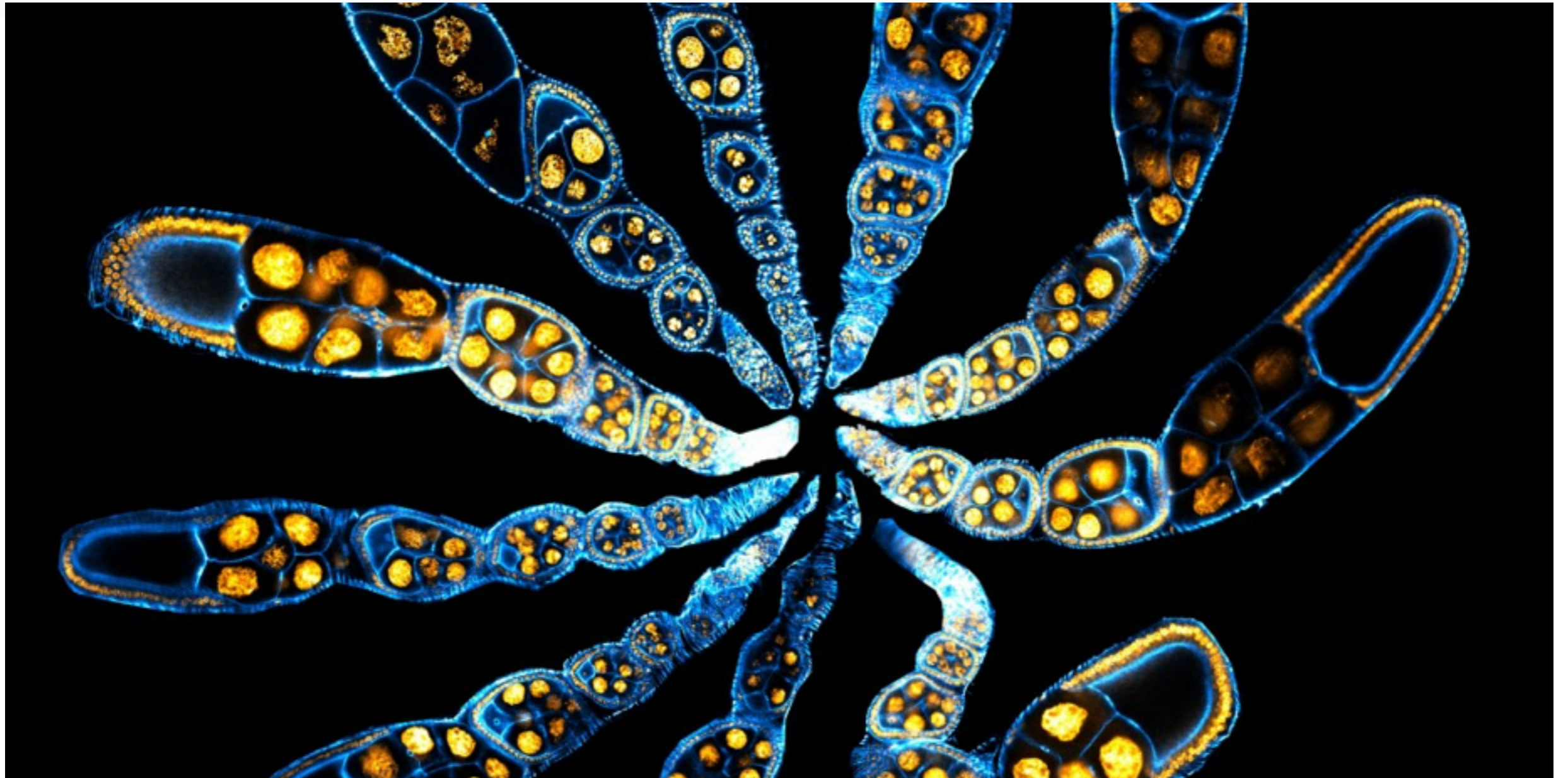


# BIOENGINEERING DAY 2015

Princeton University October 2



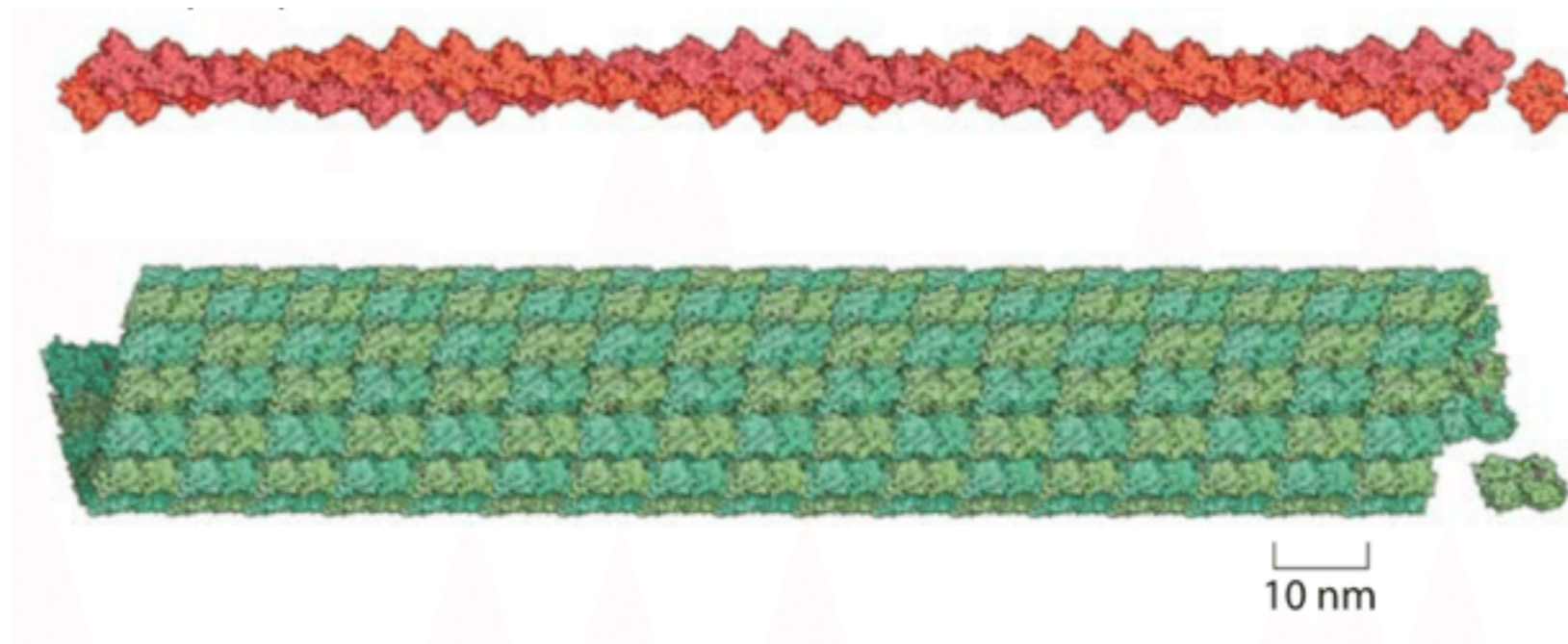
<http://bioeng.princeton.edu/bioengineering-day/>

## MAE 545: Lecture 5 (10/1)

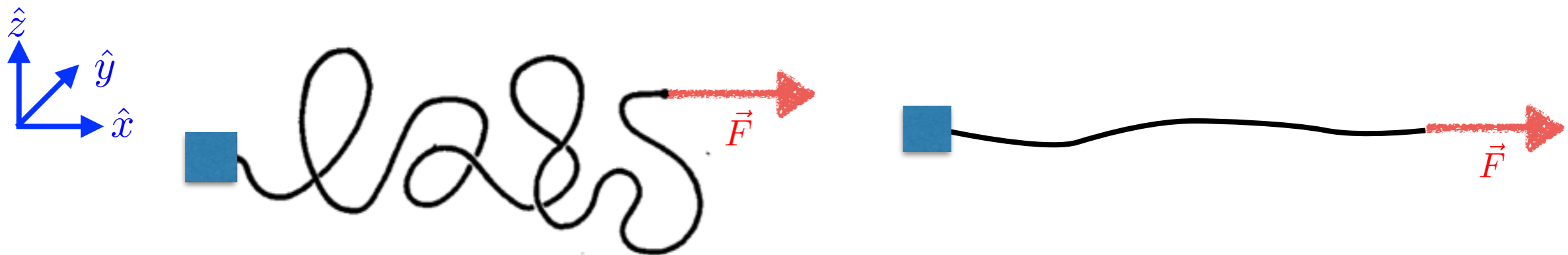
# Statistical mechanics of proteins (continued)



## Dynamics of actin filaments and microtubules



# Stretching of worm-like chains



**Small force**

$$F\ell_p \ll k_B T$$

$$\langle x \rangle \approx L \frac{2F\ell_p}{3k_B T}$$

**Large force**

$$F\ell_p \gg k_B T$$

$$\langle x \rangle \approx L \left[ 1 - \sqrt{\frac{k_B T}{4F\ell_p}} \right]$$

**Approximate expression that interpolates between both regimes**

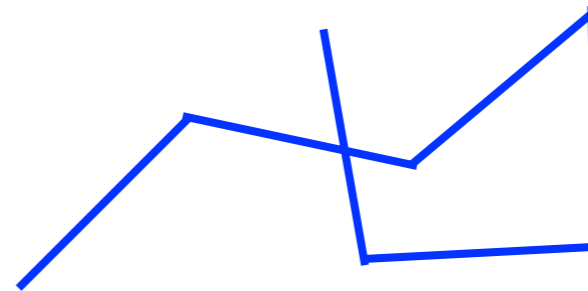
$$\frac{F\ell_p}{k_B T} = \frac{1}{4} \left( 1 - \frac{\langle x \rangle}{L} \right)^{-2} - \frac{1}{4} + \frac{\langle x \rangle}{L}$$

J.F. Marko and E.D. Siggia,  
Macromolecules 28, 8759-8770 (1995)

# Steric interactions

So far we ignored interactions between different chain segments, but in reality the chain cannot pass through itself due to steric interactions.

Example of forbidden configuration in 2D



Polymer chains are realizations of self-avoiding random walks!

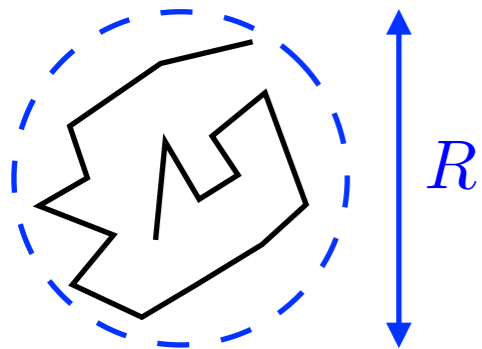


Steric interactions are important for long polymers in the absence of pulling forces



Steric interactions are not important in the presence of pulling forces.

# Mean field estimate for the radius of self-avoiding polymers



**Approximate partition function: estimate number of self-avoiding random walks of  $N$  steps of size  $a$  that are restricted to a sphere of radius  $R$ .**

$$Z(R, N) \approx g^N \times \frac{e^{-3R^2/2Na^2}}{[2\pi Na^2/3]^{3/2}} \times \underbrace{\left[ 1 \cdot \left(1 - \frac{a^3}{R^3}\right) \cdot \left(1 - \frac{2a^3}{R^3}\right) \cdots \left(1 - \frac{(N-1)a^3}{R^3}\right) \right]}_{C_{ev}}$$

total number of random walks

reduction in entropy when constrained to sphere of radius R

reduction in entropy due to excluded volume

## Excluded volume effect

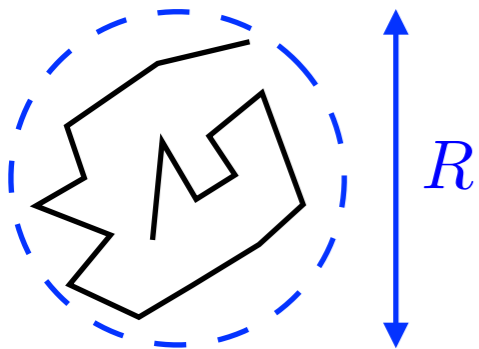
$$\ln C_{ev} = \sum_{k=1}^{N-1} \ln \left( 1 - \frac{ka^3}{R^3} \right) \approx \sum_{k=1}^{N-1} \left( -\frac{ka^3}{R^3} - \frac{k^2 a^6}{2R^6} - \cdots \right) \approx -\frac{N^2 a^3}{2R^3} - \frac{N^3 a^6}{6R^6}$$

## Approximate partition function

$$\ln Z(R, N) \approx N \ln g - \frac{3}{2} \ln(2\pi Na^2/3) - \frac{3R^2}{2Na^2} - \frac{N^2 a^3}{2R^3} - \frac{N^3 a^6}{6R^6}$$

Paul  
Flory

# Relation between partition function and free energy



## Statistical mechanics

$$Z = \sum_c e^{-E_c/k_B T} = e^{-G/k_B T} \longrightarrow G = -k_B T \ln Z$$

## Approximate partition function

$$\ln Z(R, N) \approx N \ln g - \frac{3}{2} \ln(2\pi N a^2 / 3) - \frac{3R^2}{2Na^2} - \underbrace{\frac{N^2 a^3}{2R^3} + \frac{N^3 a^6}{6R^6}}$$

reduction in entropy  
when constrained to  
sphere of radius R

reduction in entropy  
due to excluded  
volume interactions

## Free energy cost for constraining polymer to sphere of radius $R$

$$\Delta G(R, N) = G_{\text{ent}}(R, N) + G_{\text{int}}(R, N)$$

$$G_{\text{ent}}(R, N) = \frac{3k_B T R^2}{2Na^2}$$

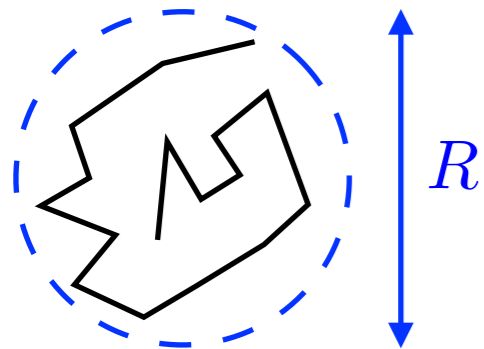
$$G_{\text{int}}(R, N) = \frac{k_B T N^2 a^3}{2R^3} + \frac{k_B T N^3 a^6}{6R^6}$$

**Estimate polymer radius by maximizing the partition function or equivalently by minimizing the free energy!**

Paul Flory

# Mean field estimate for the radius of self-avoiding polymers

(higher order term can be ignored)

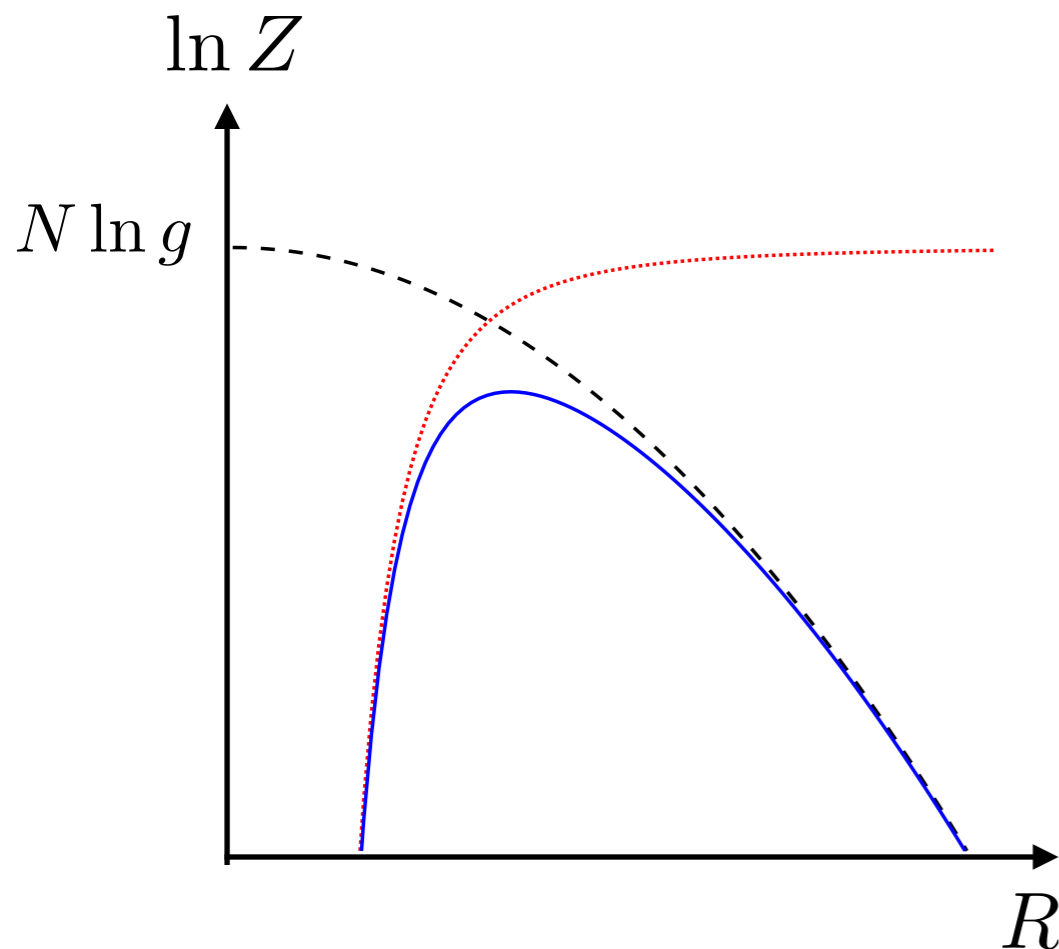


Approximate partition function

$$\ln Z(R, N) \approx N \ln g - \frac{3}{2} \ln(2\pi N a^2 / 3) - \frac{3R^2}{2Na^2} - \frac{N^2 a^3}{2R^3} - \frac{N^3 a^6}{6R^6}$$

Estimate polymer radius by maximizing the partition function

$$\frac{\partial \ln Z(R, N)}{\partial R} \approx -\frac{3R}{Na^2} + \frac{3}{2} \frac{N^2 a^3}{R^4} = 0$$



$$R \sim a N^\nu \sim \ell_p \left( \frac{L}{\ell_p} \right)^\nu$$

**Flory exponent  $\nu = 3/5$**

Exact result from more sophisticated methods

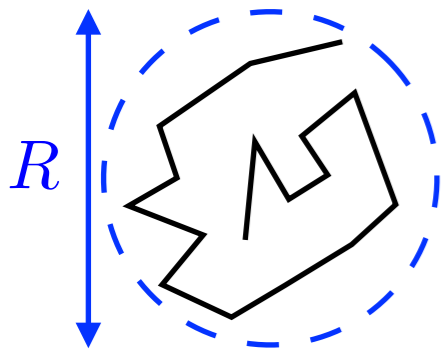
$$\nu \approx 0.591$$

non-avoiding random walks

$$\nu = 1/2$$

Paul  
Flory

# Self-avoiding walks in $d$ dimensions



## Approximate partition function

$$Z(R, N) \approx g^N \times \frac{e^{-dR^2/2Na^2}}{[2\pi Na^2/d]^{d/2}} \times \left[ 1 \cdot \left(1 - \frac{a^d}{R^d}\right) \cdot \left(1 - \frac{2a^d}{R^d}\right) \cdots \left(1 - \frac{(N-1)a^d}{R^d}\right) \right]$$

$$\ln Z(R, N) \approx N \ln g - \frac{d}{2} \ln(2\pi Na^2/d) - \frac{dR^2}{2Na^2} - \frac{N^2 a^d}{2R^d}$$

## Estimate $R$ by maximizing the partition function

$$\frac{\partial \ln Z(R, N)}{\partial R} \approx -\frac{dR}{Na^2} + \frac{d N^2 a^d}{2 R^{d+1}} = 0$$

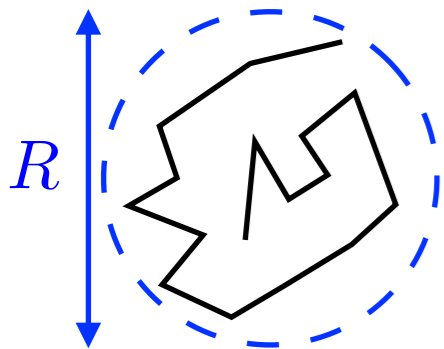
$$R \sim aN^\nu \quad \nu = \frac{3}{d+2}$$

**For  $d \geq 4$  Flory exponent is  $\nu \leq 1/2$ , but for non-avoiding walk  $\nu = 1/2$ .**

**What is then the expected scaling for radius  $R$ ?**

Paul Flory

# Self-avoiding walks in $d$ dimensions



## Approximate partition function

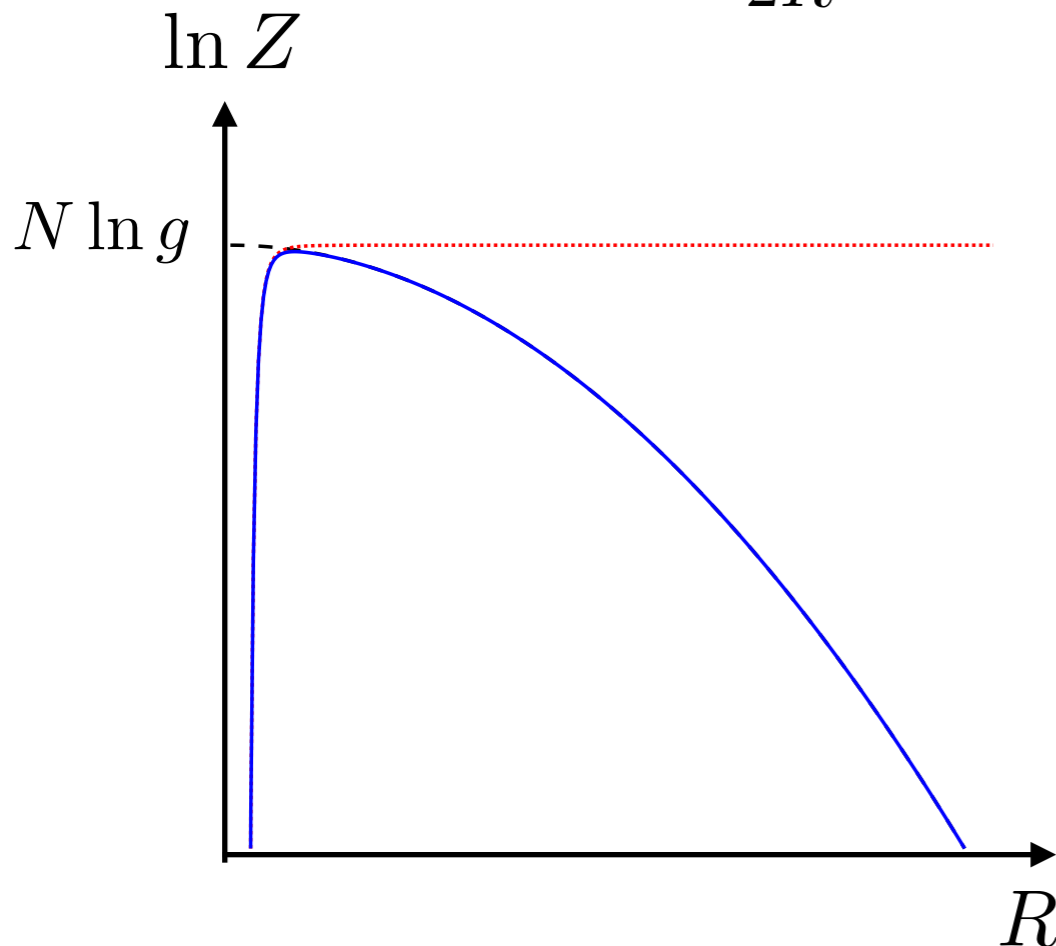
$$\ln Z(R, N) \approx N \ln g - \frac{d}{2} \ln(2\pi N a^2 / d) - \frac{dR^2}{2Na^2} - \frac{N^2 a^d}{2R^d}$$

Estimate free energy contributions when  $R \sim aN^{1/2}$

$$G_{\text{ent}} = k_B T \frac{dR^2}{2Na^2} \sim k_B T$$

$$G_{\text{int}} = k_B T \frac{N^2 a^d}{2R^d} \sim k_B T N^{(4-d)/2}$$

Excluded volume interactions are only important for  $d < 4$ !



## Flory estimate

$$R \sim aN^\nu$$

$$d \leq 4 \quad \nu = \frac{3}{d+2}$$

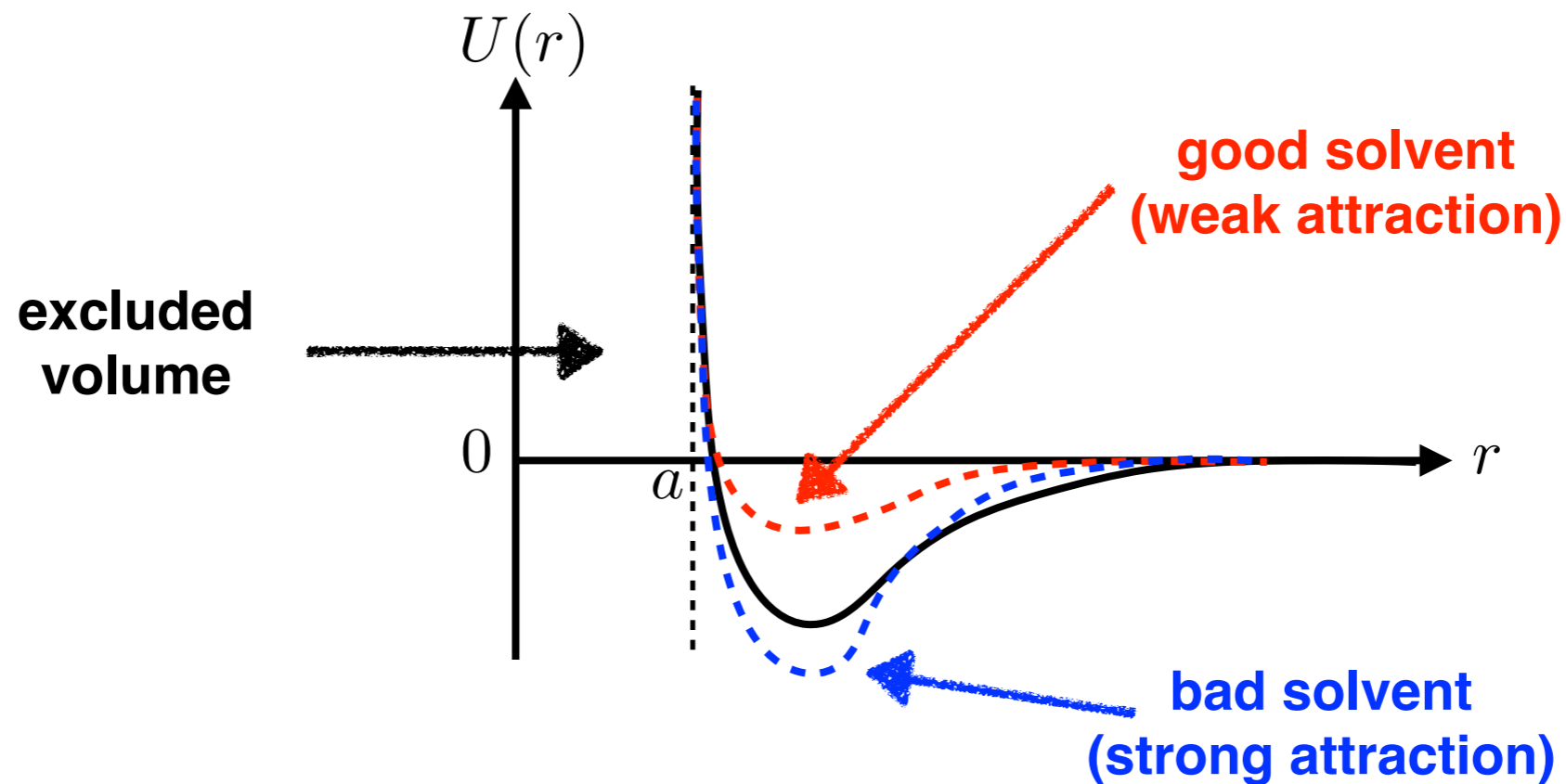
$$d \geq 4 \quad \nu = \frac{1}{2}$$

$d$	1	2	3	$\geq 4$
$\nu$	1	3/4	3/5	1/2

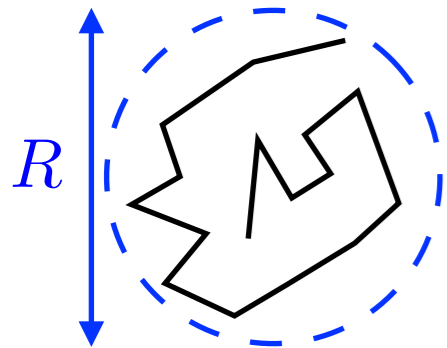
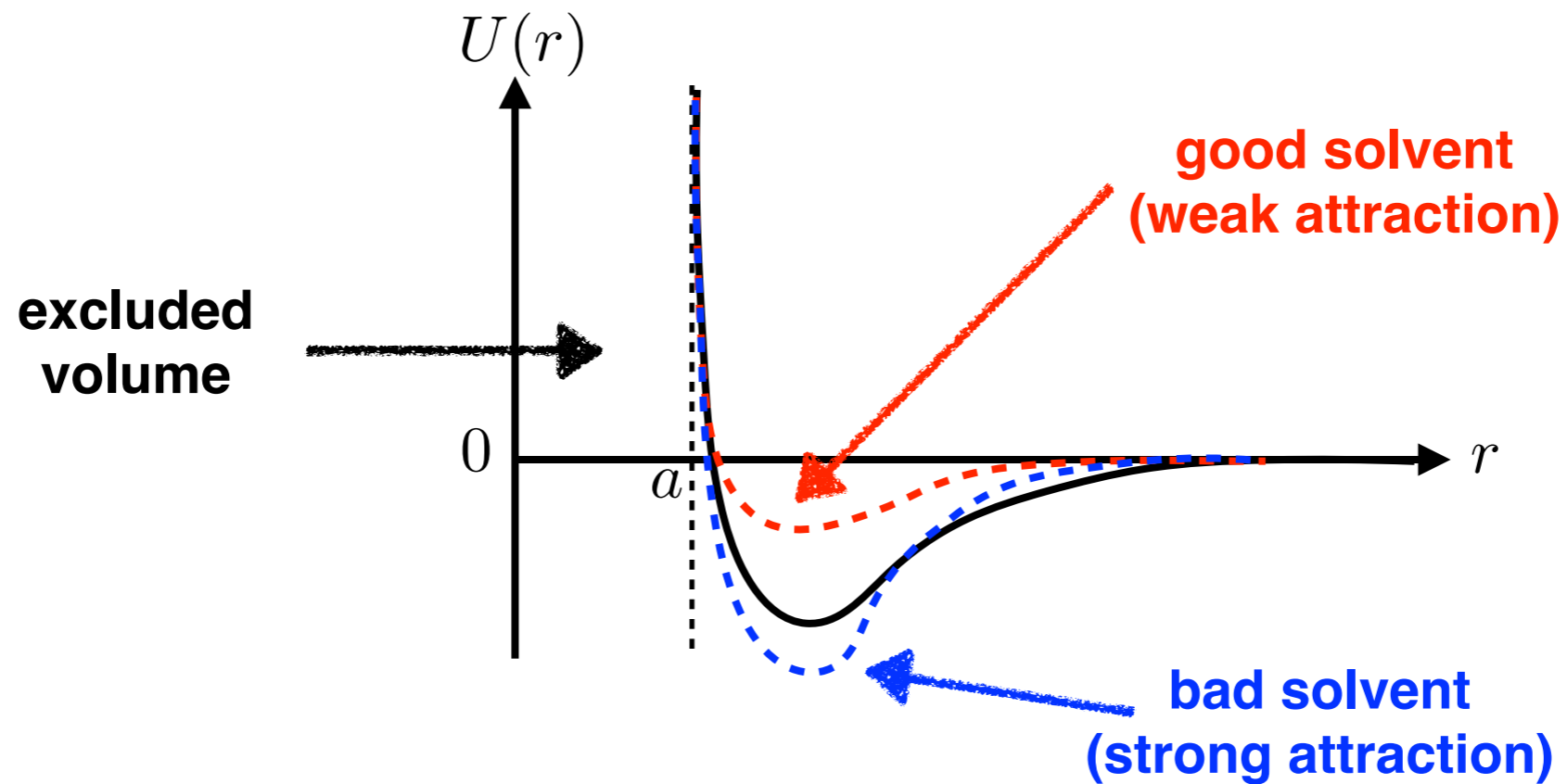
Note: except for  $d=3$  these exponents are exact!

# Interacting polymers

Now let us include also other interactions between polymer chains, e.g. van der Waals interactions. Interactions are typically attractive and their magnitude can be modulated by the choice of solvent.



# Interacting polymers



## Mean field approximation for the total attraction energy

$$E_{\text{att}} = \frac{1}{2} \sum_{i \neq j} U(\vec{r}_i - \vec{r}_j) \approx \frac{1}{2} \int d^3 \vec{r} d^3 \vec{r}' \rho(\vec{r}) \rho(\vec{r}') U(\vec{r} - \vec{r}') \quad \rho(\vec{r}) \text{ polymer density}$$

Assuming uniform polymer density  $\rho(\vec{r}) = N/V \sim N/R^3$

$$E_{\text{att}} = \frac{N^2}{2V} \int_{r>a} d^3 \vec{r} U(\vec{r}) \equiv -k_B T \chi N^2 a^3 / R^3$$

Flory-Huggins parameter  $\chi = -\frac{\int_{r>a} d^3 \vec{r} U(\vec{r})}{2a^3 k_B T}$

Excluded volume effects will be treated separately.

# Interacting polymers

## Mean field approximation for the partition function

$$Z(R, N) \approx g^N \times \frac{e^{-3R^2/2Na^2}}{[2\pi Na^2/3]^{3/2}} \times \left[ 1 \cdot \left(1 - \frac{a^3}{R^3}\right) \cdot \left(1 - \frac{2a^3}{R^3}\right) \cdots \left(1 - \frac{(N-1)a^3}{R^3}\right) \right] \times e^{-E_{\text{att}}/k_B T}$$

$$\ln Z(R, N) \approx N \ln g - \frac{3}{2} \ln(2\pi Na^2/3) - \frac{3R^2}{2Na^2} - \frac{N^2 a^3}{2R^3} - \frac{N^3 a^6}{6R^6} + \chi N^2 \frac{a^3}{R^3}$$

attraction

$$\ln Z(R, N) \approx N \ln g - \frac{3}{2} \ln(2\pi Na^2/3) - \frac{3R^2}{2Na^2} - \left(\frac{1}{2} - \chi\right) \frac{N^2 a^3}{R^3} - \frac{N^3 a^6}{6R^6}$$

**Note:**  $\chi(T)$  is typically a decreasing function of temperature and the coefficient  $(1/2 - \chi)$  in equation above changes sign at the so called  $\theta$  temperature, where  $\chi(\theta) = 1/2$ .

At large temperatures, where  $\chi < 1/2$ , polymers are in swollen coil state.

$$R \sim (1/2 - \chi)^{1/5} a N^{3/5}$$

average density  $\bar{\rho} \sim \frac{N}{R^3} \sim N^{-4/5} \rightarrow 0$

Exactly at  $\theta$  temperature, where  $\chi = 1/2$ , attractive interactions and excluded volume are balanced.

$$R \sim a N^{1/2}$$

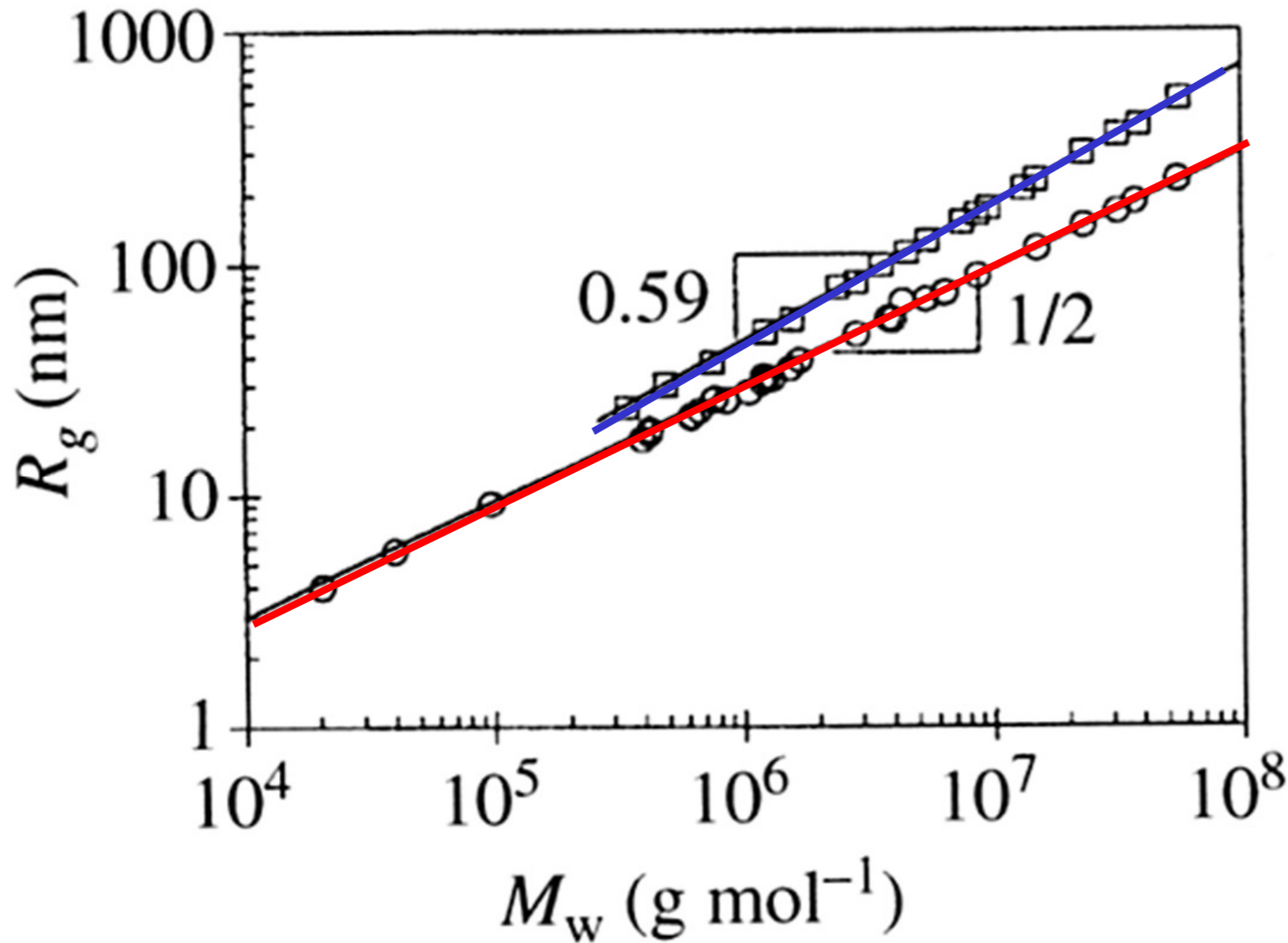
average density  $\bar{\rho} \sim N^{-1/2} \rightarrow 0$

# Good solvent - theta solvent

gyration  
radius

$$R_g^2 = \frac{1}{N} \left\langle \sum_{k=1}^N (\vec{r}_k - \vec{r}_{\text{mean}})^2 \right\rangle$$

$$\vec{r}_{\text{mean}} = \frac{1}{N} \sum_{k=1}^N \vec{r}_k$$



polystyrene in benzene  
(good solvent)

$$\chi < 1/2$$

$$R \sim N^{0.59}$$

polystyrene in cyclohexane  
(theta solvent)

$$\chi = 1/2$$

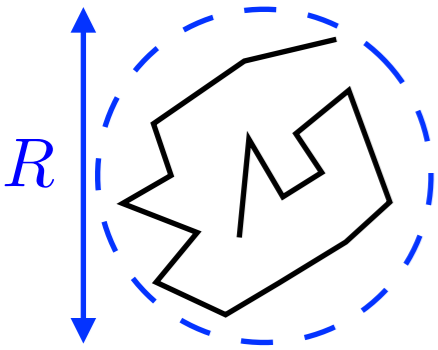
$$R \sim N^{1/2}$$

molecular weight  
of polystyrene  $\sim N$

L.J. Fetters *et al.*, J. Phys.  
Chem. 23, 619-640 (1994)

# Swollen coil to globule transition

At low temperatures, where  $\chi > 1/2$ , polymers are in compact globule state with finite density  $\rho \sim N/R^3$



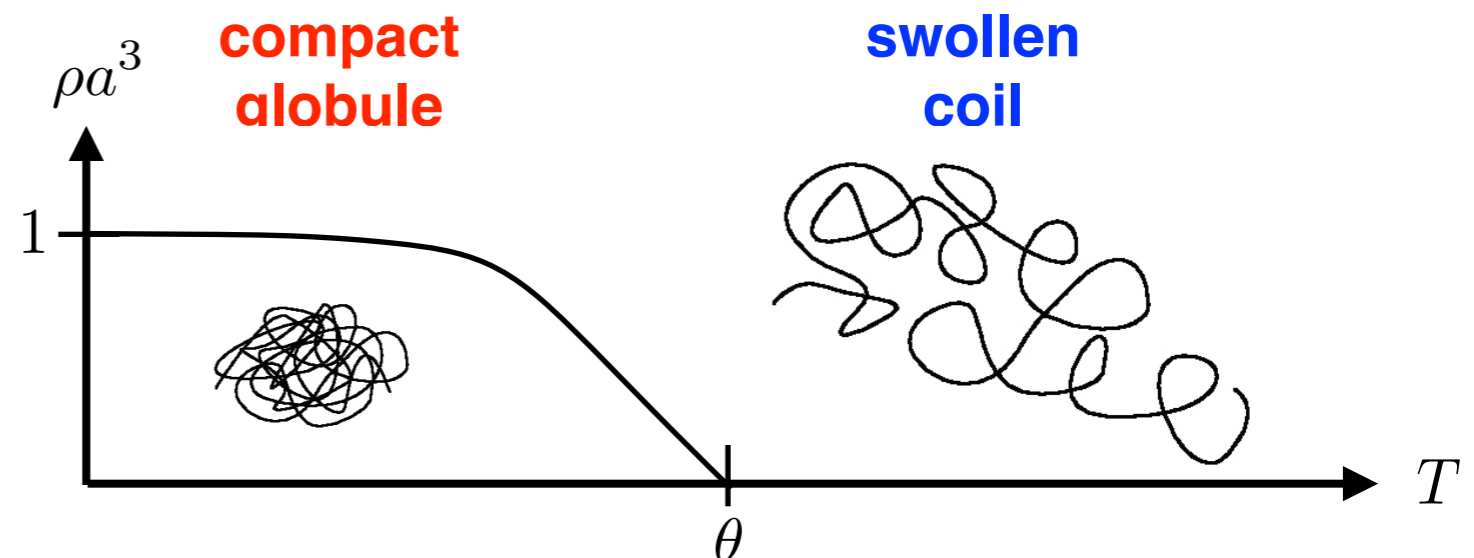
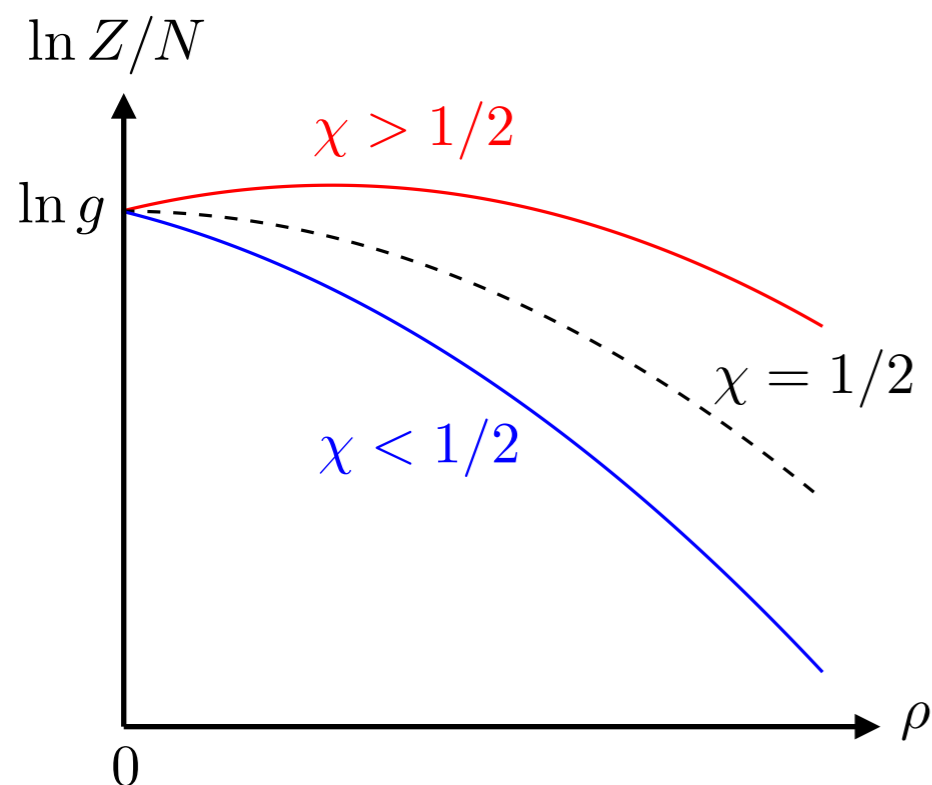
$$\frac{\ln Z(R, N)}{N} \approx \ln g - \frac{3R^2}{2N^2 a^2} - \left(\frac{1}{2} - \chi\right) \frac{Na^3}{R^3} - \frac{N^2 a^6}{6R^6}$$

(higher order term can be ignored)

$$\frac{\ln Z(\rho, N)}{N} \approx \ln g + \left(\chi - \frac{1}{2}\right) \rho a^3 - \frac{\rho^2 a^6}{6}$$

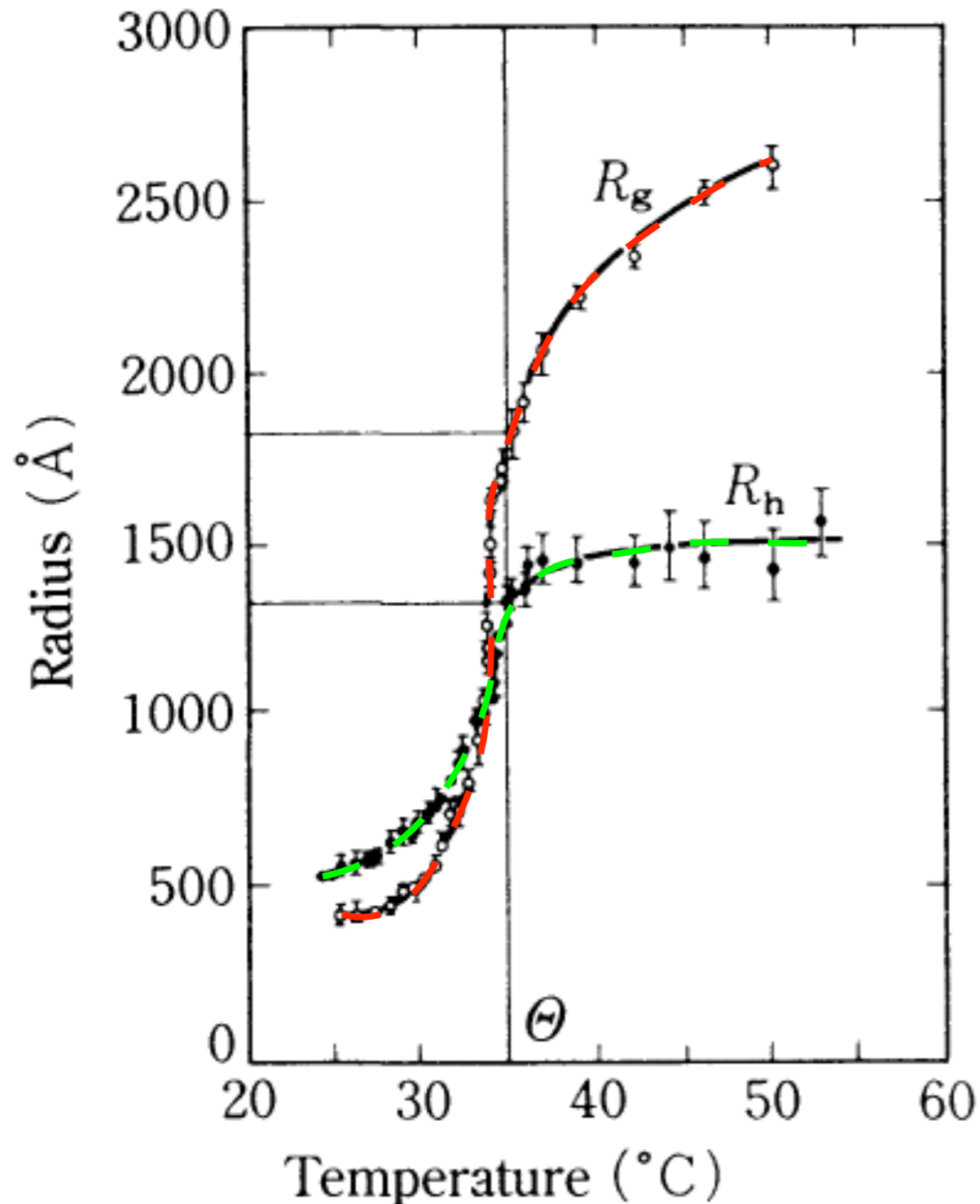
Average density of the compact globule is obtained by maximizing entropy

$$\rho \sim \left(\chi - \frac{1}{2}\right) a^{-3}$$



# Swollen coil to globule transition

polystyrene in cyclohexane



**gyration radius**

$$R_g^2 = \frac{1}{N} \left\langle \sum_{k=1}^N (\vec{r}_k - \vec{r}_{\text{mean}})^2 \right\rangle$$

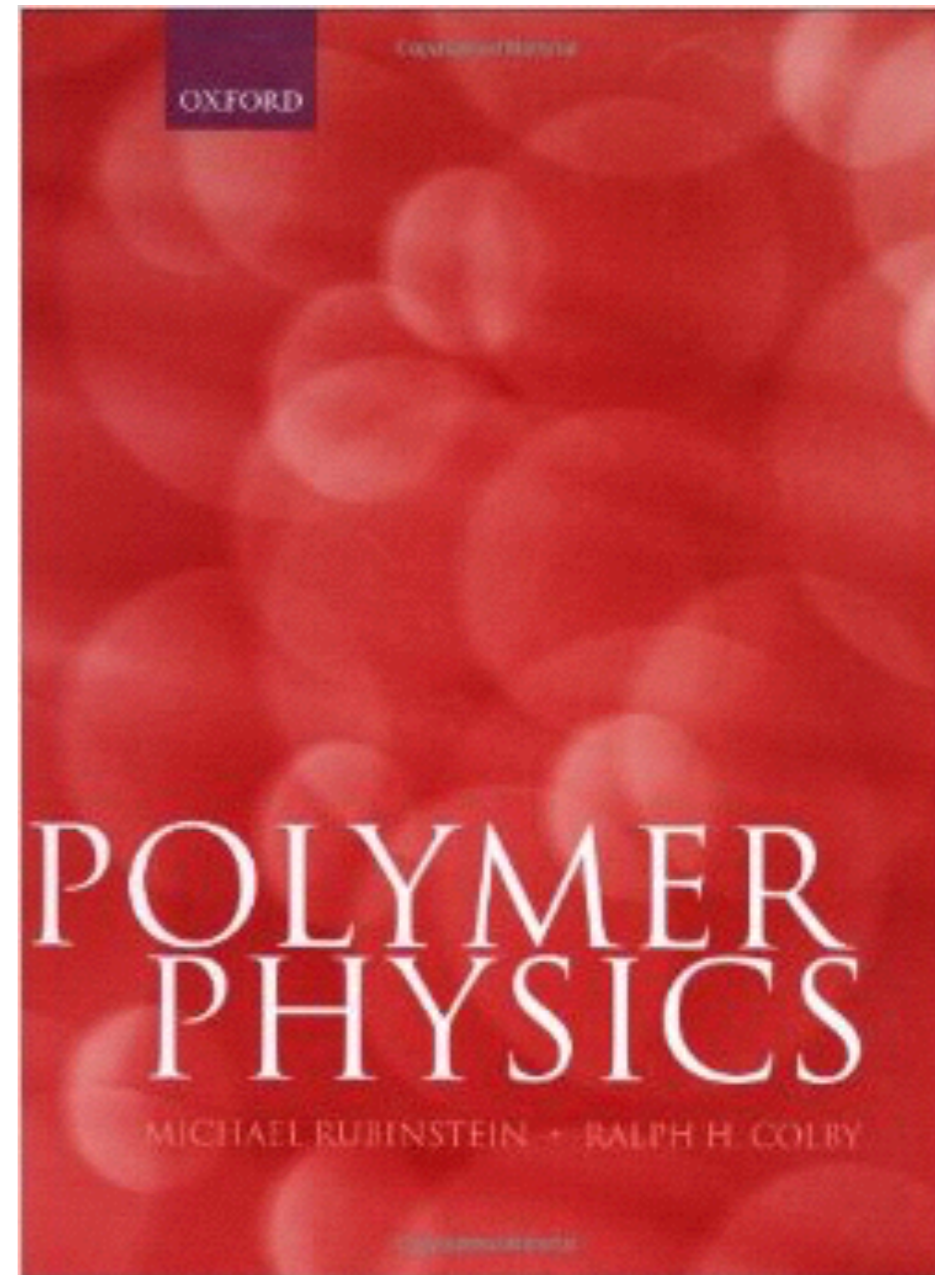
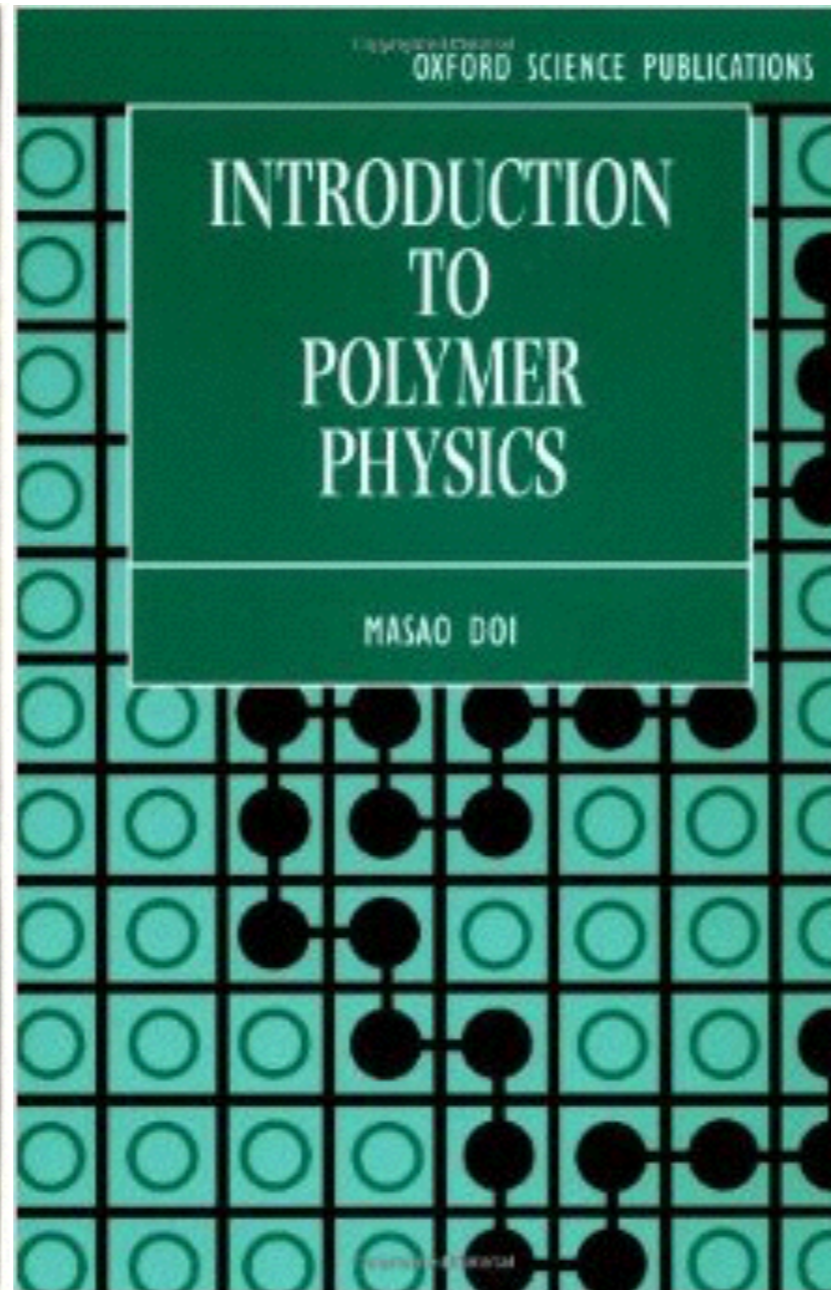
$$\vec{r}_{\text{mean}} = \frac{1}{N} \sum_{k=1}^N \vec{r}_k$$

**hydrodynamic radius**

$$R_h = \frac{k_B T}{6\pi\eta D}$$

S.T. Sun *et al.*, J. Chem. Phys. 73, 5971 (1980)

# Further reading

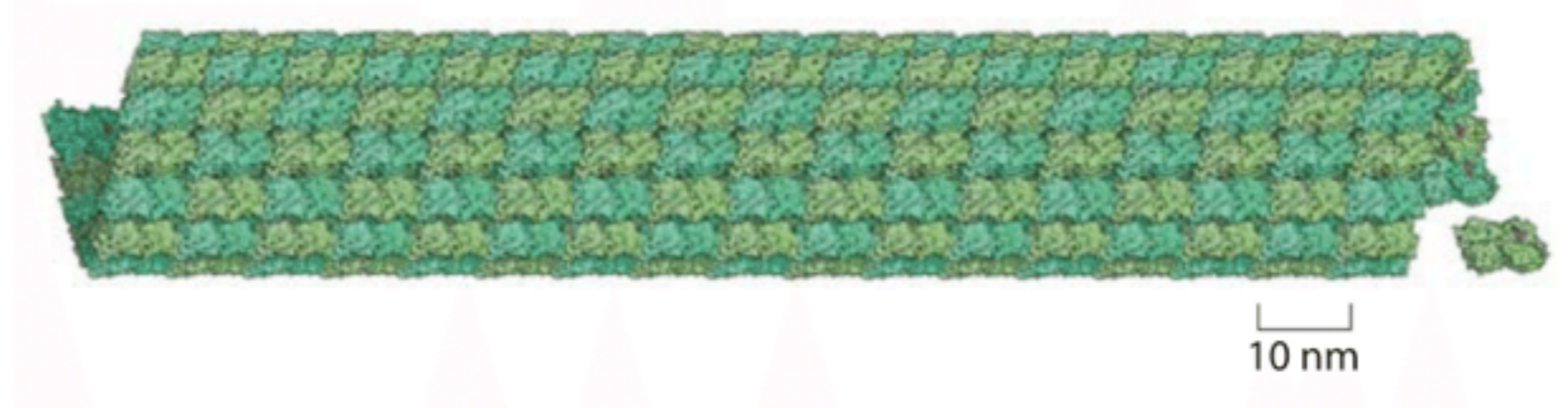


# Dynamics of actin filaments and microtubules

**Actin filament**

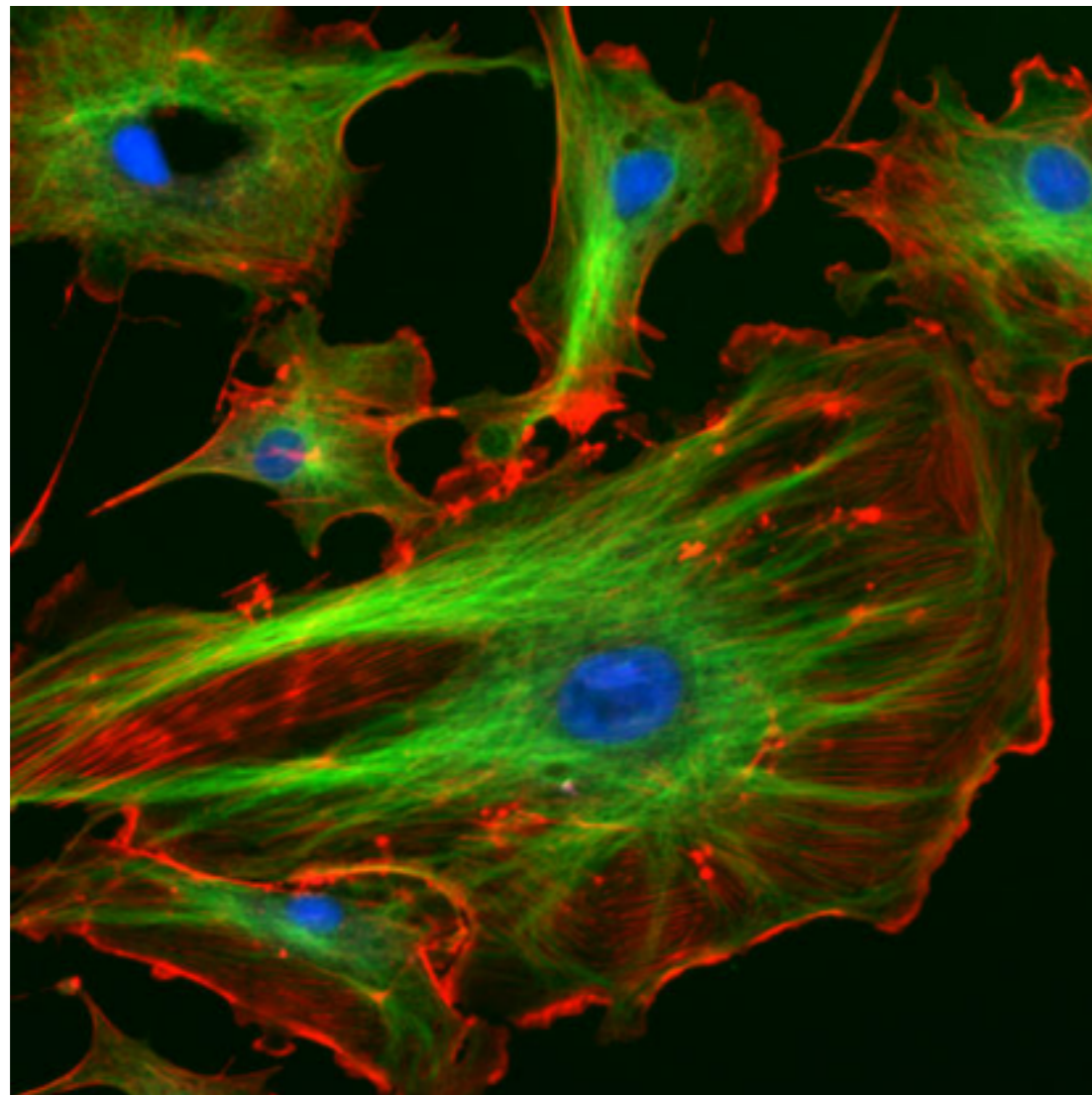


**Microtubule**

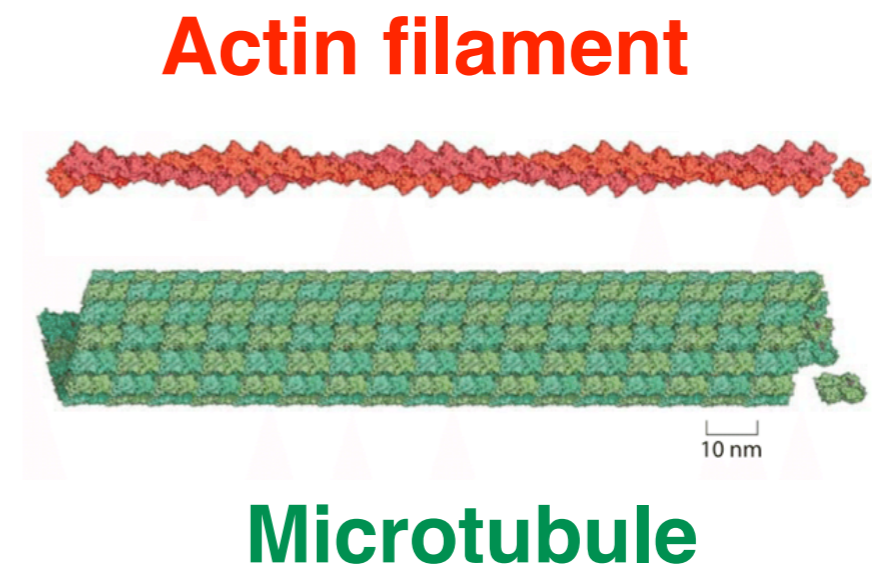


# Cytoskeleton in cells

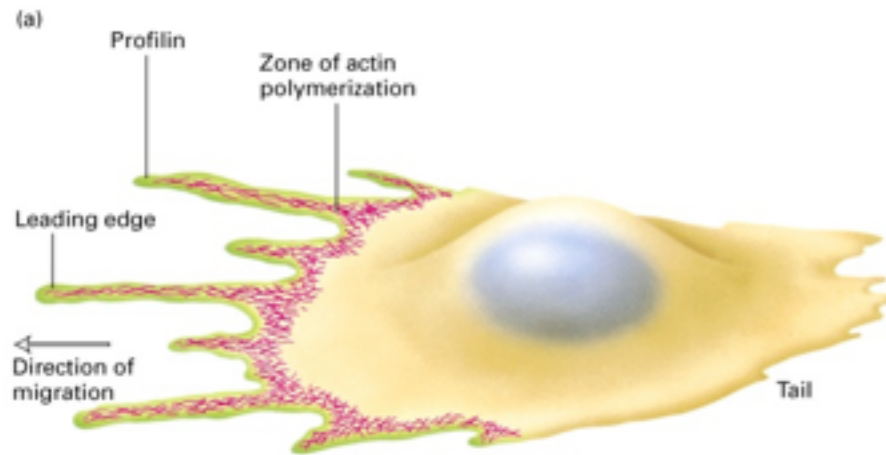
Cytoskeleton matrix gives the cell shape and mechanical resistance to deformation.



(wikipedia)



# Crawling of cells



**migration of skin cells during wound healing**

**spread of cancer cells during metastasis of tumors**

**amoeba searching for food**

**Immune system:  
neutrophils chasing bacteria**

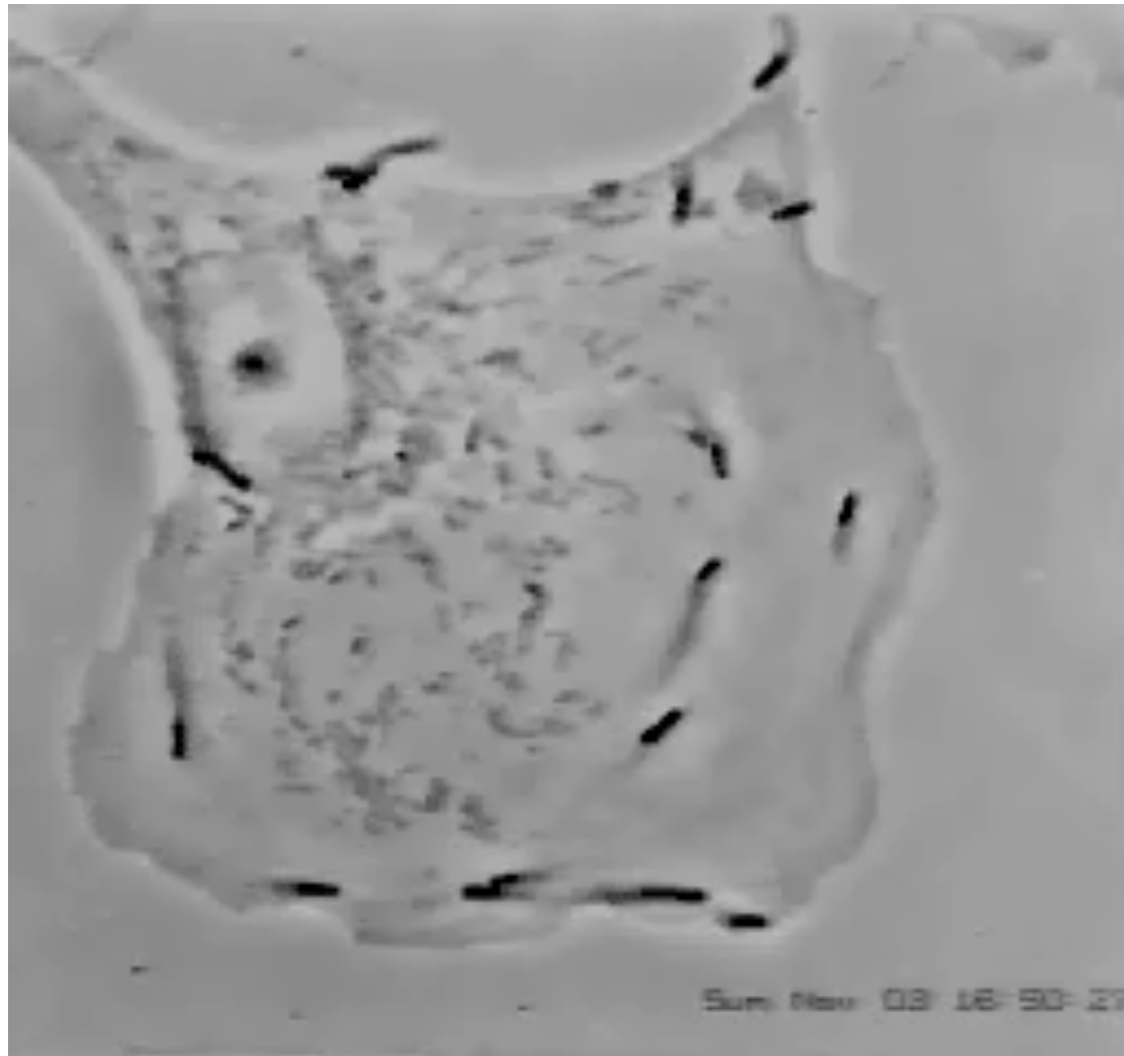


**David Rogers, 1950s**

$$v \sim 0.1 \mu\text{m/s}$$

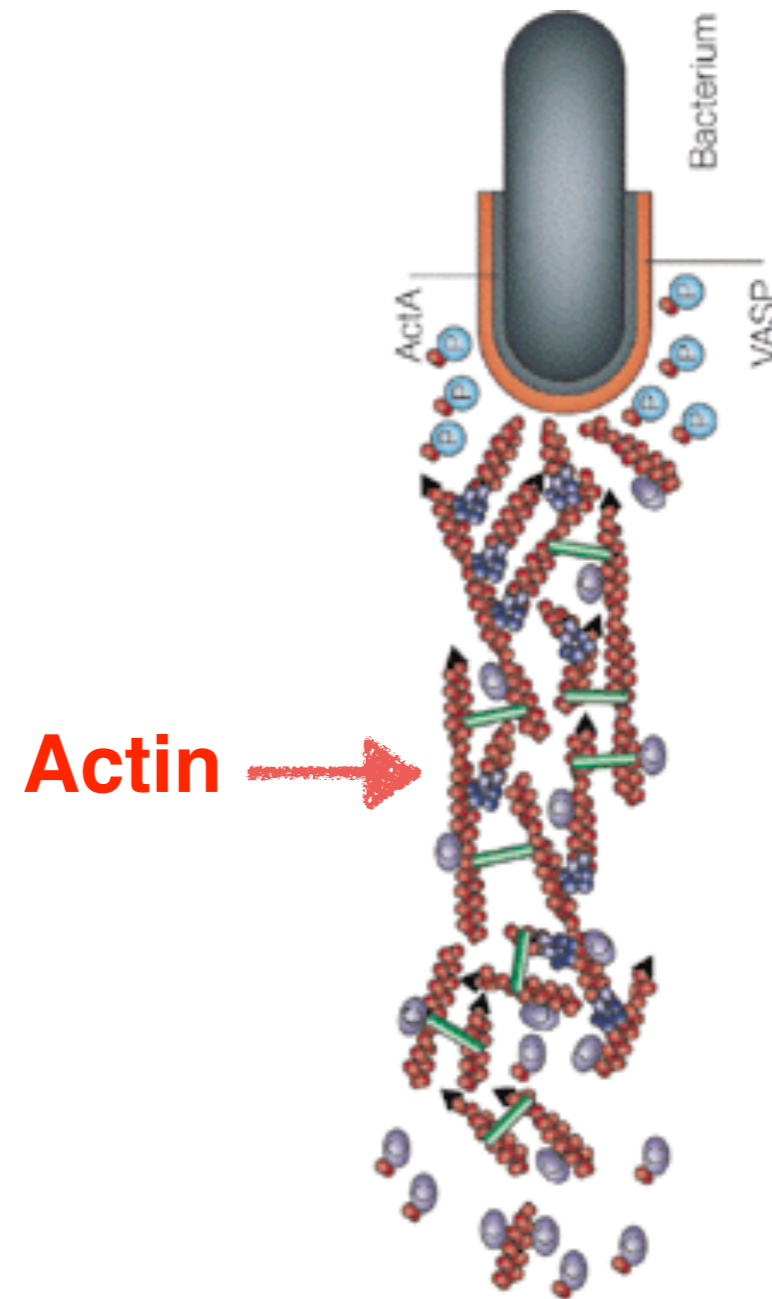
# Movement of bacteria

*Listeria monocytogenes*  
moving in PtK2 cells



Julie Theriot (speeded up 150x)

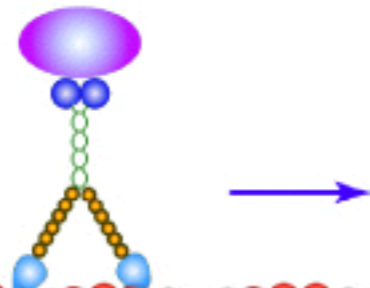
$v \sim 0.1 - 0.3 \mu\text{m/s}$



L. A. Cameron *et al.*, Nat. Rev. Mol. Cell Biol. 1, 110 (2000)

# Molecular motors

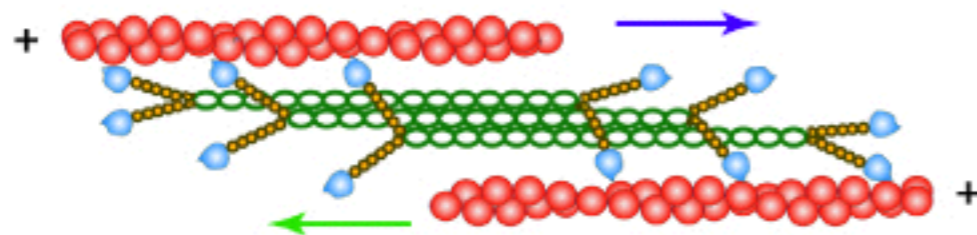
A Myosin V



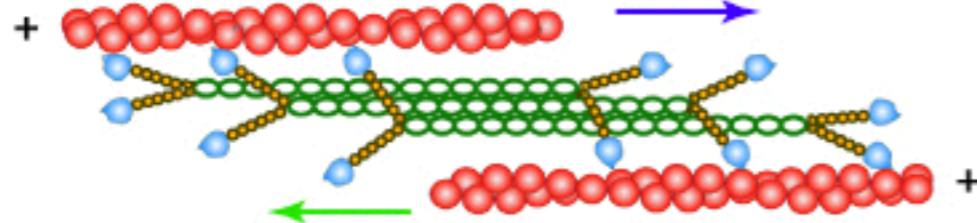
Actin



B Myosin II



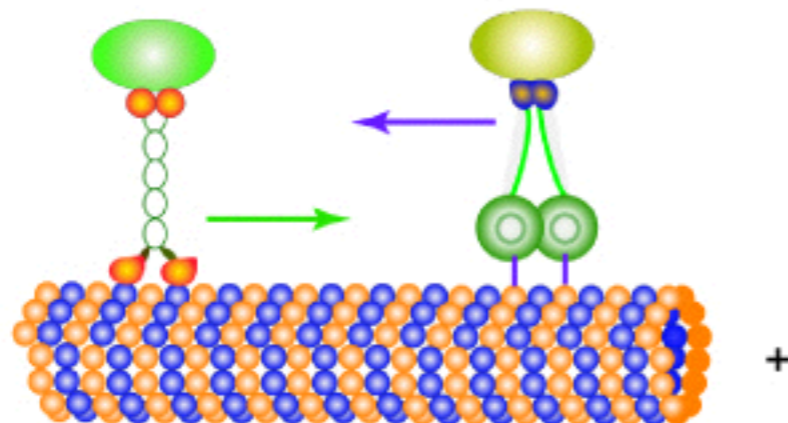
Actin



C

Kinesin-1

Dynein



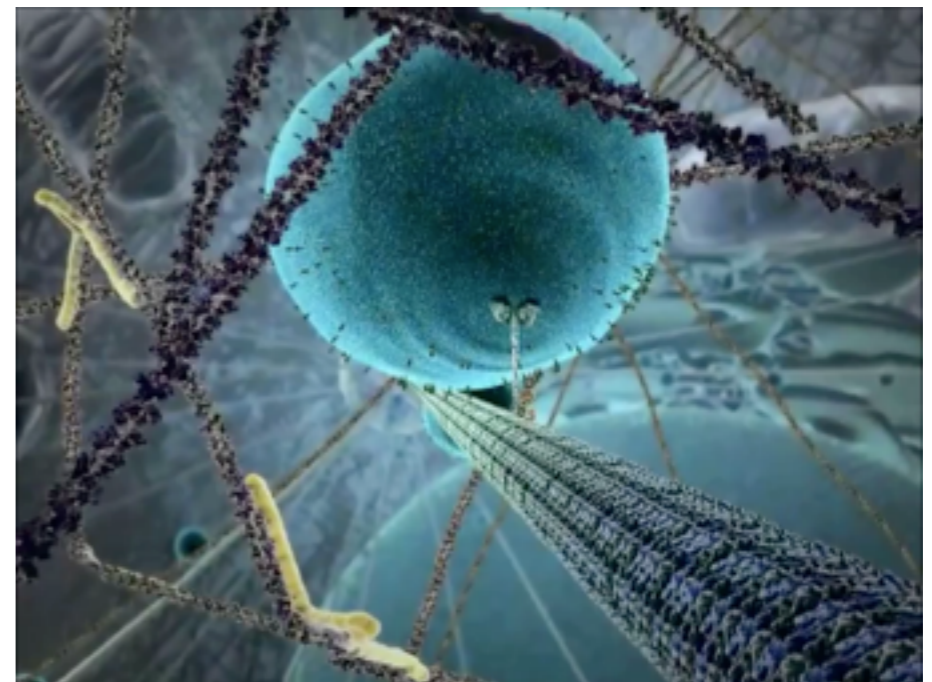
Microtubule

A.B. Kolomeisky, J. Phys.: Condens. Matter 25, 463101 (2013)

Transport of large molecules around cells  
(diffusion too slow)

$$v \sim 1 \mu\text{m/s}$$

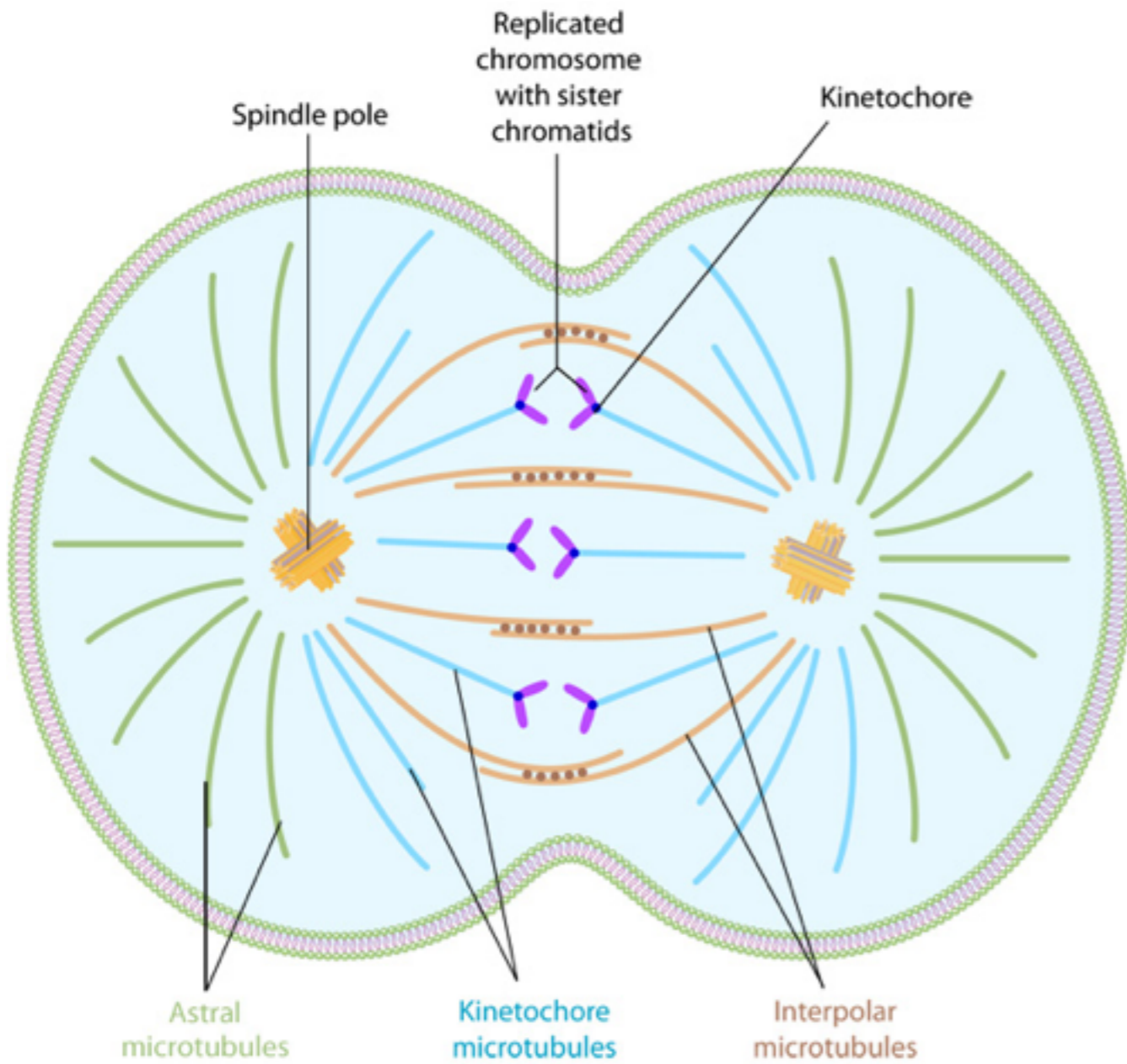
Contraction of muscles



Harvard BioVisions

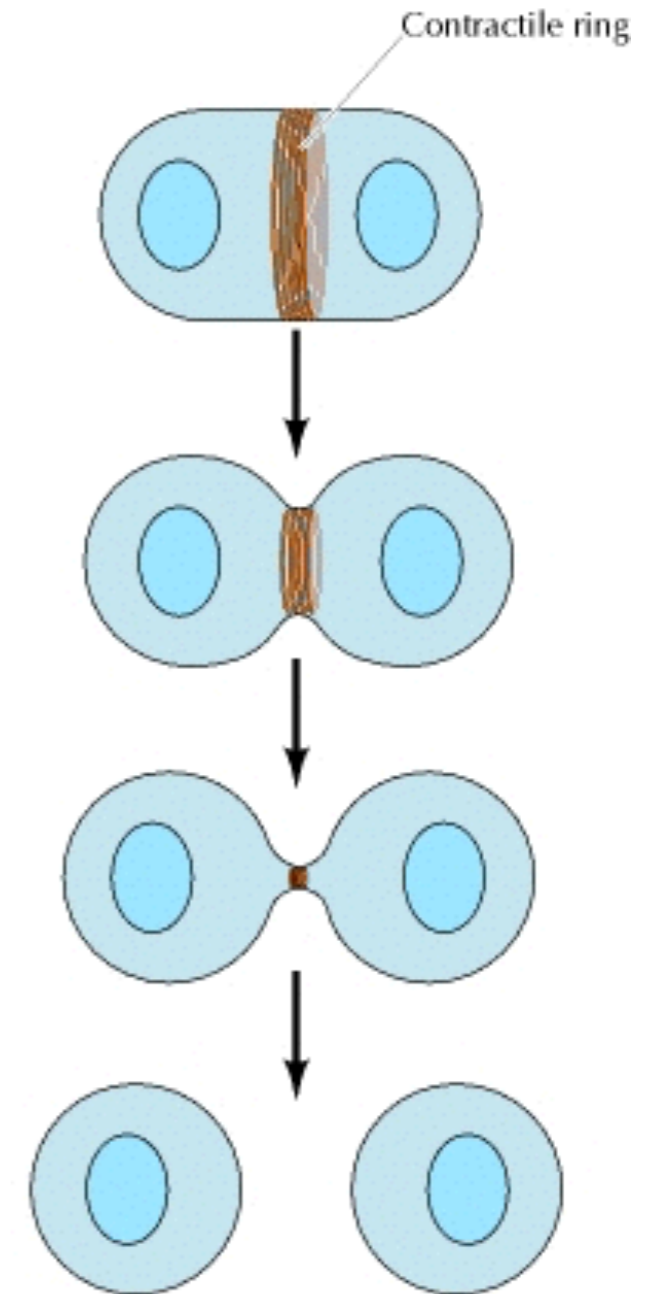
# Cell division

## Segregation of chromosomes



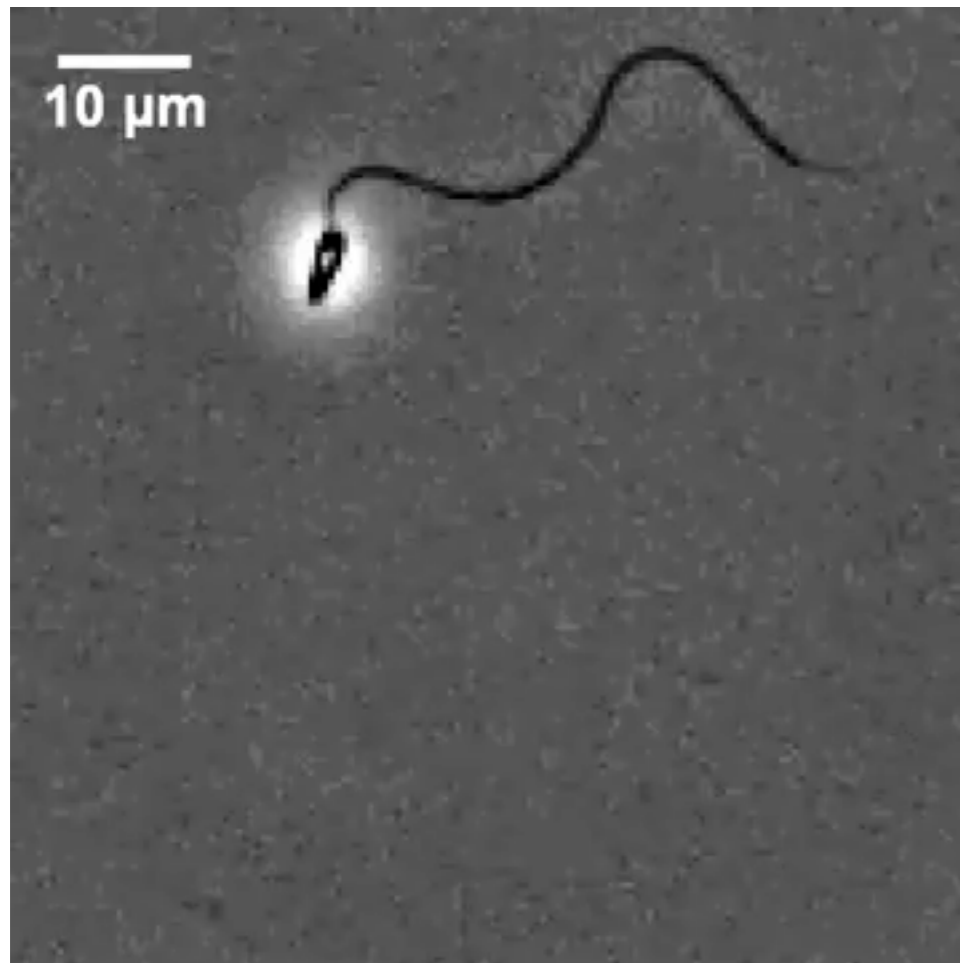
**Microtubules**

## Contractile ring divides the cell in two



**Actin**

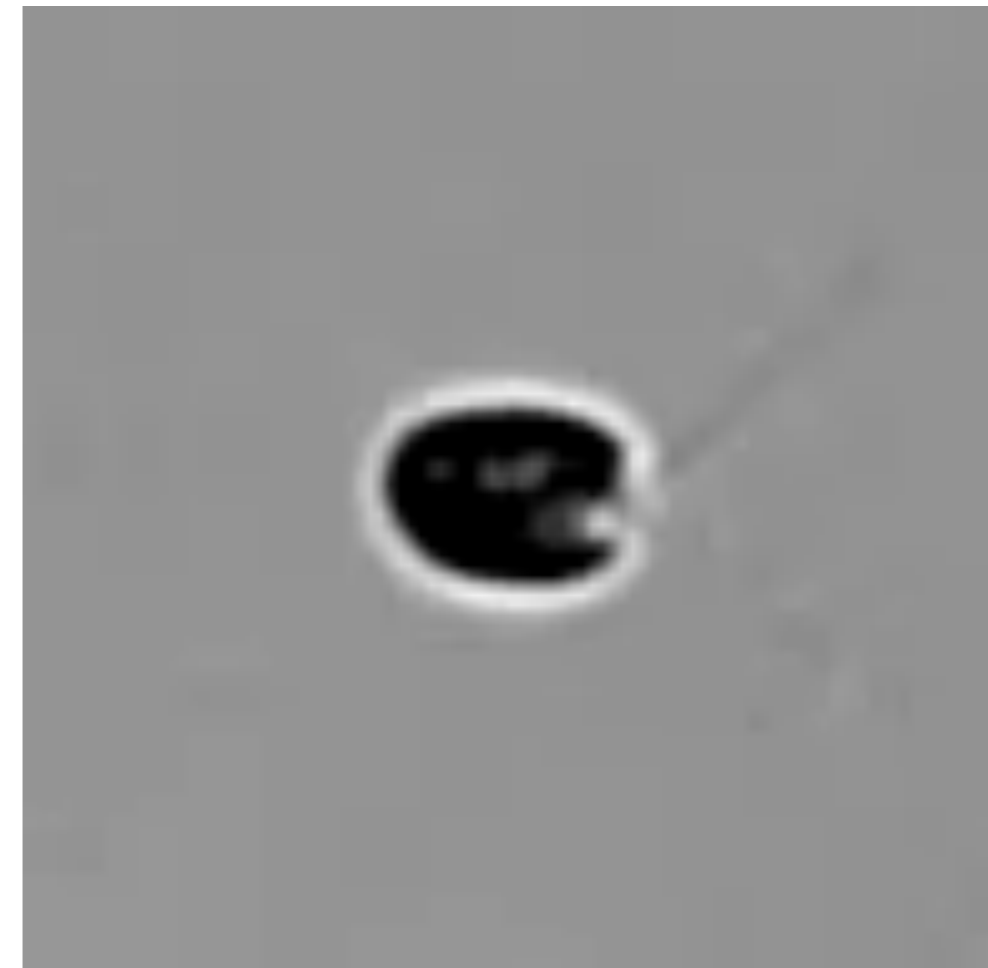
# Swimming of sperm cells



**Jeff Guasto**

$v \sim 50 \mu\text{m/s}$

# Swimming of Chlamydomonas (green alga)

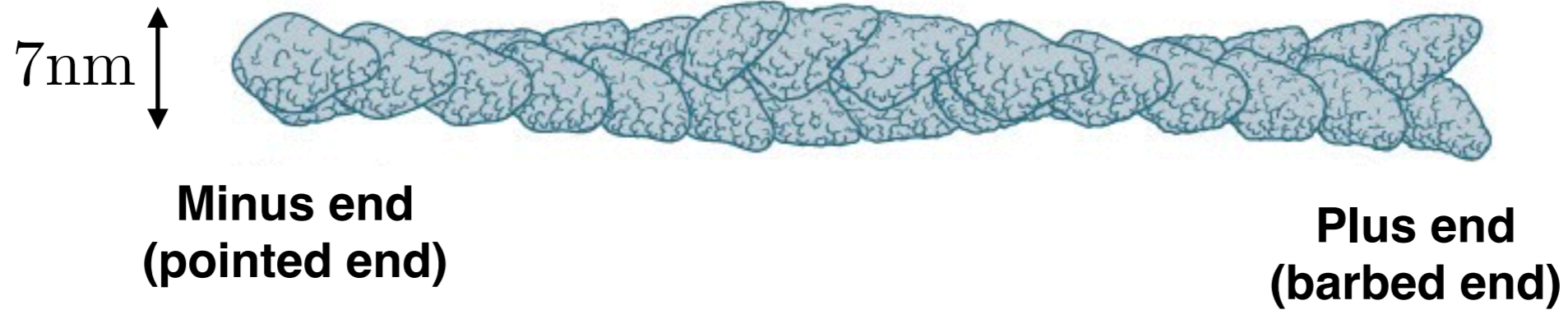


**Jeff Guasto**

$v \sim 60 \mu\text{m/s}$

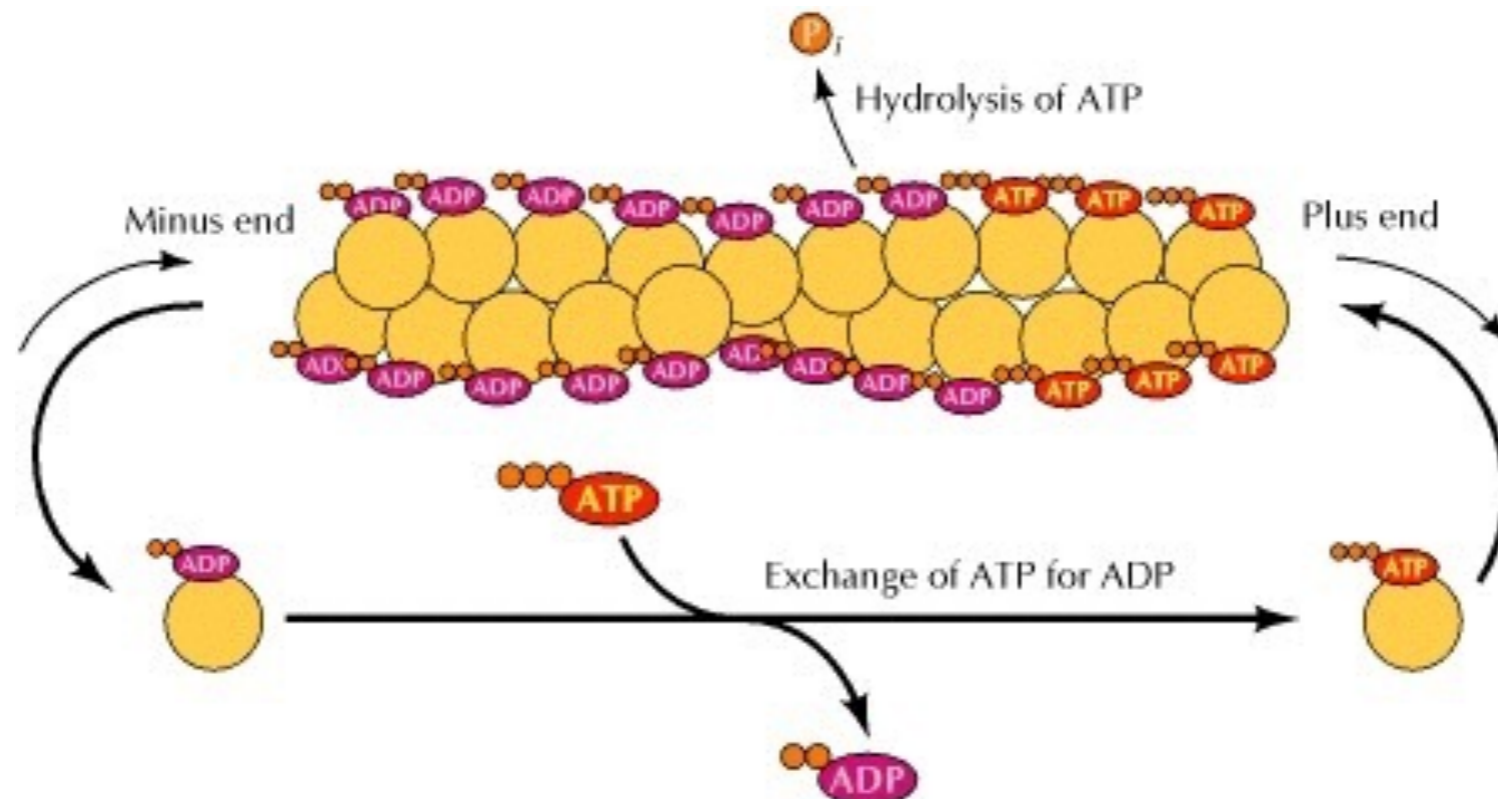
**Bending is produced by motors walking on  
neighboring microtubule-like structures**

# Actin filaments

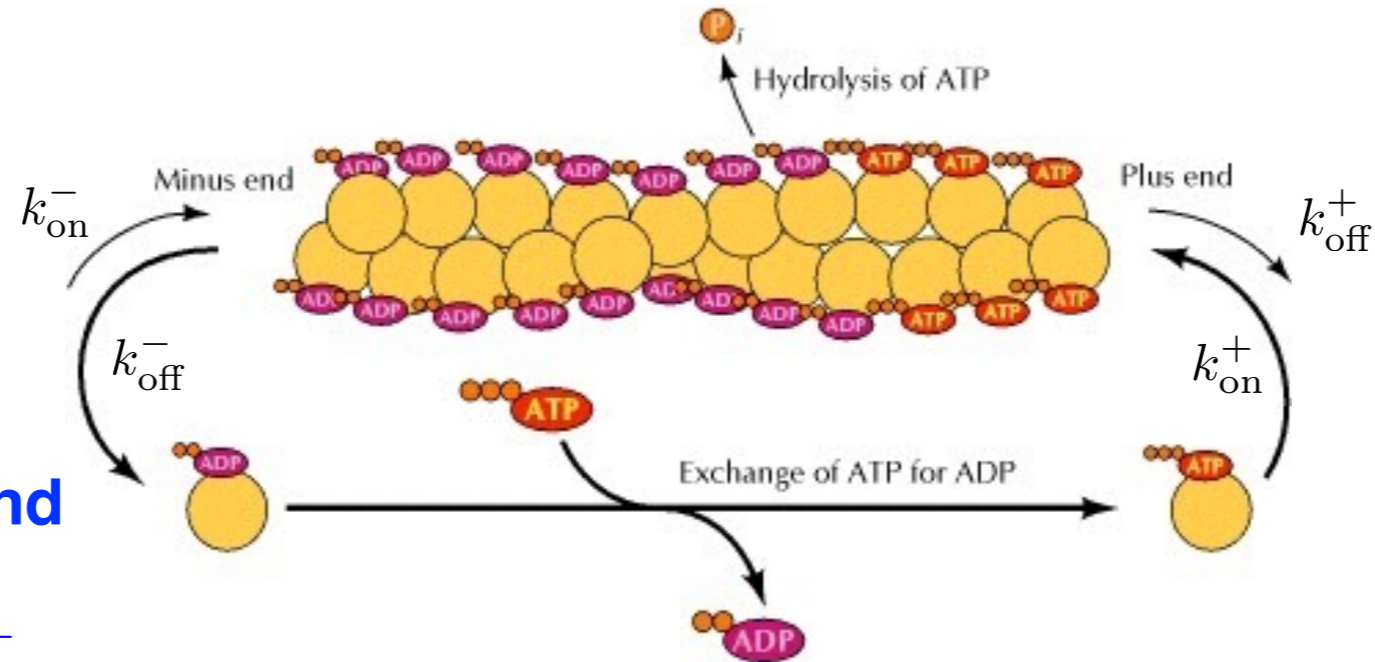


Persistence length  $\ell_p \sim 10\mu\text{m}$   
Typical length  $L \lesssim 10\mu\text{m}$

## Actin treadmilling



# Actin growth



**growth of minus end**

$$\frac{dn^-}{dt} = k_{on}^- [M] - k_{off}^-$$

**no growth at**

$$[M]_c^- = \frac{k_{off}^-}{k_{on}^-}$$

**growth of plus end**

$$\frac{dn^+}{dt} = k_{on}^+ [M] - k_{off}^+$$

**no growth at**

$$[M]_c^+ = \frac{k_{off}^+}{k_{on}^+}$$

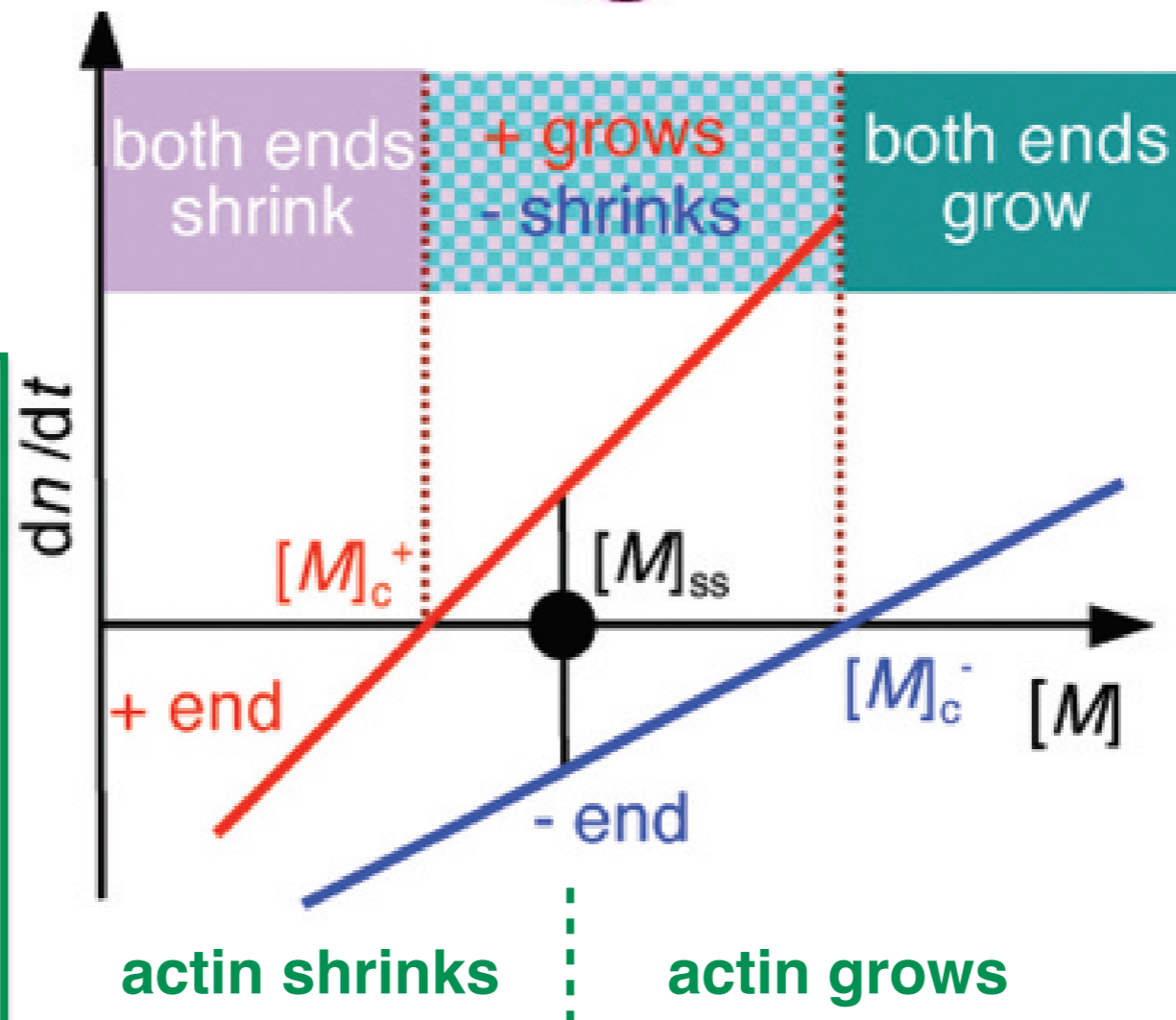
**Steady state regime**

$$\frac{dn^+}{dt} = -\frac{dn^-}{dt}$$

$$[M]_{ss} = \frac{k_{off}^+ + k_{off}^-}{k_{on}^+ + k_{on}^-} \approx 0.17 \mu\text{M}$$

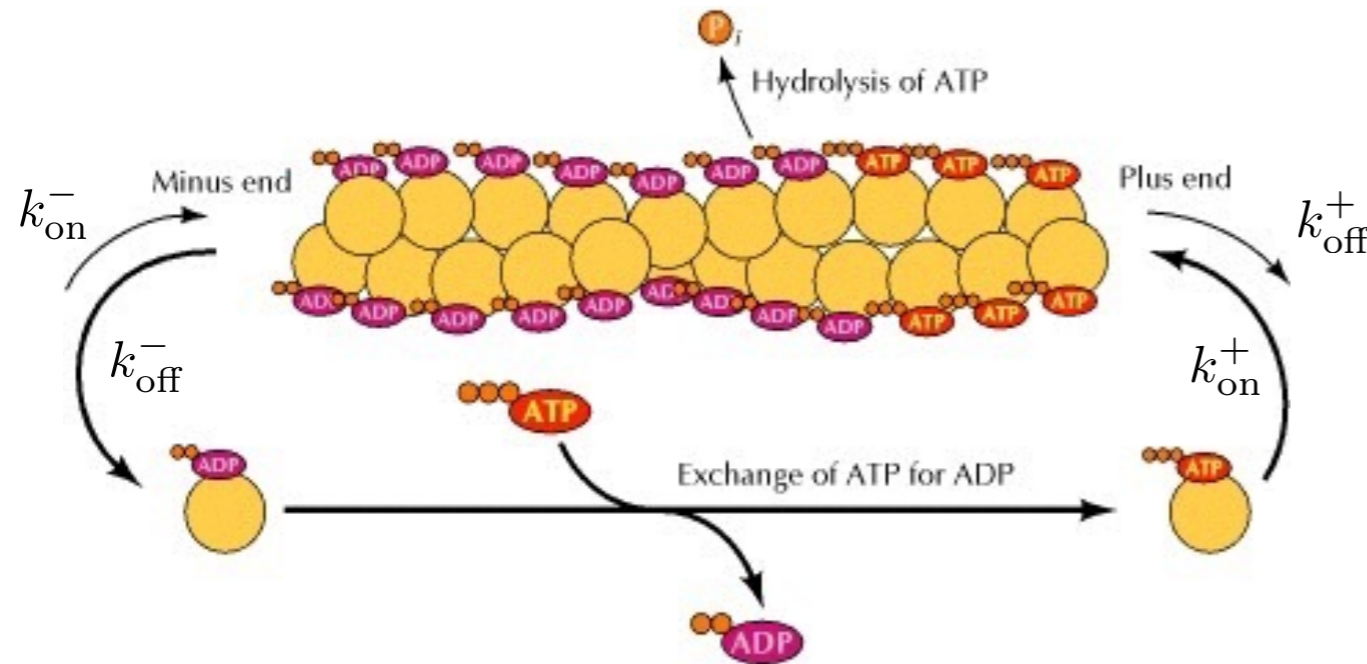
**front speed**

$$\frac{dn^+}{dt} = \frac{k_{on}^+ k_{off}^- - k_{on}^- k_{off}^+}{k_{on}^+ + k_{on}^-} \approx 0.6 \text{s}^{-1}$$



**concentration of free actin monomers**

# Distribution of actin filament lengths



**total rate of actin monomer addition**

$$k_{\text{on}} = k_{\text{on}}^+ + k_{\text{on}}^-$$

**total rate of actin monomer removal**

$$k_{\text{off}} = k_{\text{off}}^+ + k_{\text{off}}^-$$

## Master equation

$$\frac{\partial p(n, t)}{\partial t} = k_{\text{on}}[M]p(n-1, t) + k_{\text{off}}p(n+1, t) - k_{\text{on}}[M]p(n, t) - k_{\text{off}}p(n, t)$$

## Continuum limit

$$\frac{\partial p(n, t)}{\partial t} = -v \frac{\partial p(n, t)}{\partial n} + D \frac{\partial^2 p(n, t)}{\partial n^2}$$

**drift velocity**  $v = k_{\text{on}}[M] - k_{\text{off}}$

**diffusion constant**  $D = (k_{\text{on}}[M] + k_{\text{off}})/2$

**at large concentrations**

**actin grows (  $v > 0$  )**

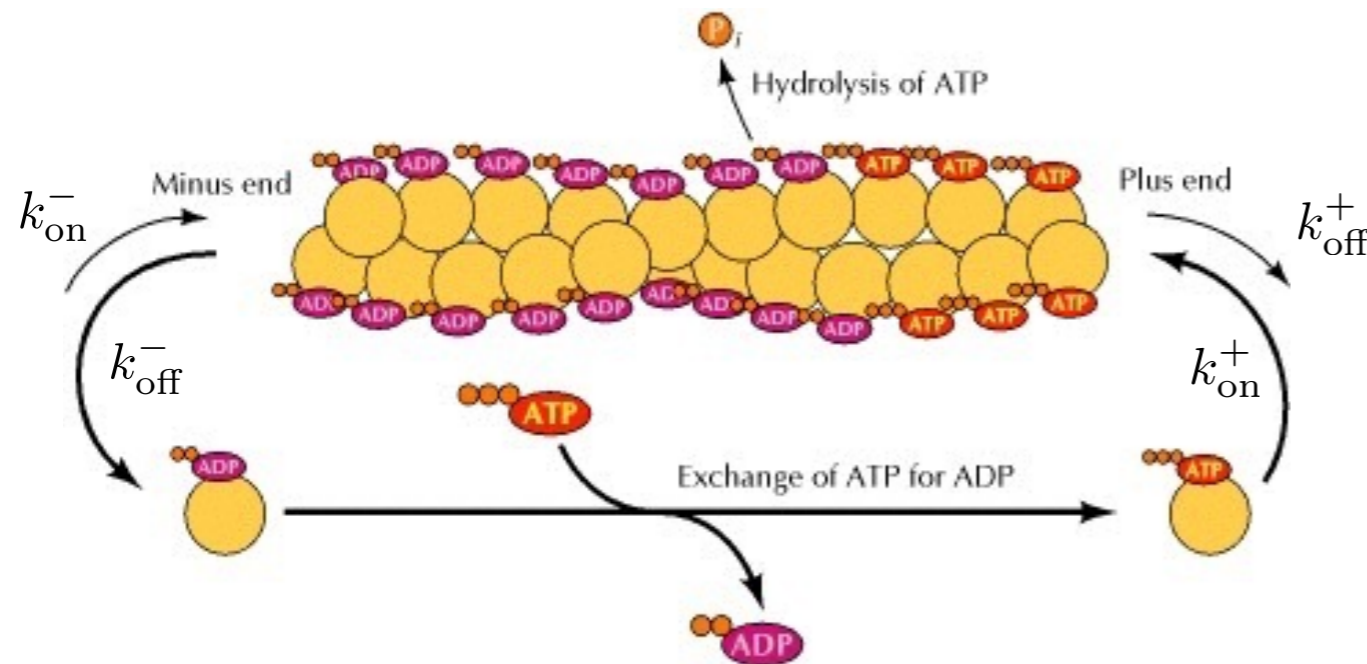
$$[M] > \frac{k_{\text{off}}}{k_{\text{on}}} = [M]_{\text{ss}}$$

**at low concentrations**

**actin shrinks (  $v < 0$  )**

$$[M] < \frac{k_{\text{off}}}{k_{\text{on}}} = [M]_{\text{ss}}$$

# Distribution of actin filament lengths



**total rate of actin monomer addition**

$$k_{\text{on}} = k_{\text{on}}^+ + k_{\text{on}}^-$$

**total rate of actin monomer removal**

$$k_{\text{off}} = k_{\text{off}}^+ + k_{\text{off}}^-$$

**What is steady state distribution of actin filament lengths at low concentration?**

$$\frac{\partial p^*(n, t)}{\partial t} = -v \frac{\partial p^*(n, t)}{\partial n} + D \frac{\partial^2 p^*(n, t)}{\partial n^2} = 0$$

**drift velocity**  $v = k_{\text{on}}[M] - k_{\text{off}} < 0$

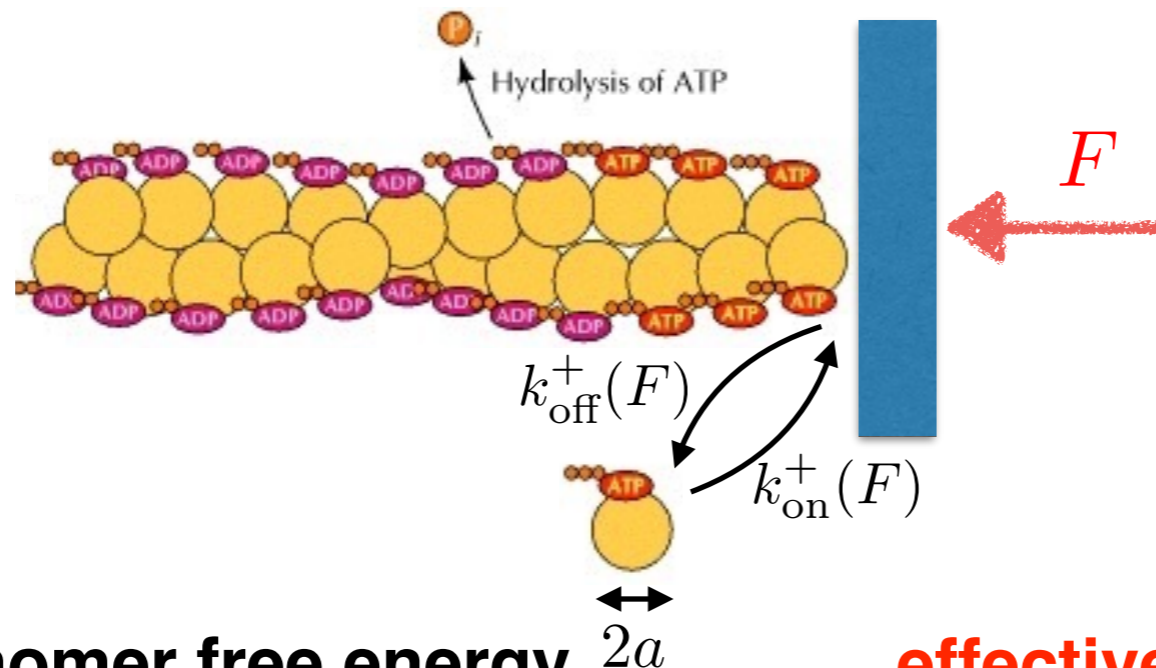
**diffusion constant**  $D = (k_{\text{on}}[M] + k_{\text{off}})/2$

$$p^*(n) = \frac{|v|}{D} e^{-|v|n/D} = \frac{1}{\bar{n}} e^{-n/\bar{n}}$$

**average actin filament length**

$$\bar{n} = \frac{D}{|v|} = \frac{(k_{\text{off}} + k_{\text{on}}[M])}{2(k_{\text{off}} - k_{\text{on}}[M])}$$

# Actin filament growing against the barrier

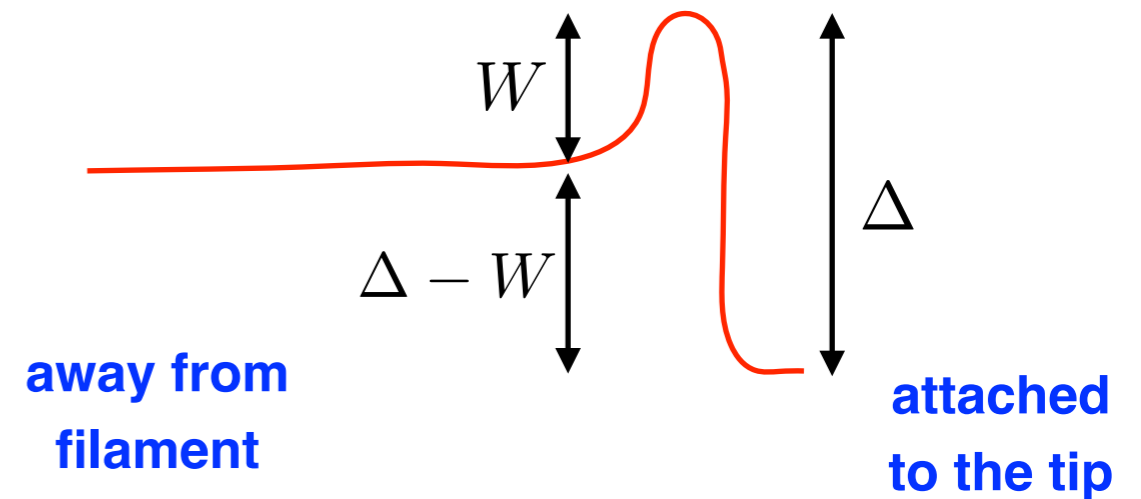
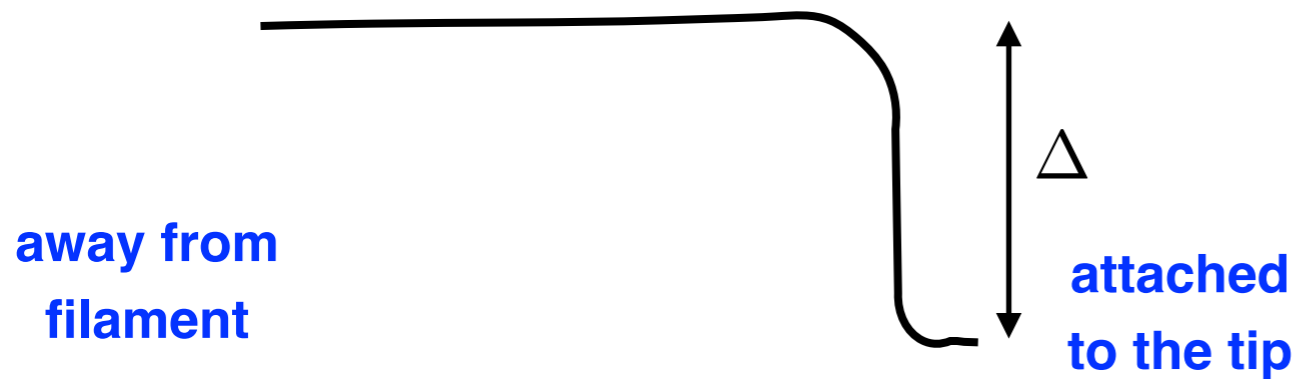


work done against the barrier for insertion of new monomer

$$W = Fa$$

effective monomer free energy potential without barrier

effective monomer free energy potential with barrier



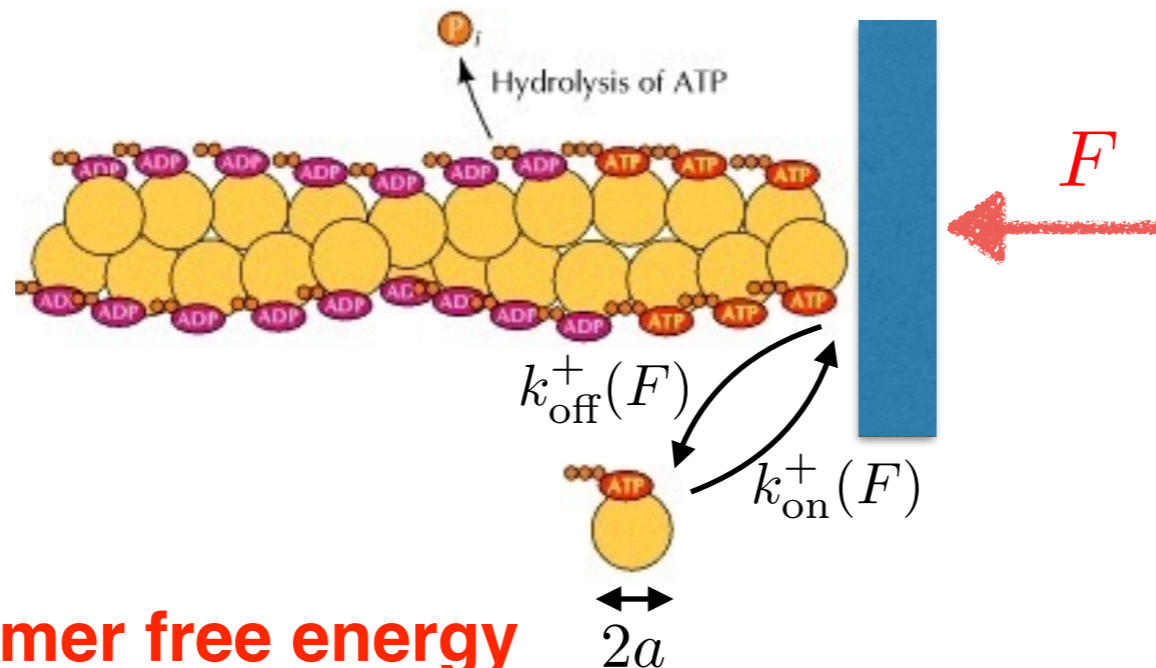
$$k_{\text{on}}^+ \sim 4\pi D_3 a$$

$$k_{\text{off}}^+ \propto e^{-\Delta/k_B T}$$

$$k_{\text{on}}^+(F) \sim k_{\text{on}}^+ e^{-Fa/k_B T}$$

$$k_{\text{off}}^+(F) \sim k_{\text{off}}^+$$

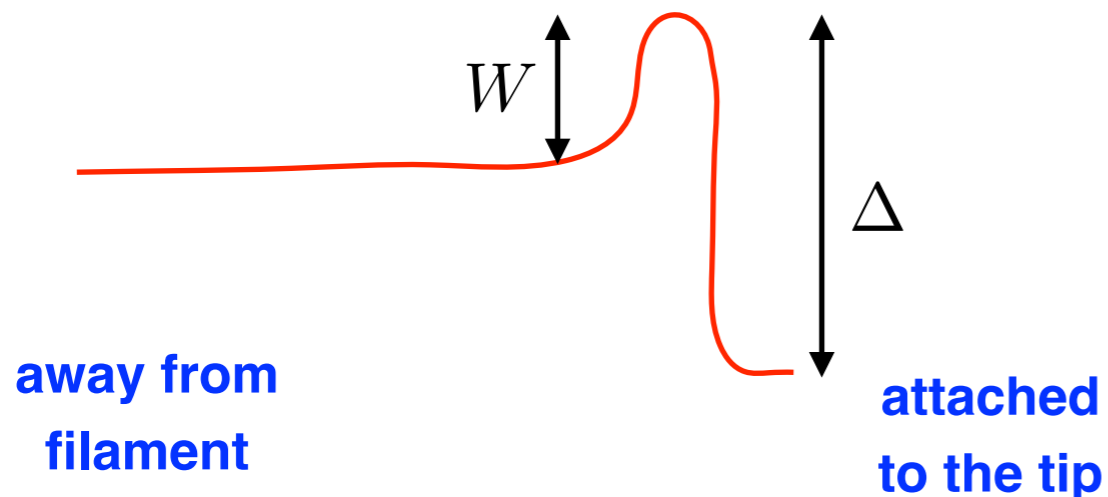
# Actin filament growing against the barrier



work done against the barrier for insertion of new monomer

$$W = Fa$$

effective monomer free energy potential with barrier



$$k_{\text{on}}^+(F) \sim k_{\text{on}}^+ e^{-Fa/k_B T}$$

$$k_{\text{off}}^+(F) \sim k_{\text{off}}^+$$

Growth speed of the tip

$$v^+(F) = k_{\text{on}}^+[M]e^{-Fa/k_B T} - k_{\text{off}}^+$$

Maximal force that can be balanced by growing filament

$$v^+(F_{\text{max}}) = 0 \longrightarrow F_{\text{max}} = \frac{k_B T}{a} \ln \left( \frac{k_{\text{on}}^+[M]}{k_{\text{off}}^+} \right)$$