



30th International  
Symposium on Combustion,  
Chicago, IL,  
July 25-30, 2004

# A Comprehensive Kinetic Mechanism for $C_1$ Species Combustion

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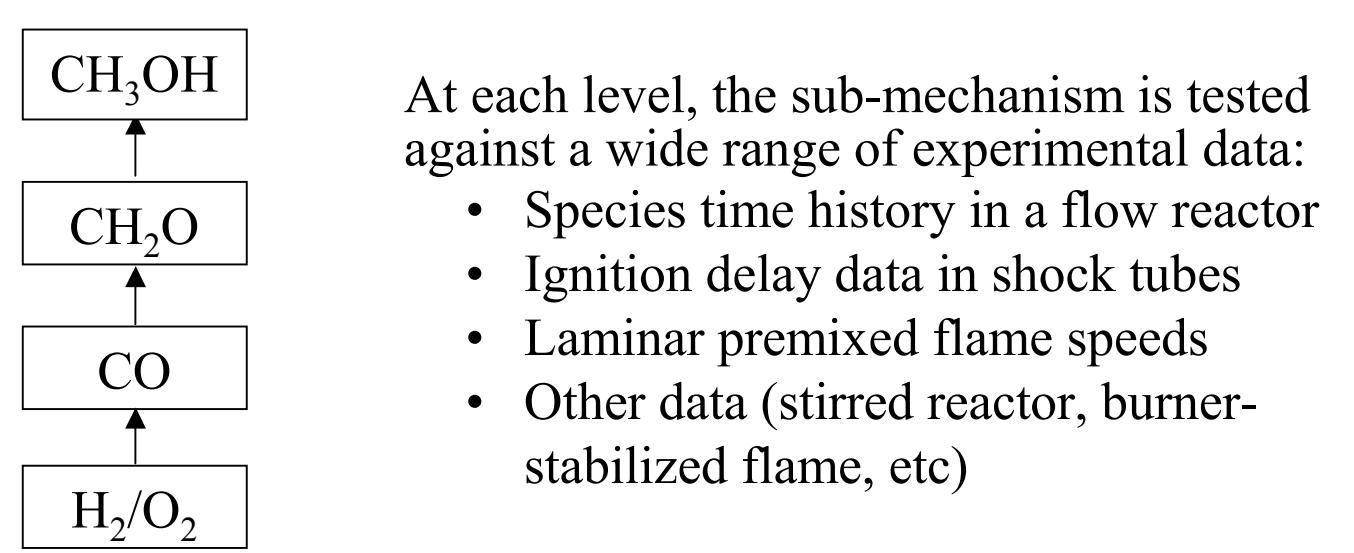
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## Motivation

- $C_1$  species are of practical importance:
  - CO is a primary intermediate of hydrocarbon combustion
  - emission of  $CH_2O$  from combustion engines has been a great environmental concern because it is a suspected carcinogen and can contribute to photochemical smog
  - $CH_3OH$  is a widely used oxygenate additive in reformulated gasoline, and is an attractive alternative to traditional transportation fuels
- Chemical kinetics of  $C_1$  species plays a critical role in hydrocarbon combustion chemistry:
  - the conversion of CO to  $CO_2$  is highly exothermic portion of any hydrocarbon oxidation system
  - nearly all carbon atoms in alkyl hydrocarbons and aromatics are converted to CO through  $CH_2O$  and HCO
  - study of  $CH_3OH$  oxidation mechanism lays a foundation for the study of larger alcohols chemistry, and can provide useful information regarding  $CH_2O$  reactions

## Outline of the Present $C_1$ Mechanism

- The mechanism consists of 85 elementary reactions among 21 species, and is based on the  $CH_3OH/O_2$  mechanism of Held and Dryer (1998).
- Revisions encompass recently published kinetic and thermochemical information, while continuing to predict both new experiments and the experimental targets investigated by the original mechanism.
- It is developed in a hierarchical manner:

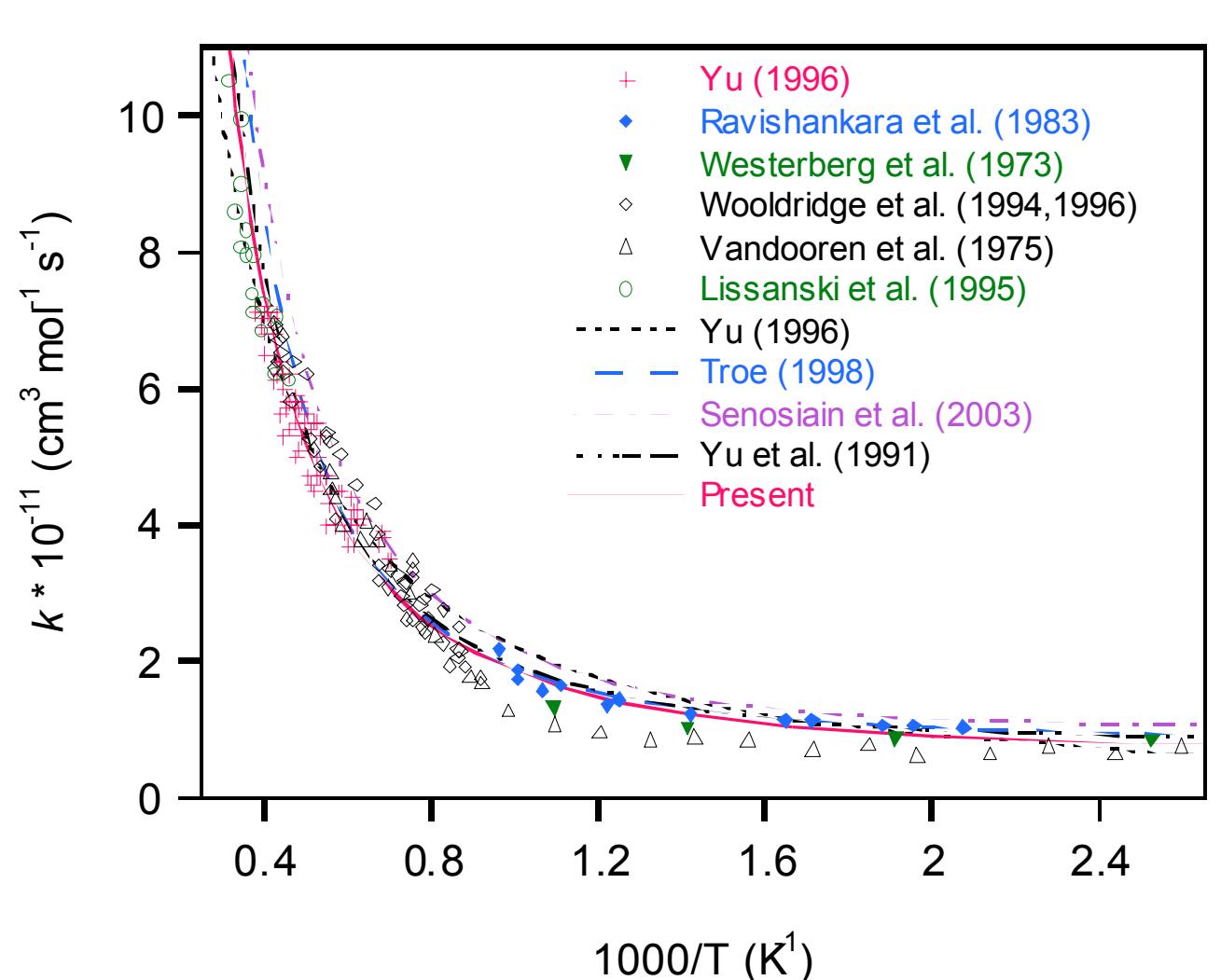


## Key Mechanism Refinements

### Part I: $CO + OH = CO_2 + H$

- this reaction is the main pathway to convert CO to  $CO_2$  and is responsible for a major fraction of the energy release derived in hydrocarbon oxidation
- recent theoretical calculations predict higher rates than experimental measurements at low to intermediate temperature range
- the temperature-dependent sensitivity analysis of Zhao et al. (this symposium, poster 1F2-13) demonstrates that the laminar flame speed of CO oxidation systems is most sensitive to this reaction at 300-1900 K
- The mechanism uses a new, weighted least squares fit of all of the experimentally measured rate constants available in literature. The expression obtained for the rate constant is:

$$k = 2.23 \times 10^5 T^{1.89} \exp(-\frac{583}{T})$$

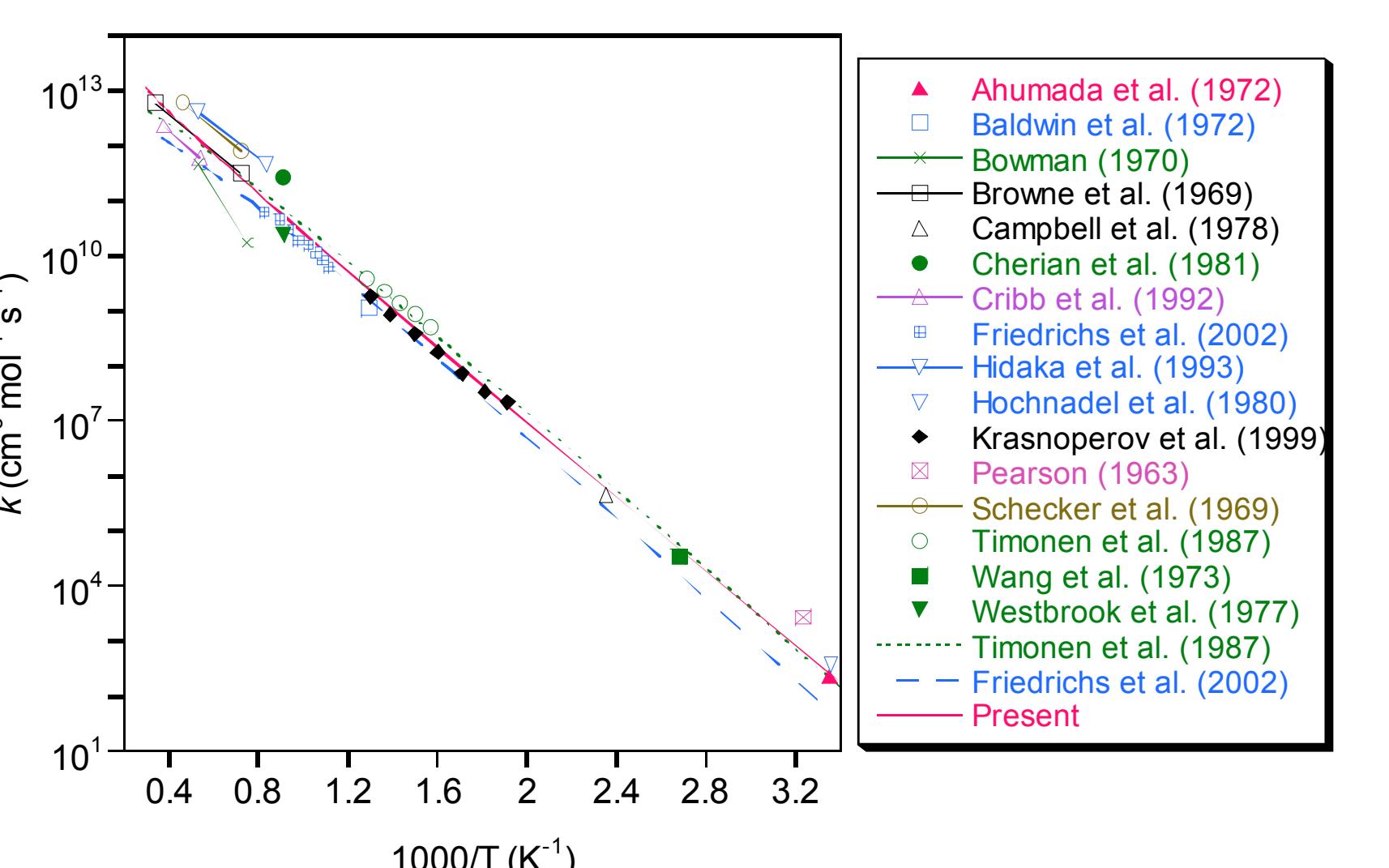


## Key Mechanism Refinements

### Part II: $HCO + M = H + CO + M$

- this reaction is the main pathway generating CO during the high temperature combustion of hydrocarbons.
- the temperature-dependent sensitivity analysis of Zhao et al. (this symposium, poster 1F2-13) demonstrates that the laminar flame speed of hydrocarbon combustion systems is most sensitive to this reaction at 1300-2000 K, which is above the temperature range of recent experimental studies of this reaction (Friedrichs et al., 2002).
- Extrapolation of Friedrichs et al. causes difficulties in reproducing flame speed and flow reactor results for numerous hydrocarbons
- In the present study, the method of least squares fitting was applied using experimental data available in literature, and this gives a new expression of the rate constant of this reaction:

$$k = 4.75 \times 10^{11} T^{0.66} \exp(-\frac{7485}{T})$$



## Full Set of Updated Kinetic Parameters

- Reaction rate coefficients:
  - $H_2/O_2$  sub-mechanism: Li et al. (Int. J. Chem. Kinet. 2004, in press)
  - $CO + OH = CO_2 + H$ : this study
    - weighted least squares fitting of experimental results in literature
  - $HCO + M = H + CO + M$ : this study
    - weighted least squares fitting of experimental results in literature
  - $CH_2O$  decomposition reactions: Friedrichs et al. (Int. J. Chem. Kinet. 2004, 36, 157)
  - $CH_2O + H = HCO + H_2$ : Irdam et al. (Int. J. Chem. Kinet. 1993, 25, 285)
  - $CH_2O + H_2O_2 = HCO + H_2O_2$ : Etienne et al. (J. Phys. Chem. A 1998, 102, 5196)
  - $CH_3OH$  decomposition reactions: GRI-MECH 3.0 (1999)
- Thermodynamic data:
  - OH: Ruscic et al. (J. Phys. Chem. A 2002, 106, 2727)
  - $CH_3$ : Ruscic et al. (J. Phys. Chem. A 1999, 103, 8625)
  - $CH_2OH$ : Johnson and Hudgens (J. Phys. Chem. 1996, 100, 19874)

## Literature CO Experiments Used for Validation

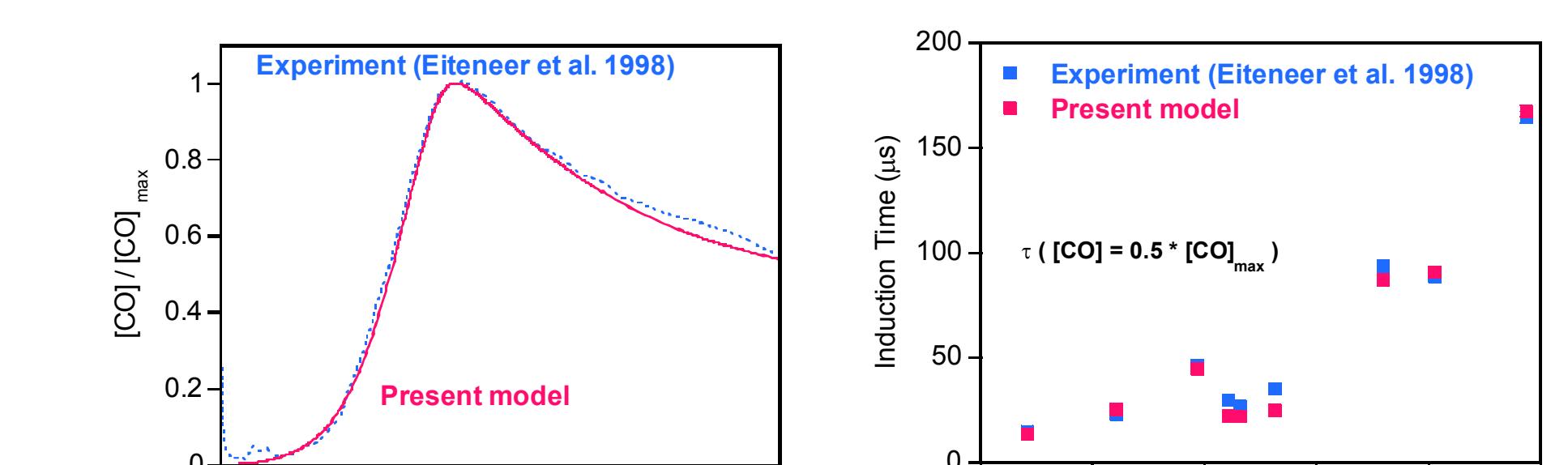
Method	Source	Mixture	T (K)	P (atm)	$\phi$
Shock Tube	Gardiner et al. (1971)	$CO/H_2O_2/Ar$	1400–2500	0.15–0.3	0.40
	Dean et al. (1978)	$CO/H_2O_2/Ar$	2000–2850	1.2–2.2	1.6–6.1
Laminar Premixed Flame	McLean et al. (1994)	$CO/H_2$	298	1	0.5–6.0
	Huang et al. (2003)	$CO/H_2N_2/air$	298	1	0.7–1.4
Flow Reactor	Yetter et al. (1991)	$CO/H_2O_2/N_2$	1033	1	0.4–1.4
	Kim et al. (1994)	$CO/H_2O/N_2$	960–1200	1.0–9.6	0.3–2.1
	Mueller et al. (1999)	$CO/H_2O$	1038	1.0–9.6	1.0

## Literature $CH_2O$ Experiments Used for Validation

Method	Source	Mixture	T (K)	P (atm)	$\phi$
Shock Tube	Dean et al. (1980)	$CH_2O/O_2/Ar$	1935–2150	1.1–1.3	0.67
	Buxton and Simpson (1986)	$CH_2O/Ar$	1750–2100	0.6–3.5	pyrolysis
	Hidaka et al. (1993)	$CH_2O/O_2/Ar$	1240–1950	1.5–2.9	4.0
	Etienne et al. (1998)	$CH_2O/O_2/Ar$	1440–2120	0.9–2.3	pyrolysis
	Friedrichs et al. (2002)	$CH_2O/Ar$	955–975	0.3–1.8	pyrolysis
Burner-Stabilized Flame	Vandooren et al. (1986)	$CH_2O/O_2$	300	0.03	0.22
	Hochgrob and Dryer (1992)	$CH_2O/O_2/N_2$	945–1095	1	0.013–1.74
Flow Reactor	Scire (2002)	$CH_2O/H_2O/O_2/N_2$	850–950	1.5–6.0	~0.005

## Representative Test Cases

### Part II: $C_1$ Model vs. $CH_2O$ Experiments



Initial Conditions:  
 $CH_2O = 1.5\%$ ,  $O_2 = 1.5\%$  with balance Ar at 1532 K and 1.35 atm,  $CH_2O/O_2$  mixture in a shock tube

Initial Conditions:  
0.9–2.3 atm,  $CH_2O = 0.5\%$ –2.0%,  $\phi = 0.2$ –pyrolysis,  $CH_2O/O_2/Ar$  mixture in a shock tube

Initial Conditions:  
 $CH_2O = 4.0\%$  with balance Ar at 1805 K and 2.81 atm,  $CH_2O$  mixture in a shock tube

Initial Conditions:  
 $CH_2O = 0.348\%$ ,  $O_2 = 0.223\%$  with balance  $N_2$  at 945 K and 1 atm

Symbols: flow reactor data of Hochgrob and Dryer (1992)

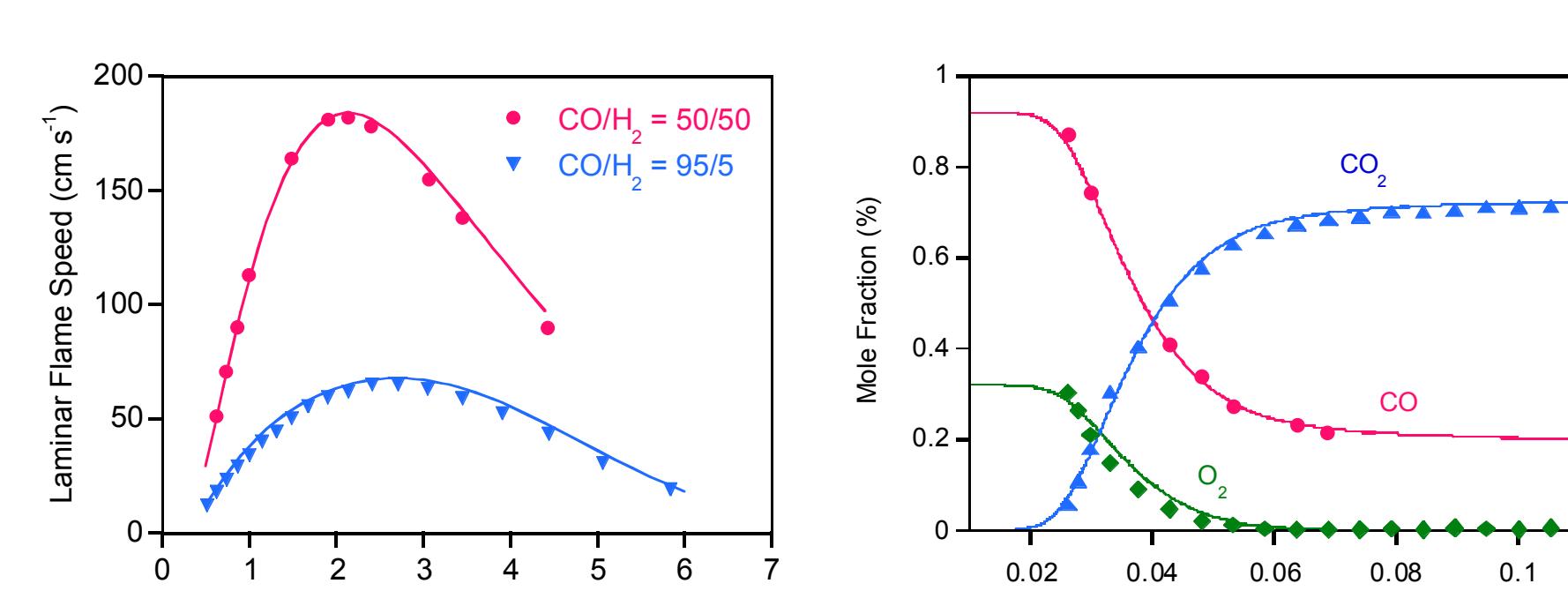
—: Present model

## Literature $CH_3OH$ Experiments Used for Validation

Method	Source	Mixture	T (K)	P (atm)	$\phi$
Shock Tube	Bowman (1975)	$CH_3OH/O_2/CO/Ar$	1545–2180	1.2–4.7	0.375–6.0
Laminar Premixed Flame	Egolfopoulos et al. (1992)	$CH_3OH/air$	318–368	1.0	0.5–2.0
	Aronowitz et al. (1979)	$CH_3OH/O_2/N_2$	1000–1010	1.0	0.05–1.6
Flow Reactor	Norton and Dryer (1989)	$CH_3OH/O_2/N_2$	1027–1034	1.0	0.6–1.6
	Held (1993)	$CH_3OH/O_2/N_2$	750–1040	1.5–20.0	0.3–2.6

## Representative Test Cases

### Part I: $C_1$ Model vs. CO Experiments



Initial Conditions:  
298 K, 1 atm,  $CO/H_2$  air mixture

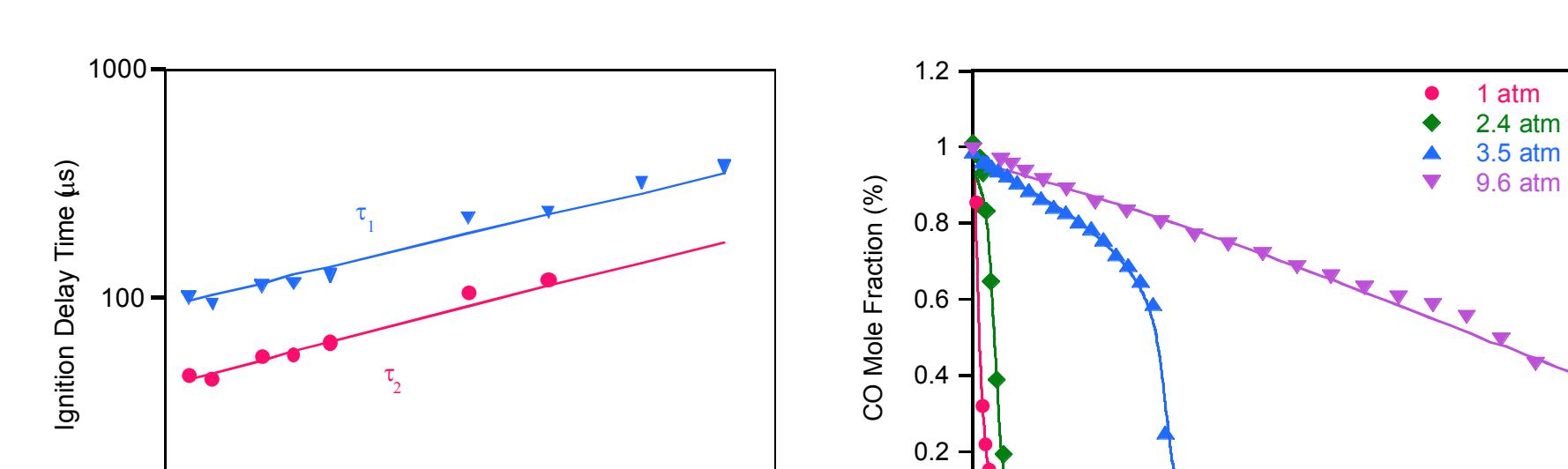
Symbols: laminar flame speed data of McLean et al. (1994)

—: Present model

Initial Conditions:  
 $CO = 0.92\%$ ,  $H_2O = 0.59\%$ ,  $O_2 = 0.32\%$  with balance  $N_2$  at 1034 K and 1 atm

Symbols: flow reactor data of Yetter et al. (1991)

—: Present model



Initial Conditions:  
2.9–3.3 atm,  $CH_3OH = 1.0\%$ ,  $\phi = 1.5$ ,  $CH_3OH/O_2/Ar$  mixture in a shock tube

The present mechanism has improved predictive capability over Held and Dryer mechanism (1998)

The agreement of the present mechanism with other literature experiments is also very good

## Summary

- A detailed chemical kinetic mechanism for  $C_1$  species (CO,  $CH_2O$ , and  $CH_3OH$ ) combustion has been developed hierarchically
- The mechanism has been verified against a wide range of experimental data, and demonstrates very good predictive capabilities for CO,  $CH_2O$ , and  $CH_3OH$  combustion
- Mechanism is available in Chemkin II format from our Web site or by contacting the authors

## Acknowledgements

This study was supported by the U.S. Department of Energy, Office of Basic Sciences through Grant No. DE-FG02-86ER-13503, and by NASA under Grant No. NCC3-735.