



Characteristics of ultrahigh temperature flame

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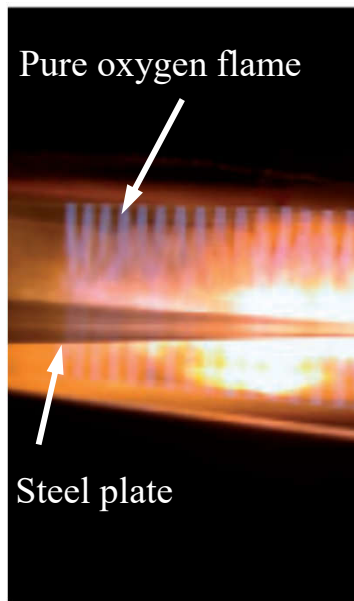
- **Background**
- Theoretical analysis
- Experimental investigation
- Summary

Definition for ultrahigh temperature flame: $T_f \geq 3000 \text{ K}$

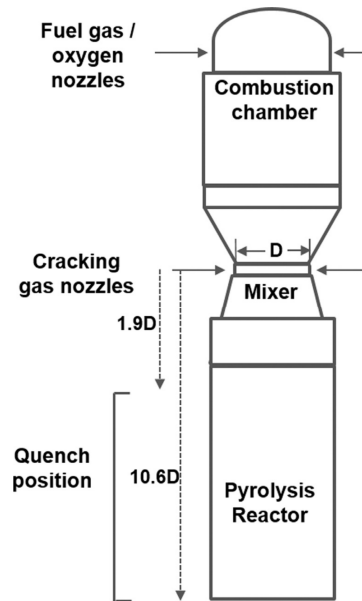
Typical flame: pure oxygen combustion, metal particle burning (Al, Mg)...



Rocket engine¹



Manufacturing²

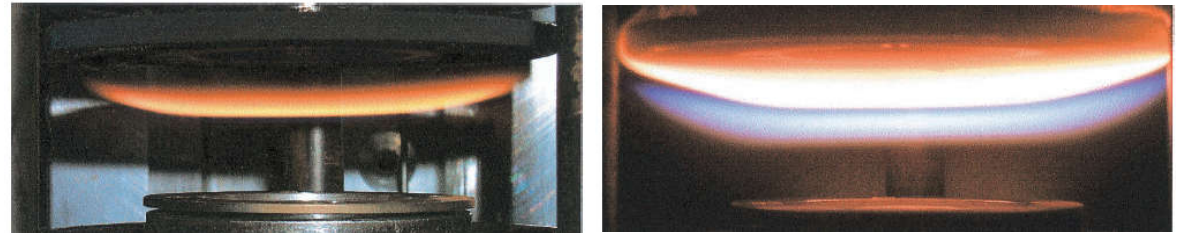
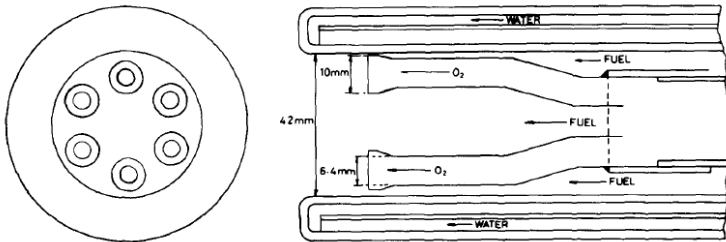


Pyrolysis reactor for acetylene³

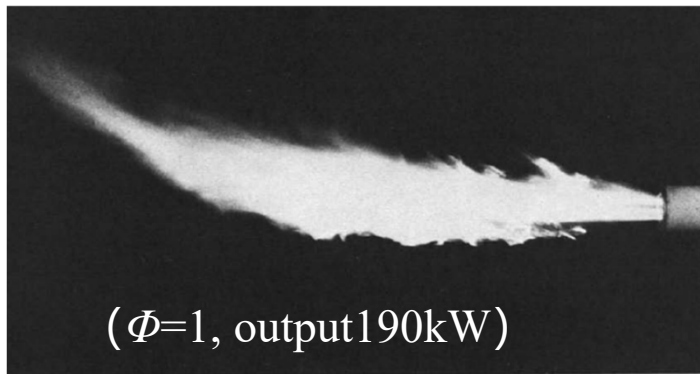
Benefits in industrial field

(e.g., Linde Corp.²)

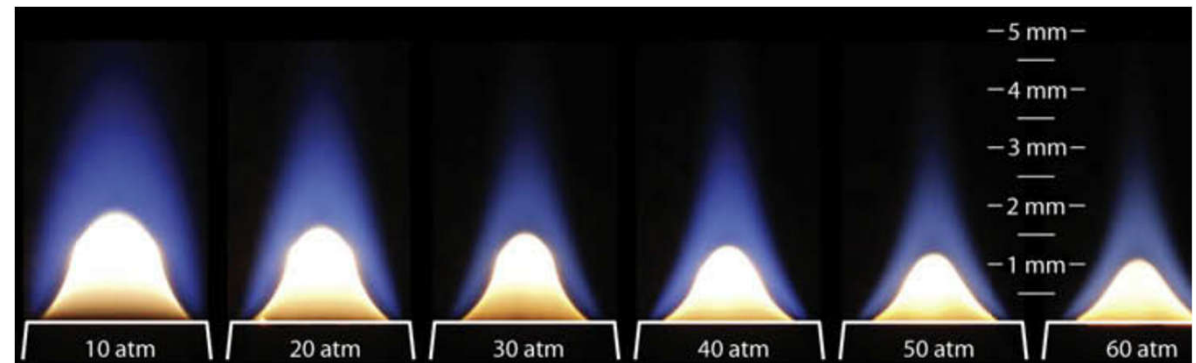
- Capacity increase **50%**
- Fuel saving up to **50%**
- CO₂ reduction up to **50%**
- NO_x emission reduction
- Reduce scaling losses



CH₄/air (left) vs. CH₄/O₂ (right) diffusion flames



CH₄/O₂ jet diffusion flame
(mixing, emission and noise)

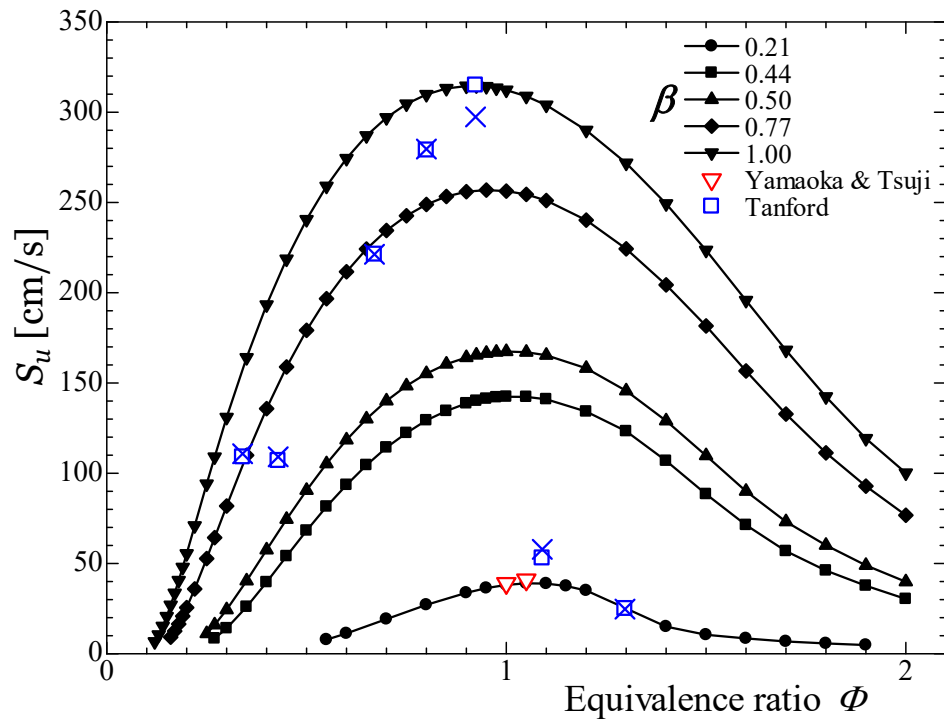


Pure oxygen flame under various pressures (10-100atm)
(flame structure and soot formation)

Mainly limited to non-premixed combustion in case of flame flash back in premixed mode

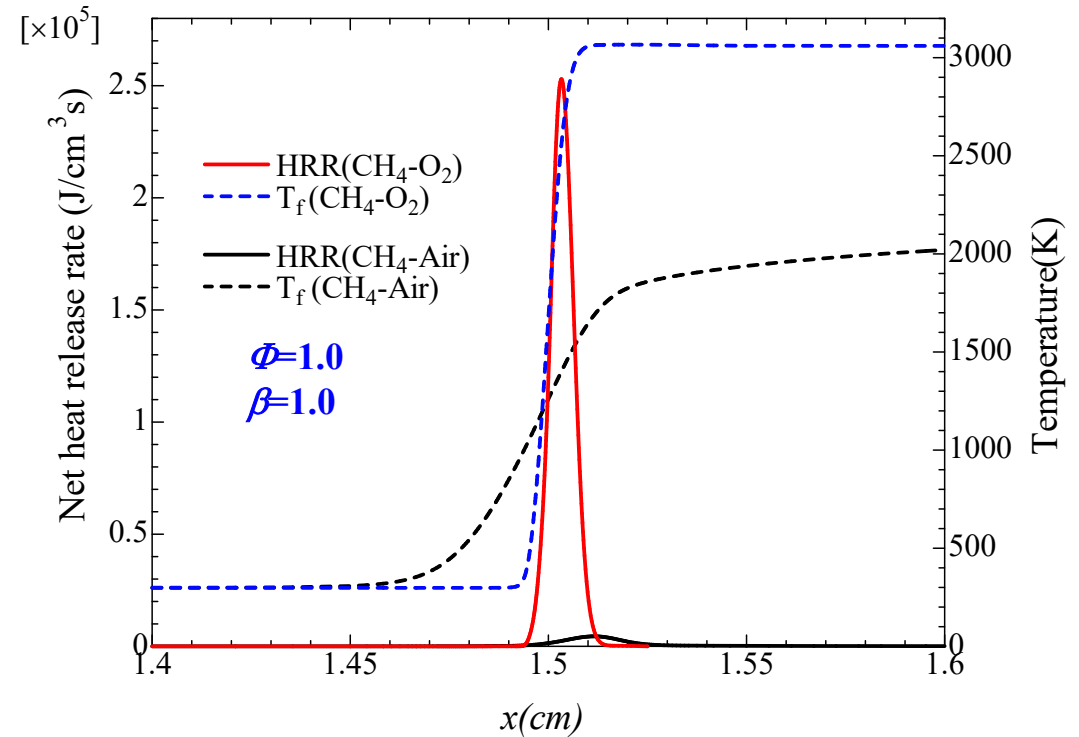


Calculated S_u for $\text{CH}_4/\text{O}_2/\text{N}_2$ flame (GRI 3.0)



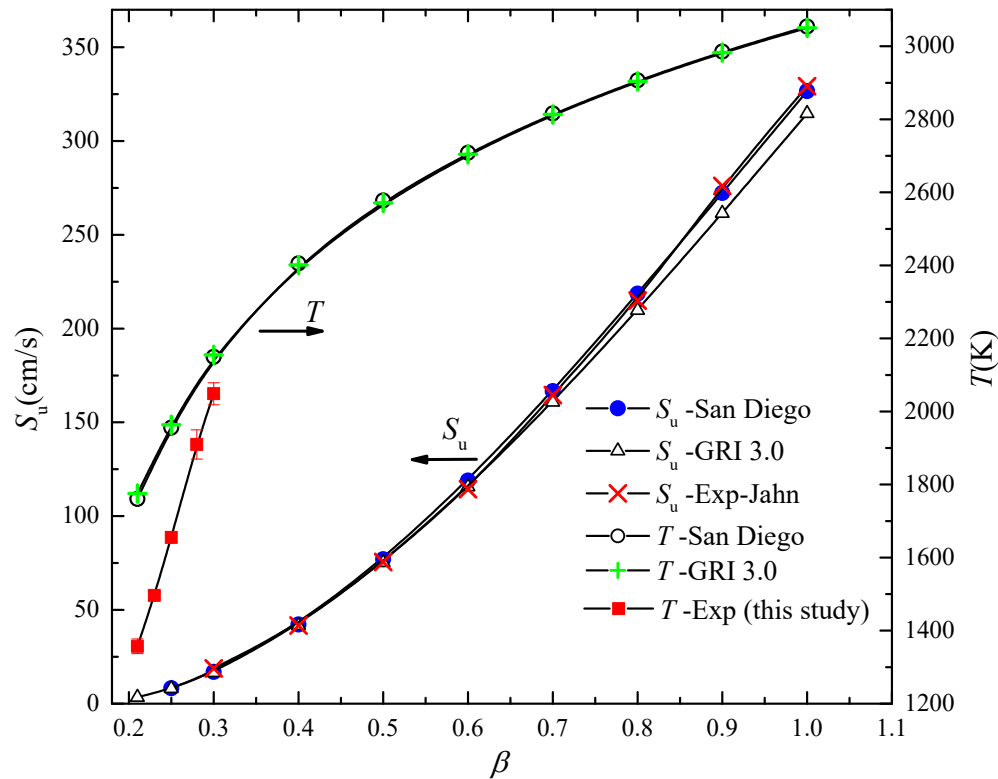
Maximum $S_u = 330 \text{ cm/s}$ (at $\Phi = 0.955$, $\beta = 1$)

Premixed CH_4/O_2 flame at $\Phi = 0.75-1.4$, $T_f \geq 3000 \text{ K}$

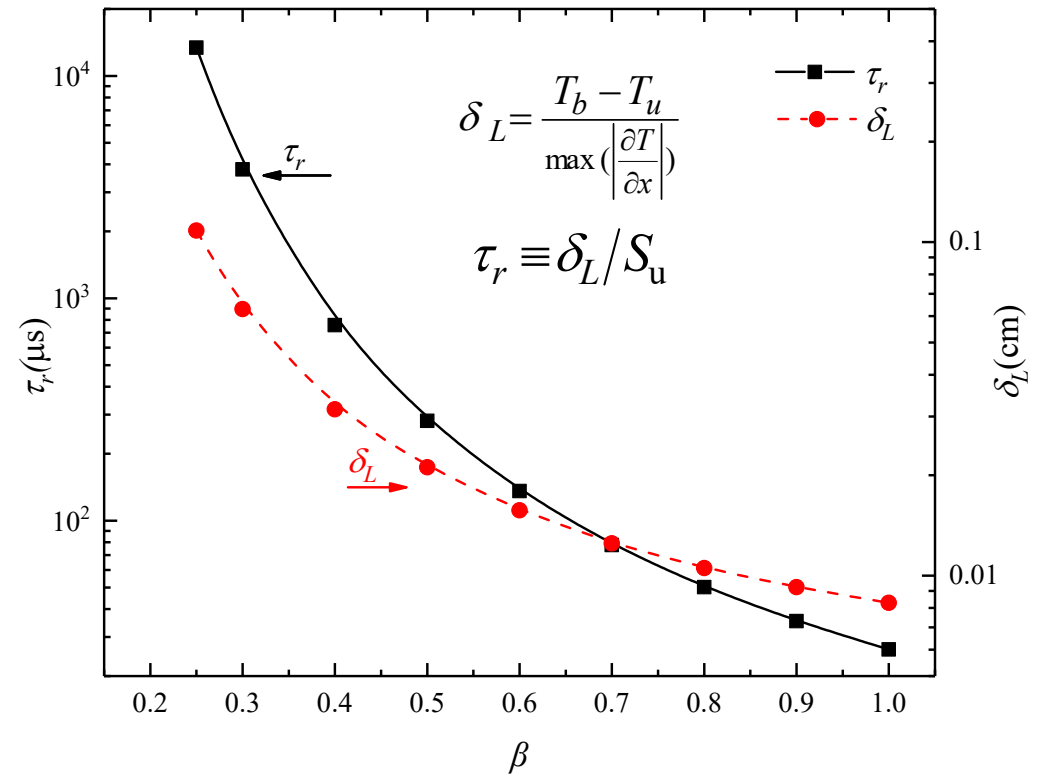


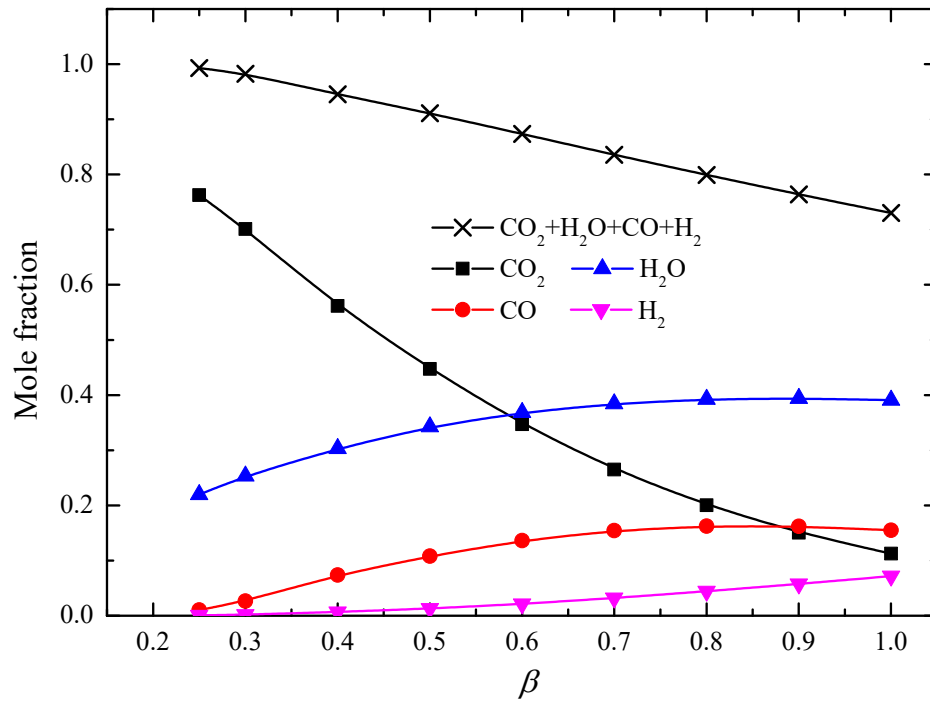
T_f : **3050 K** (vs. 2220 K in air)

Peak of HRR: **$2.54 \times 10^5 \text{ J/cm}^3 \cdot \text{s}$** (vs. $4.5 \times 10^3 \text{ J/cm}^3 \cdot \text{s}$ in air)

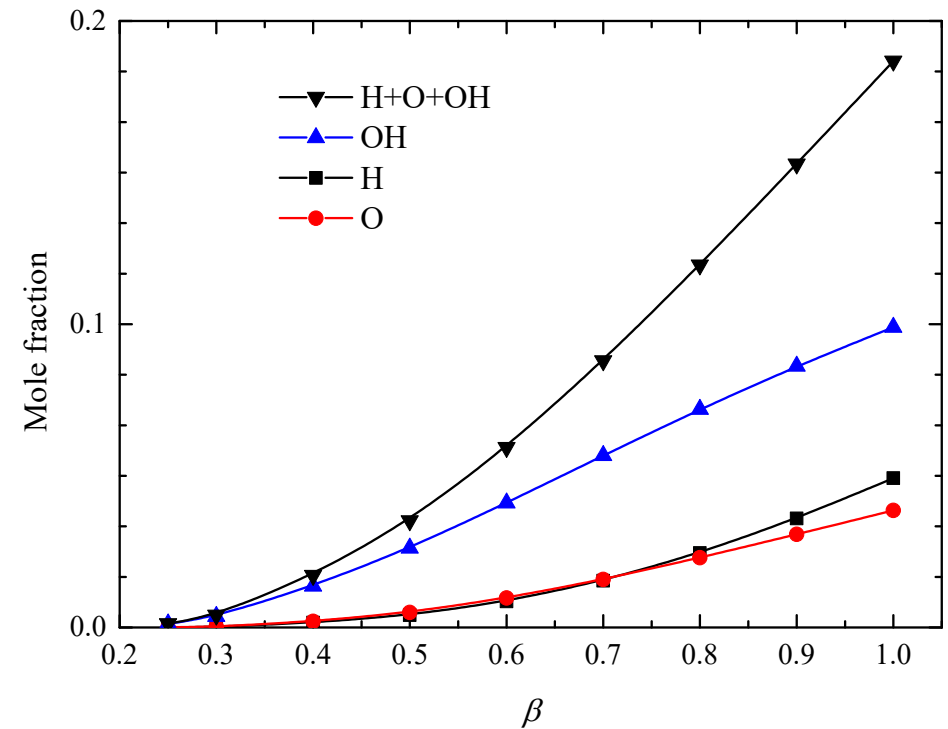
Stoichiometric $\text{CH}_4/\text{O}_2/\text{CO}_2$ premixed flame

1 D premixed flame thickness and reaction time



Stoichiometric $\text{CH}_4/\text{O}_2/\text{CO}_2$ premixed flame

Under high temperature CO_2 and H_2O cannot stably exist, yielding CO and H_2



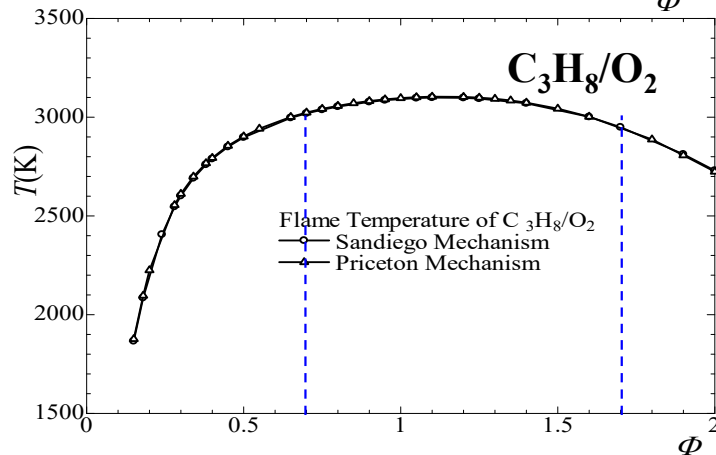
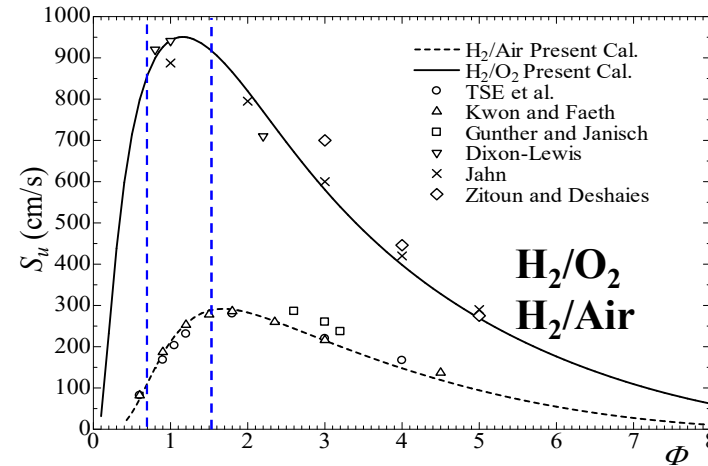
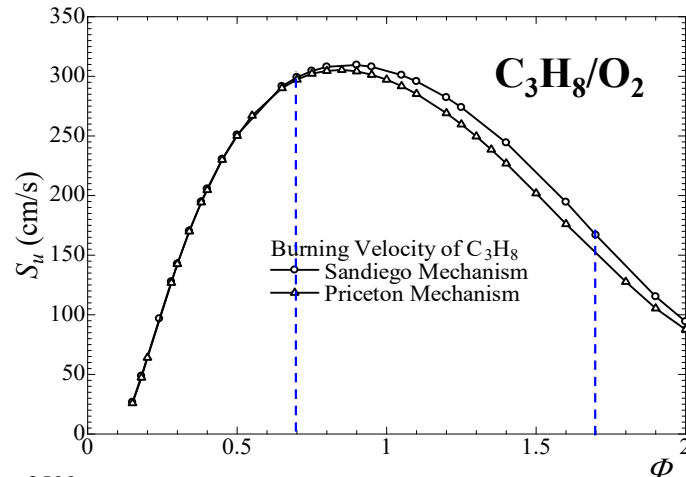
Formation of O , H and OH radicals $\sim 20\%$
 --Thermochemical heat release, reaction uncertainty

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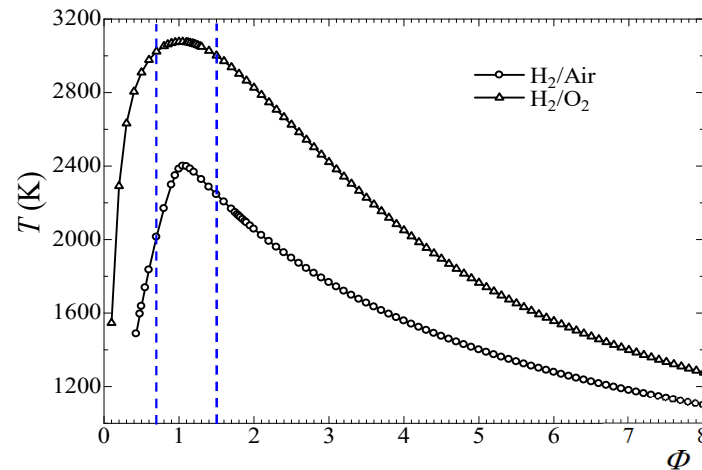
Theoretical analysis



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$\Phi=0.7-1.7: T \geq 3000 \text{ K}$

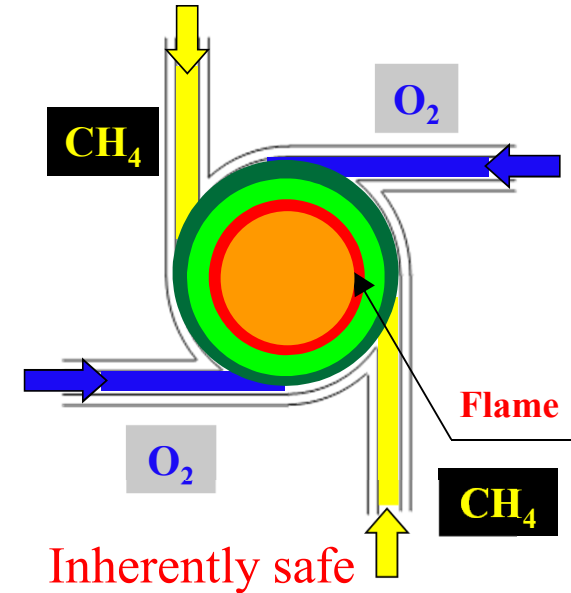


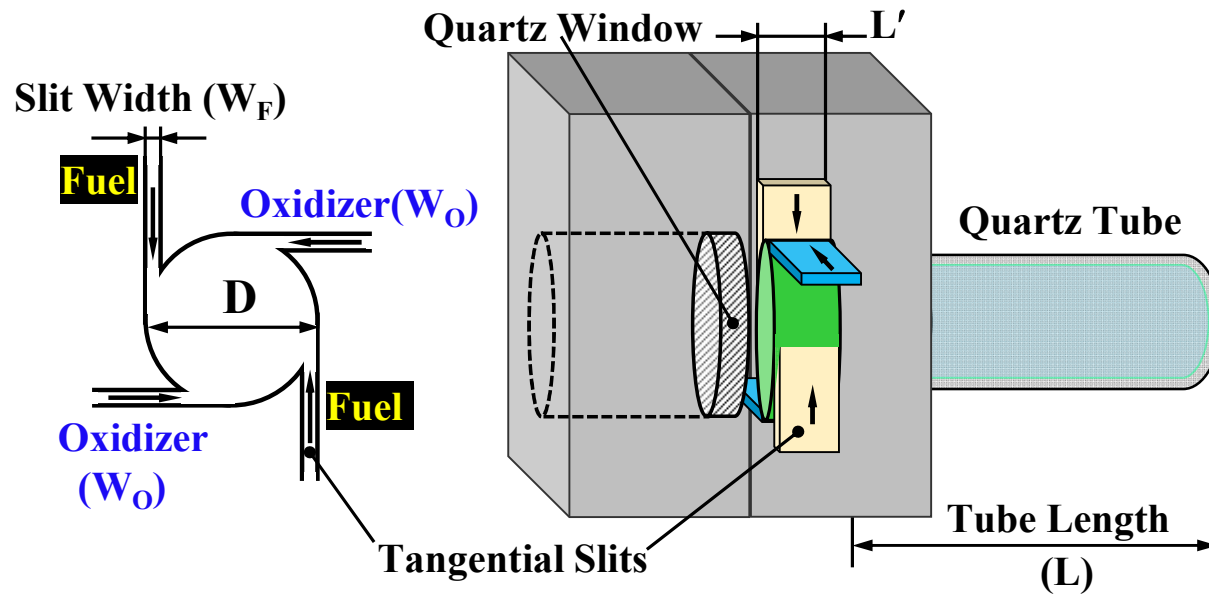
$\Phi=0.7-1.5: T \geq 3000 \text{ K}$

High $S_u \rightarrow$ flash back

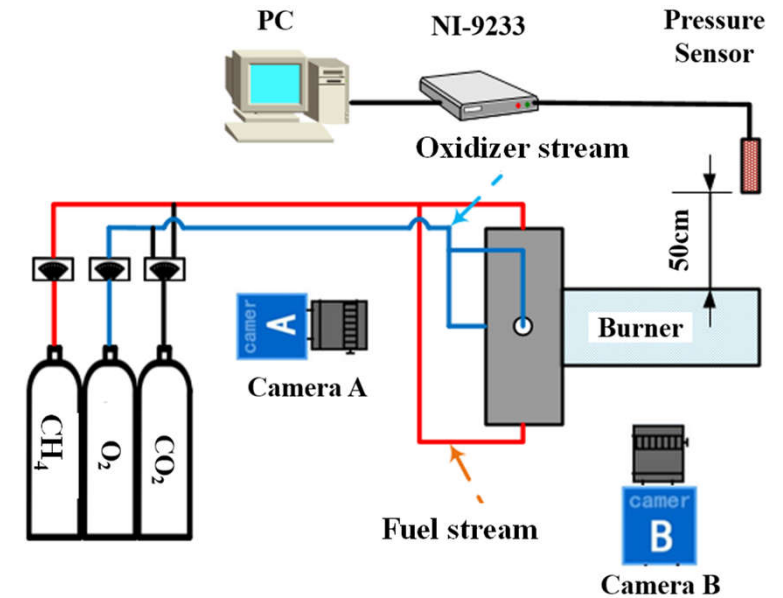
High $T \rightarrow$ ablation

Attempt quashi-premixed combustion by adopting the technique of rapidly mixed tubular flame



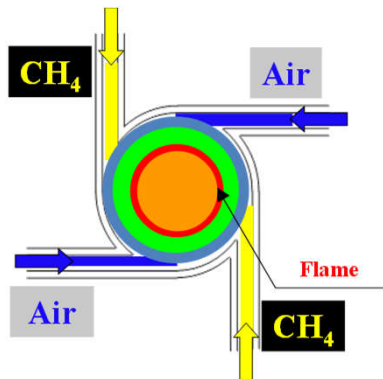


Tangential jet swirl burner

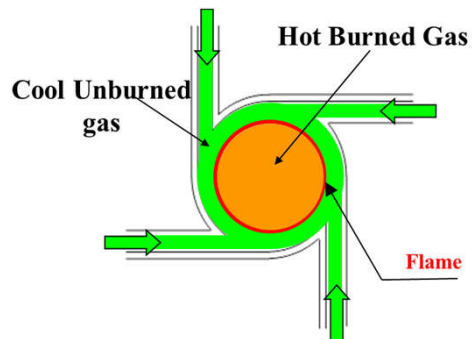


High Speed Camera: VRI, Phantom v7.3
FASTCAM- APXRS with HS-IRO intensifier
and CH* filters

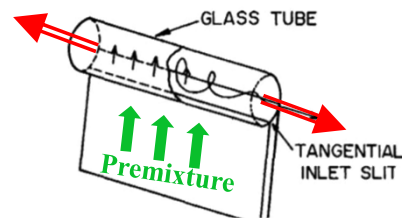
Pressure Sensor: BSWA TECH, MPA416



Rapidly mixed



Premixed

 $\Phi = 1.0$ 

Tubular Flame

S. Ishizuka: Proc. Combust. Inst. 20 (1984)

Stretched, laminar flame, tubular shape established in a rotating flow field.

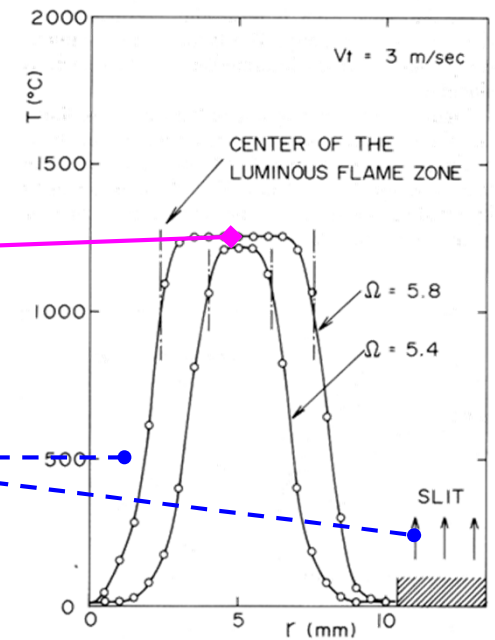
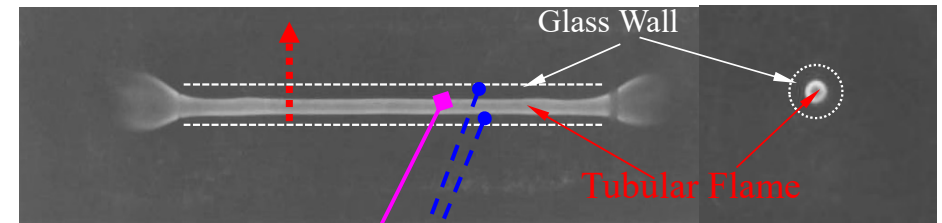
Inside : high temperature, burned gas with low density

Outside : low temperature, unburned gas with high density

Rayleigh stability : aerodynamically stable

T distribution: thermally stable

Possible for long time operation/high T_f



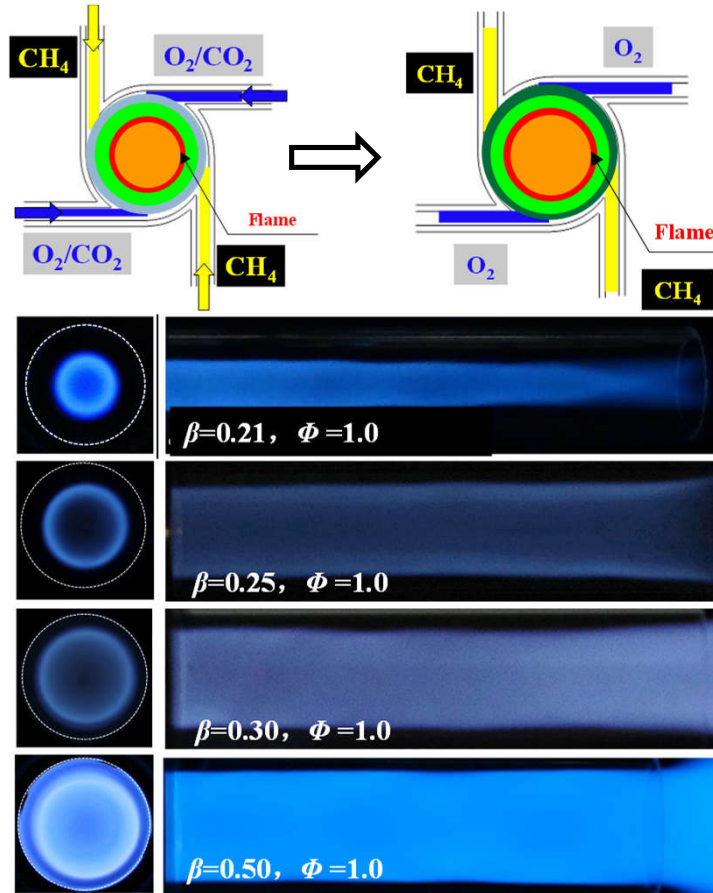
Radial temperature distribution

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Experimental investigation-Oxy-methane

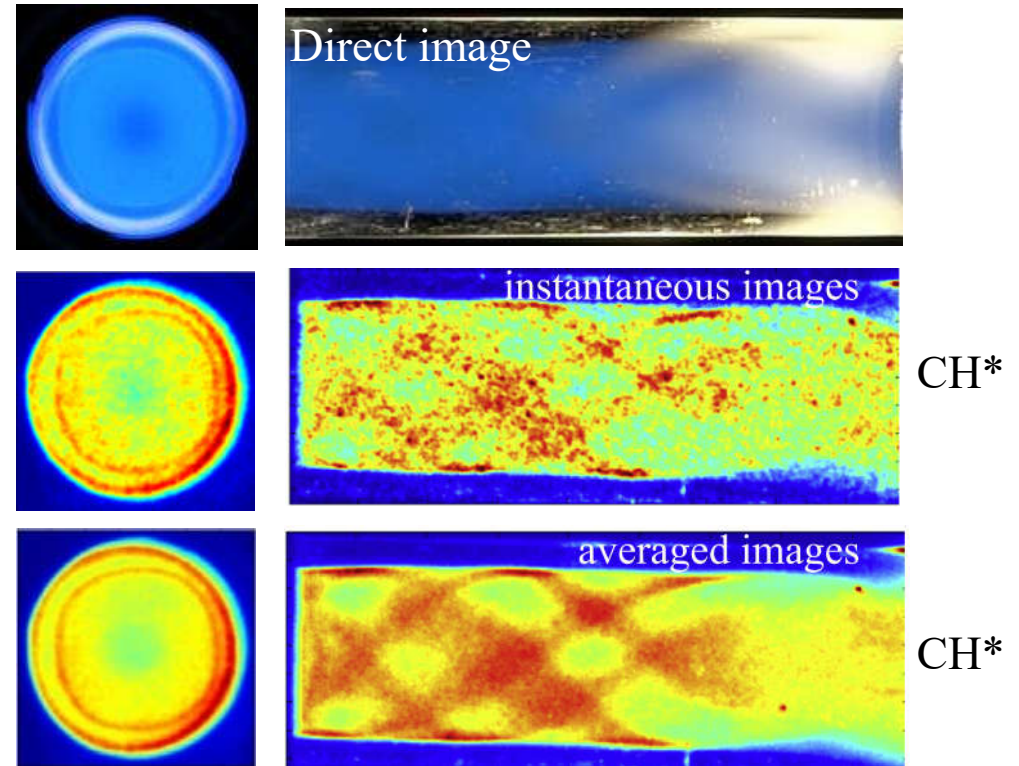


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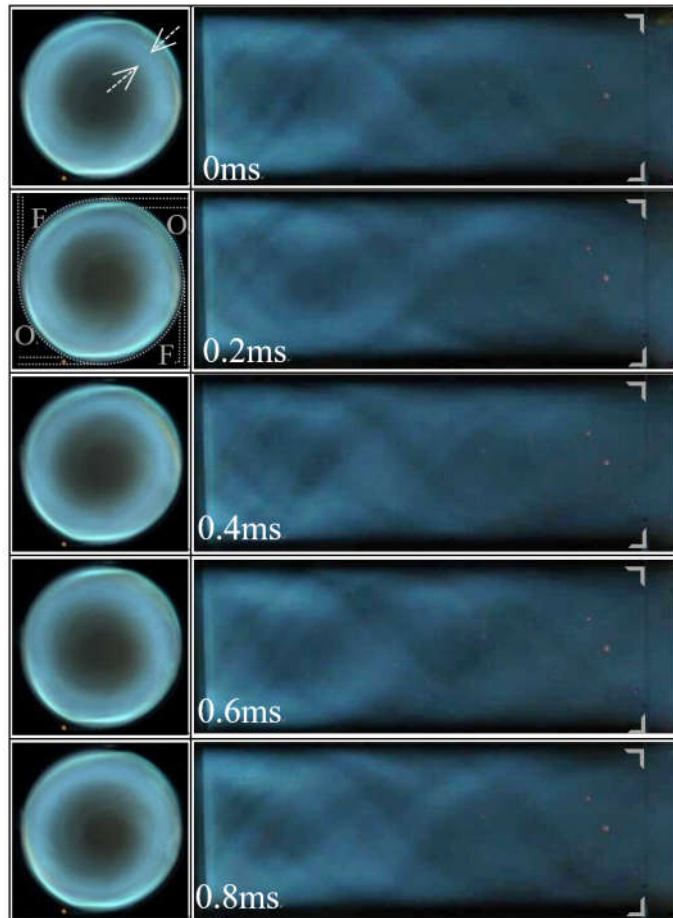
Oxygen mole fraction $\beta \leq 0.5$

Steady, uniform, laminar flame

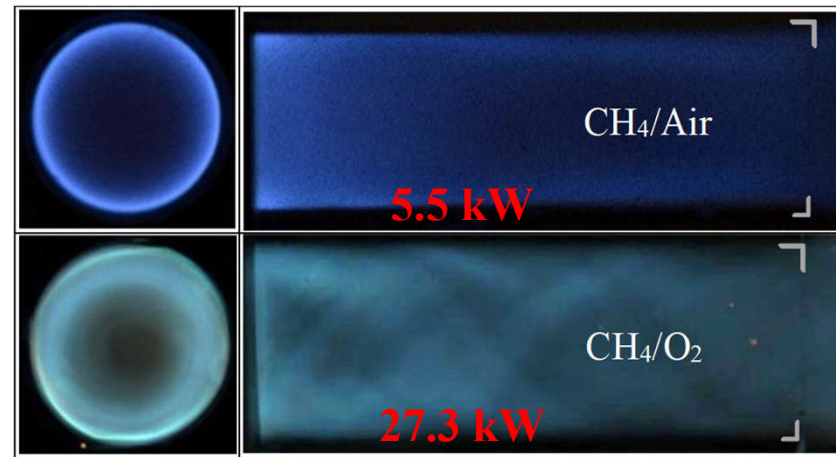


Steady laminar flame, $\beta = 0.67, \Phi = 1.0$

$\beta \geq 0.6$, **non-uniform** laminar flame



$\beta = 1.0, \Phi = 1.0$, steady laminar flame



$Q_0 = 6.0 \text{ m}^3/\text{h}, \Phi = 1.0$

CH_4/Air

$T = 2220 \text{ K}$

$\lambda = 0.25 \text{ W/m}\cdot\text{K}$

$\text{HRR} = 4.5 \times 10^3 \text{ J/cm}^3\cdot\text{s}$

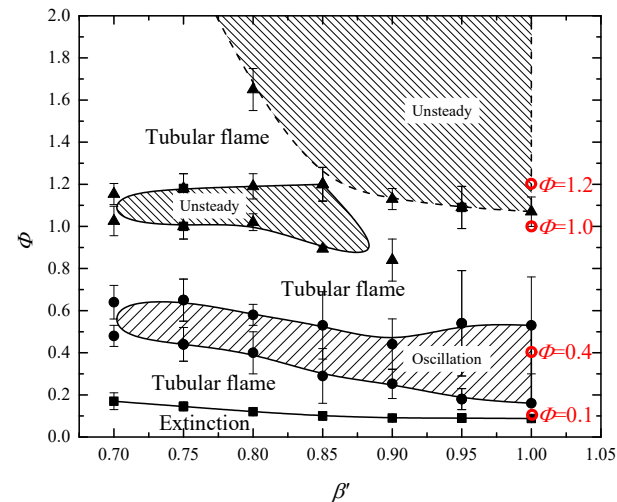
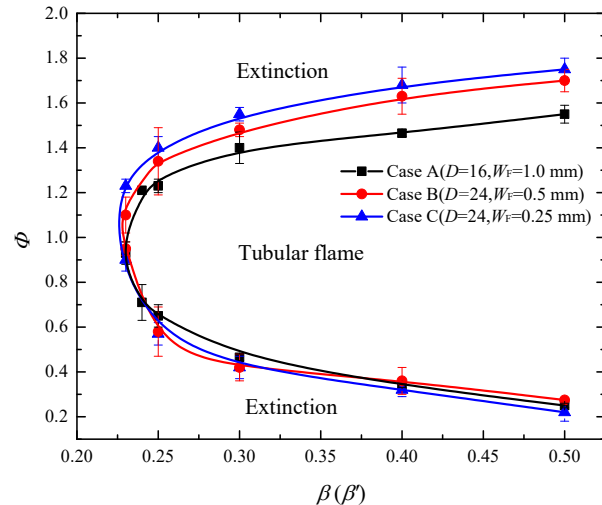
CH_4/O_2

$T = 3050 \text{ K}$

$\lambda = 2.8 \text{ W/m}\cdot\text{K}$

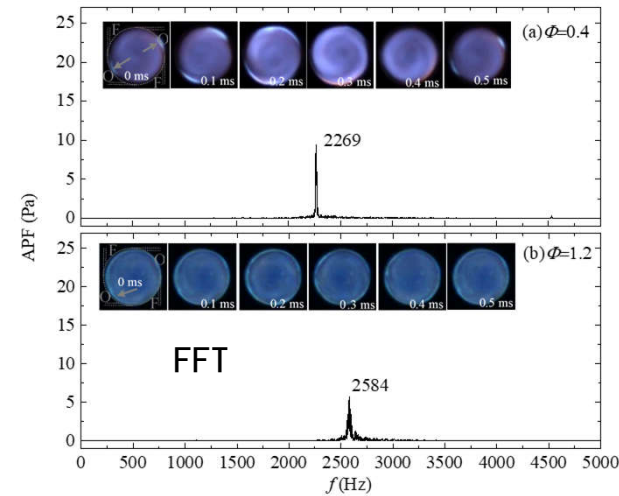
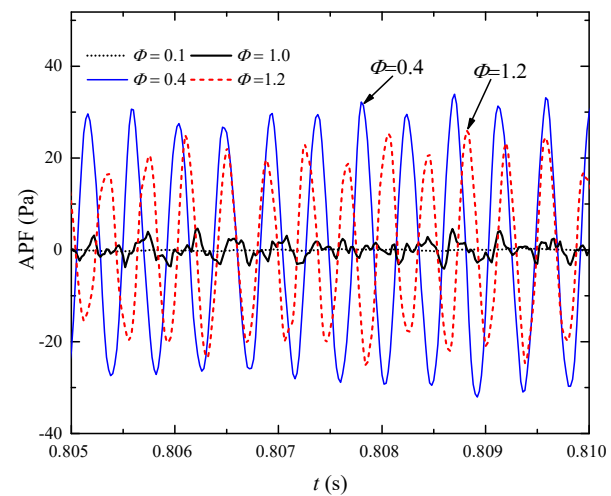
$\text{HRR} = 2.54 \times 10^5 \text{ J/cm}^3\cdot\text{s}$

Reaction time $\approx 22 \mu\text{s}$



Premixed CH_4/O_2 flame
 $\Phi=0.75-1.4$, $T_f \geq 3000$ K

Combustion instability
e.g., $\Phi=0.4, 1.2$



High frequency oscillation,
Axial mode thermal acoustic
 $f_z = (2n_z + 1)c / 4(l + \Delta l)$
owing to **poor mixing**

3

Experimental investigation- D_a



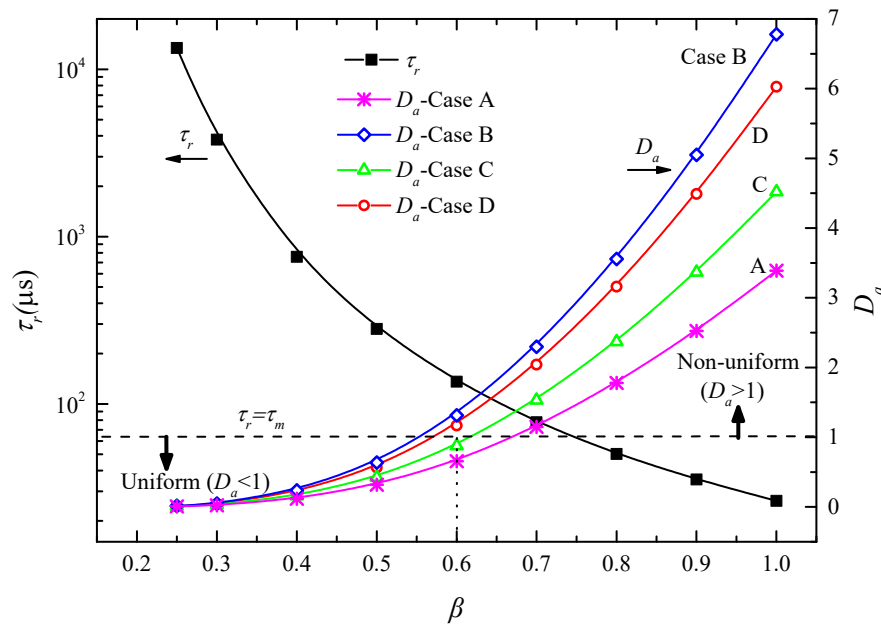
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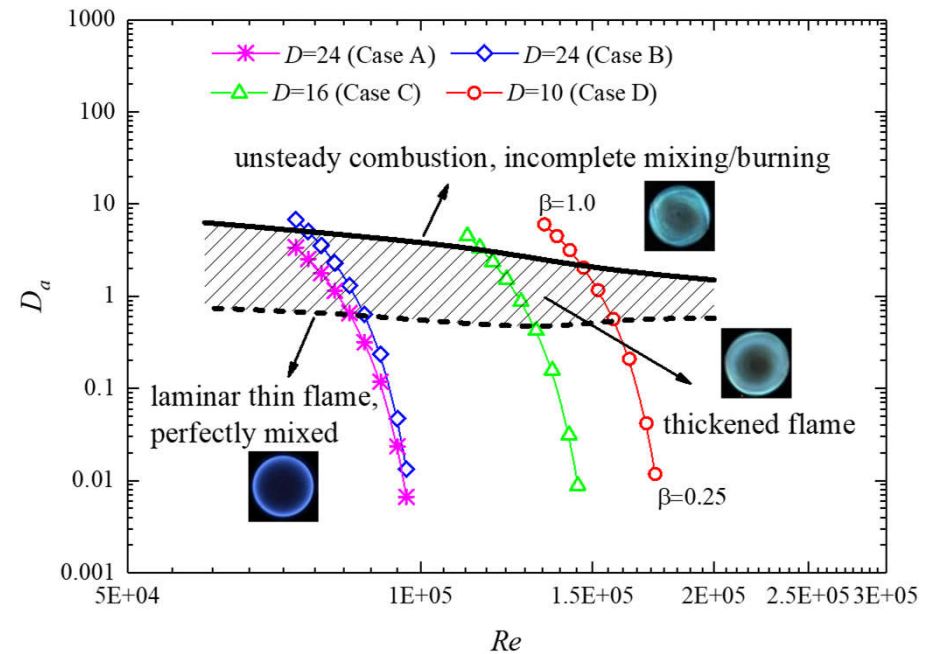
$$D_a \equiv \frac{\tau_m}{\tau_r} = \frac{\text{mixing time}}{\text{reaction time}} \leq \text{or } \approx 1$$

$$\tau_m \equiv \delta_m^2 / D_{mass} \quad \tau_r \equiv \delta_L / S_u$$

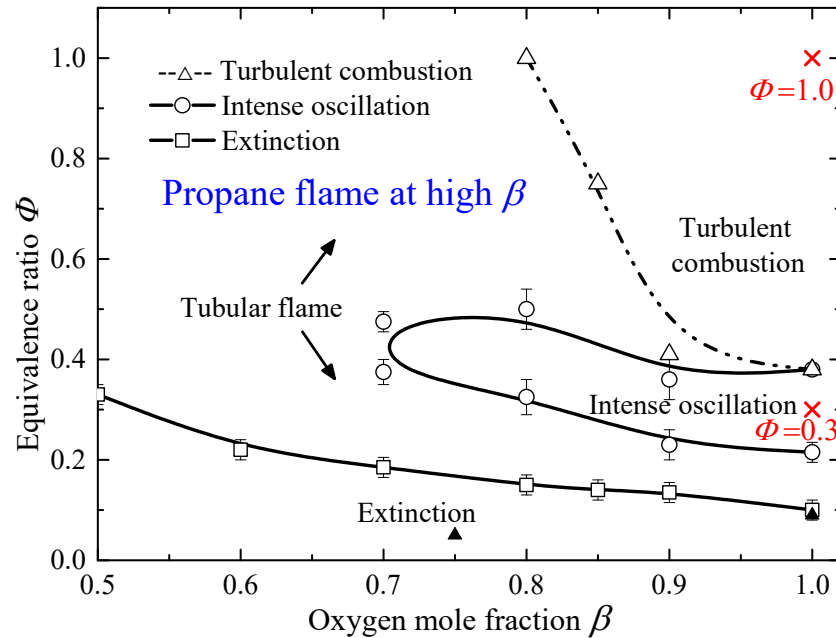
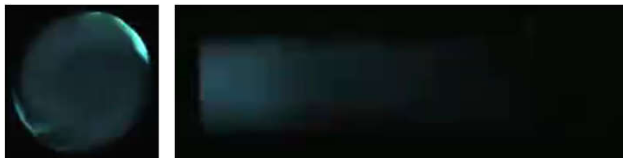
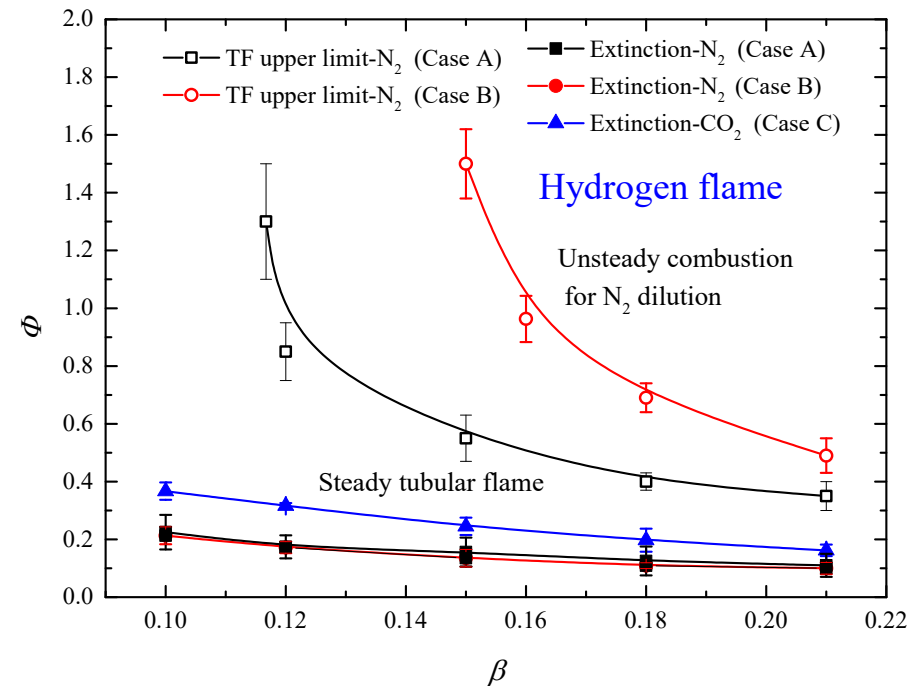
Mixing of fuel/oxidizer should be completed before onset of reaction



D_a in a variety of tests



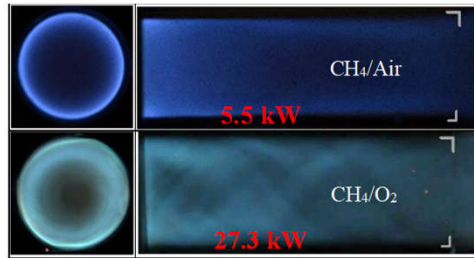
Borghi graph (considering diameter, inlet size, flow rate)

 $\beta = 1.0, \Phi = 0.3$  $\beta = 1.0, \Phi = 1.0$ 

Combustion modes of hydrogen

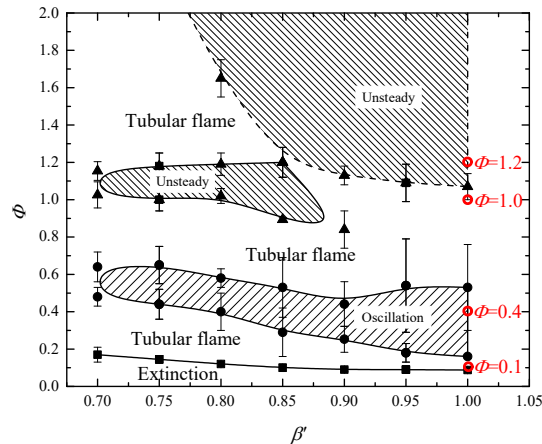
Limited range of β for steady combustion

High burning velocity?


 $Q_O = 6.0 \text{ m}^3/\text{h}, \Phi = 1.0$
CH₄/AirCH₄/O₂

T=2220 K

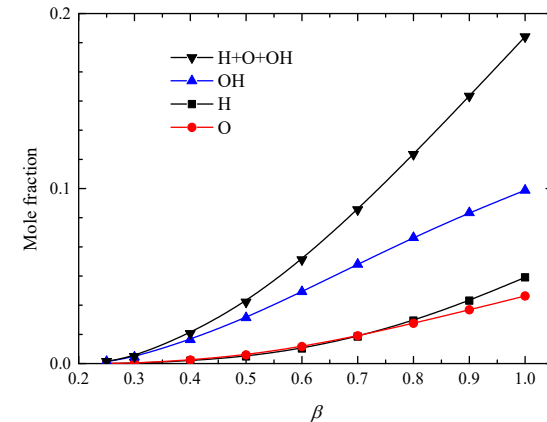
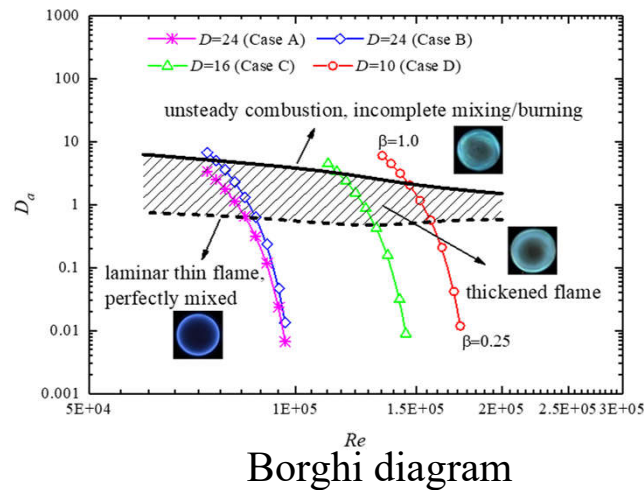
T=3050 K

 $\lambda = 0.25 \text{ W/m}\cdot\text{K}$ $\lambda = 2.8 \text{ W/m}\cdot\text{K}$ HRR=4.5x10³ J/cm³·sHRR=2.54x10⁵ J/cm³·s

Combustion regime (instability)

Benefits of ultrahigh temperature combustion in industry

- Capacity increase
- Fuel saving
- CO₂, NO_x reduction
- Reduce scaling losses
- Quality improvement

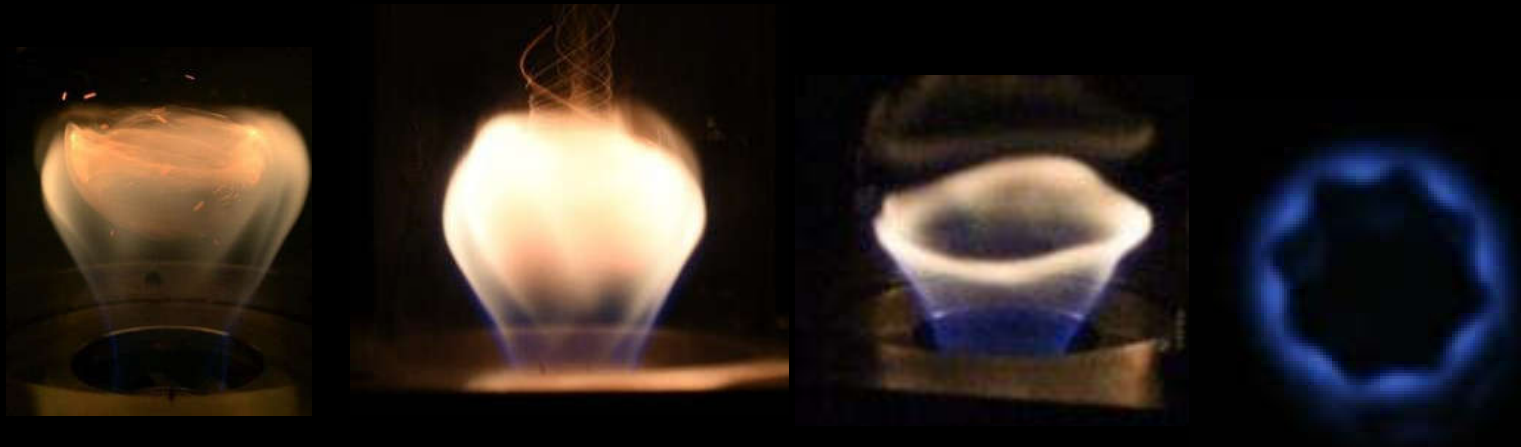
Plenty of active radicals ($\beta=1.0$)

Borghi diagram

Challenges in measurement:

- Detailed flame structure,
- O, H, OH radicals,
- Temperature,
- Emissions...

Acknowledgement



NSFC: No. 51676016 , 91641204
Prof. Ishizuka & my team members!