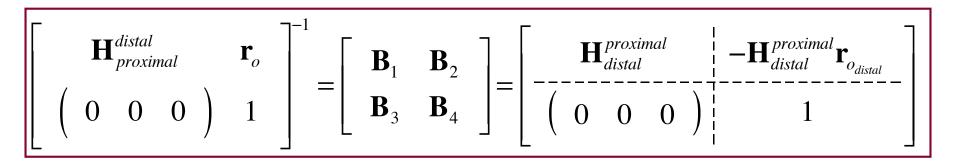
$$\begin{bmatrix} \mathbf{B}_{1} & \mathbf{B}_{2} \\ \mathbf{B}_{3} & \mathbf{B}_{4} \end{bmatrix} = \begin{bmatrix} (\mathbf{A}_{1} - \mathbf{A}_{2}\mathbf{A}_{4}^{-1}\mathbf{A}_{3})^{-1} & -\mathbf{A}_{1}^{-1}\mathbf{A}_{2}(\mathbf{A}_{4} - \mathbf{A}_{3}\mathbf{A}_{1}^{-1}\mathbf{A}_{2})^{-1} \\ -\mathbf{A}_{4}^{-1}\mathbf{A}_{3}(\mathbf{A}_{1} - \mathbf{A}_{2}\mathbf{A}_{4}^{-1}\mathbf{A}_{3})^{-1} & (\mathbf{A}_{4} - \mathbf{A}_{3}\mathbf{A}_{1}^{-1}\mathbf{A}_{2})^{-1} \end{bmatrix}$$

Apply to Homogeneous Transformation

Forward transformation (to distal frame)

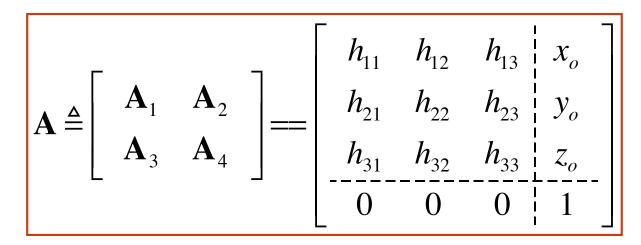


Inverse transformation (to proximal frame)



Apply to Homogeneous Transformation

Forward transformation



Inverse transformation

$\begin{bmatrix} h_{11} \end{bmatrix}$	<i>h</i> ₁₂	h_{13}]-1	h_{11}	<i>h</i> ₂₁	h_{31}	$-(h_{11}x_o + h_{21}y_o + h_{31}z_o)$
h_{21}	h_{22}	h_{23}	y _o	_	h_{12}	h_{22}	<i>h</i> ₃₂	$-(h_{12}x_{o}+h_{22}y_{o}+h_{32}z_{o})$
11	h_{32}		z_o		h_{13}	h_{23}	h_{33}	$-(h_{13}x_o + h_{23}y_o + h_{33}z_o)$
0	0	0	1 -] [0	0	0	1

Next Time: Transformations, Trajectories, and Path Planning