# AN APPROACH TO THE FEEDBACK CONTROL OF NONLINEAR ECONOMETRIC SYSTEMS

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## AN APPROACH TO THE FEEDBACK CONTROL OF NONLINEAR ECONOMETRIC SYSTEMS

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In this paper, I present an approach to perform approximately optimal feed-back control to minimize the expectation of a quadratic loss function given a system of nonlinear structural econometric equations. The method is explained for simultaneous equation systems with given or unknown parameters (sections 1 and 2). The usefulness of having a solution in feedback form is discussed (section 3). The Klein-Goldberger model is used as an illustration (section 4). Some concluding remarks concerning the approach completes the paper (section 5).

#### 1. Feedback Control for Known Econometric Systems

The solution presented in this section for the feedback control of a non-linear econometric system with known parameters has been obtained in Chow (1975a, Chapter 12) and Chow (1975b). The former reference applies the method of Lagrange multipliers while the latter applies the method of dynamic programming to the control of an econometric system with unknown parameters and deduces the solution as a by-product. The exposition in this section applies dynamic programming to the case of known parameters directly. It attempts to relate the theory of control for nonlinear systems to linear theory and emphasizes the computational aspects of the solution more than the previous references.

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The i-th structural equation for the observation in period t is

(1.1) 
$$y_{it} = \Phi_i(y_t, y_{t-1}, x_t, n_{it}) + \varepsilon_{it}$$

where  $y_{it}$  is the i-th element in the vector  $y_t$  of endogenous variables,  $x_t$  is a vector of control variables,  $\eta_{it}$  is a vector of parameters and exogenous variables not subject to control, and  $\varepsilon_{it}$  is an additive random disturbance with mean zero, variance  $\sigma_{ii}$  and distributed independently through time. In this section, the elements of  $\eta_{it}$  are treated as given, leaving  $\varepsilon_{it}$  to be the only random variables. Section 2 will deal with uncertainty in  $\eta_{it}$  which may also incorporate non-additive random disturbances if necessary. Lagged endogenous variables dated prior to t-1 will be eliminated by introducing identities of the form  $y_{kt} = y_{j,t-1}$ . Control variables will be incorporated in the vector  $y_t$  for two purposes. First, by defining  $y_{kt} = x_{jt}$ , one can write welfare loss as a function of  $y_t$  alone. Second, lagged control variables can be eliminated by identities of the form  $y_{mt} = y_{k,t-1} = x_{j,t-1}$ . The system of structural equations (1.1) can be written as

(1.2) 
$$y_{+} = \Phi(y_{+}, y_{+-1}, x_{+}, \eta_{+}) + \varepsilon_{+}$$

with  $~\Phi~$  denoting a vector function, and with  $~E\epsilon_{\mbox{t}}\epsilon_{\mbox{t}}^{\,\mbox{\tiny T}}=\Sigma$  .

We assume a quadratic loss function for a T-period control problem,

(1.3) 
$$W = \sum_{t=1}^{T} (y_t - a_t)' K_t (y_t - a_t) = \sum_{t=1}^{T} (y_t' K_t y_t - 2y_t' K_t a_t + a_t' K_t a_t)$$

where  $a_t$  are given targets, and  $K_t$  are known symmetric positive semidefinite matrices. The problem is to minimize the expectation  $E_0W$  conditioned on the information available at the end of period 0. Following the method of dynamic programming, we first solve the optimal control problem for the last period T by minimizing

$$V_{T} = E_{T-1} (y_{T}^{\dagger} K_{T} y_{T} - 2y_{T}^{\dagger} K_{T} a_{T} + a_{T}^{\dagger} K_{T} a_{T}) = E_{T-1} (y_{T}^{\dagger} H_{T} y_{T} - 2y_{T}^{\dagger} h_{T} + c_{T})$$

with respect to  $\mathbf{x}_{_{\!\boldsymbol{m}}}$  . In (1.4) we have defined

(1.5) 
$$H_{T} = K_{T} ; h_{T} = K_{T} a_{T} ; c_{T} = a_{T}^{\dagger} K_{T} a_{T}$$

for the sake of future treatment of the multi-period control problem. The problem for period T is solved in the following steps.

(1) Starting with some trial value  $\tilde{x}_T$  for the control, we set  $\epsilon_T$  equal to zero and linearize the right hand side of (1.2) about  $y_{T-1} = y_{T-1}^{\circ}$  (given),  $x_T = \tilde{x}_T$  and  $y_T = y_T^{\star}$  which is the solution of the system

$$\mathbf{y_{T}^{\star}} = \Phi(\mathbf{y_{T}^{\star}}, \mathbf{y_{T-1}^{\circ}}, \mathbf{x_{T}^{\star}}, \mathbf{\eta_{T}^{\star}})$$

where  $y_T^{\star}$  can be computed by some iterative method such as the Gauss-Seidel. The linearized version of the structure (1.2) is

$$(1.7) y_{T} = y_{T}^{\star} + B_{1T}(y_{T} - y_{T}^{\star}) + B_{2T}(y_{T-1} - y_{T-1}^{\circ}) + B_{3T}(x_{T} - \tilde{x}_{T}) + \varepsilon_{T}$$

where the j-th column of  $\,^B_{1T}\,^{}$  consists of the partial derivatives of the vector function  $\,^\Phi$  with respect to the j-th element of  $\,^y_T$  , evaluated at the given

values  $y_T^\star$ ,  $y_{T-1}^\circ$ ,  $\tilde{x}_T^\circ$  and  $\eta_T^\circ$ , and similarly for the j-th column of  $B_{2T}^\circ$  and  $B_{3T}^\circ$ . Computationally, if the structural functions  $\Phi_i^\circ$  are listed in Fortran, each column of  $B_{1T}^\circ$  can be evaluated numerically as the rates of change in  $\Phi_i^\circ$  with respect to a small change in the j-th element of  $y_T^\circ$  from  $\tilde{y}_T^\circ$ , and similarly for  $B_{2T}^\circ$  and  $B_{3T}^\circ$ . In econometric applications,  $B_{1T}^\circ$  is very sparse, each row typically consisting of very few elements corresponding to the other current endogenous variables in the equation.

(2) We solve (1.7) for the linearized reduced-form

(1.8) 
$$y_{\mathbf{T}} = A_{\mathbf{T}} y_{\mathbf{T}-1} + C_{\mathbf{T}} x_{\mathbf{T}} + b_{\mathbf{T}} + u_{\mathbf{T}}$$

where

(1.9) 
$$(A_{T} \quad C_{T} \quad u_{T}) = (I - B_{1T})^{-1} (B_{2T} \quad B_{3T} \quad \varepsilon_{T}) ,$$

$$b_{T} = y_{T}^{*} - A_{T}y_{T-1}^{\circ} - C_{T}\tilde{x}_{T} .$$

Note that, since all the identities used to reduce a higher-order structure to first-order and to incorporate the current and lagged x's into  $y_t$  are already reduced-form equations, the matrix  $I - B_{1T}$  takes the form

(1.10) 
$$I - B_{1T} = \begin{bmatrix} I - B_{1T}^* & 0 \\ 0 & I \end{bmatrix}$$

where the order of  $B_{1T}^{\star}$  is the number of simultaneous structural equations excluding these identities. Thus only I -  $B_{1T}^{\star}$  has to be inverted for the computation of  $A_{T}$ ,  $C_{T}$  and  $b_{T}$  in (1.8).

(3) We minimize (1.4) with respect to  $\mathbf{x}_{\mathrm{T}}$ , assuming that  $\mathbf{y}_{\mathrm{T}}$  is governed by (1.8). This is done by differentiating (1.4) with respect to  $\mathbf{x}_{\mathrm{T}}$  and interchanging the order of taking expectation and differentiation:

$$(1.11) \qquad \frac{\partial V_{T}}{\partial x_{T}} = 2E_{T-1} \left[ \left( \frac{\partial y_{T}^{\prime}}{\partial x_{T}} \right) H_{T} y_{T} - \left( \frac{\partial y_{T}^{\prime}}{\partial x_{T}} \right) h_{T} \right]$$

$$= 2E_{T-1} \left[ C_{T}^{\prime} H_{T} \left( A_{T} y_{T-1} + C_{T} x_{T} + b_{T} + u_{T} \right) - C_{T}^{\prime} h_{T} \right] = 0$$

where (1.8) has been used to substitute for  $\left(\frac{\partial y_T}{\partial x_T}\right)$  and  $y_T$ . The solution of (1.11) for  $x_T$  is

(1.12) 
$$\hat{x}_{T} = G_{T} Y_{T-1} + G_{T}$$

where

$$G_{T} = - (E_{T-1}C_{T}'H_{T}C_{T})^{-1}(E_{T-1}C_{T}'H_{T}A_{T})$$

$$G_{T} = - (E_{T-1}C_{T}'H_{T}C_{T})^{-1}(E_{T-1}C_{T}'H_{T}A_{T}) - E_{T-1}C_{T}'h_{T} .$$

By the linear approximation (1.8),  $A_T$ ,  $C_T$  and  $b_T$  are not functions of  $\epsilon_T$  and are thus nonrandom. Therefore, the expectation signs in (1.13) can be dropped, but we retain them for future discussion.

(4) Using the solution  $\hat{x}_T$  of (1.12) to replace the initial guess  $\hat{x}_T$  in step (1), we repeat steps (1) through (4) till convergence in  $\hat{x}_T$ . Observe that the solution, even when converging, is not truly optimal because we have used the approximate reduced form (1.8) with constant coefficients  $A_T$ ,  $C_T$ 

and b $_{T}$ . To obtain an exactly optimal solution, one would first compute  $\tilde{y}_{T}$  as the solution of the stochastic structure (1.2) with  $\epsilon_{T}$  included, rather than  $y_{T}^{\star}$  as a solution of (1.6). Thus  $\tilde{y}_{T}$  is a random vector depending on  $\epsilon_{m}$ . Secondly, (1.7) would be replaced by

$$(1.14) y_{T} = \tilde{y}_{T} + B_{1T}(y_{T} - \tilde{y}_{T}) + B_{2T}(y_{T-1} - y_{T-1}) + B_{3T}(x_{T} - \tilde{x}_{T}) .$$

The derivatives  ${
m B}_{
m 1T}$ ,  ${
m B}_{
m 2T}$  and  ${
m B}_{
m 3T}$  in (1.14) which are evaluated at  ${
m v}_{
m T}$  , and hence the matrices  $\mathbf{A}_{\overline{\mathbf{T}}}$ ,  $\mathbf{C}_{\overline{\mathbf{T}}}$  and  $\mathbf{b}_{\overline{\mathbf{T}}}$  in the resulting reduced form corresponding to (1.8), will be dependent on  $\,\epsilon_{_{\hbox{\scriptsize T}}}^{}$  . The matrices  $\,{\rm G}_{_{\hbox{\scriptsize T}}}^{}$  and  $\,{\rm g}_{_{\hbox{\scriptsize T}}}^{}$  in the solution for  $\hat{x}_{T}$  will be calculated by (1.13) with the expectation signs retained. Such a four-step iterative procedure would be optimal because when the solution  $\hat{x}_{m}$  converges the value  $y_{m}$  given by the linearized structure (1.14) and its reduced form would be exactly equal to  $\tilde{y}_{\mathbf{r}}$ , the solution value from the original structure (1.2); the second line of (1.11) would be exactly equal to the first line and not be merely an approximation. The above approximate solution amounts to replacing (1.14) by (1.7), i.e., linearizing the structure about the nonstochastic  $\mathbf{y}_{\mathrm{T}}^{\star}$  rather than the stochastic  $\mathbf{y}_{\mathrm{T}}^{\star}$ , thus making the derivatives  $B_{1T}$ ,  $B_{2T}$  and  $B_{3T}$  nonstochastic. The first  $y_T$  in (1.14), which equals  $\Phi(y_T,...) + \epsilon_T$  by (1.2), is replaced by  $\Phi(y_T^\star,...) + \epsilon_T$ or  $y_{\mathrm{T}}^{\star}$  +  $\epsilon_{\mathrm{T}}^{}$  in (1.7). This approximate solution is the same as the certaintyequivalence solution obtained by minimizing (1.4) subject to the constraint (1.2) with  $\varepsilon_{_{\rm T}}$  = 0 .

(5) Using (1.8) for  $y_T$  and (1.12) for  $x_T$ , we compute the minimum expected loss for period T from (1.4), yielding

$$\hat{V}_{T} = \hat{Y}_{T-1}^{'} E_{T-1}^{'} (A_{T} + C_{T}^{G}_{T})^{'} H_{T}^{'} (A_{T} + C_{T}^{G}_{T}) Y_{T-1}$$

$$+ 2 \hat{Y}_{T-1}^{'} E_{T-1}^{'} (A_{T} + C_{T}^{G}_{T})^{'} (H_{T}^{b}_{T} - h_{T}^{'})$$

$$+ E_{T-1}^{'} (b_{T} + C_{T}^{g}_{T})^{'} H_{T}^{'} (b_{T} + C_{T}^{g}_{T}^{'})$$

$$+ E_{T-1}^{'} u_{T}^{'} H_{T}^{u}_{T}^{'} - 2 E_{T-1}^{'} (b_{T} + C_{T}^{g}_{T}^{'})^{'} h_{T}^{'} + E_{T-1}^{C}_{T}^{C} .$$

To generalize the solution to T periods, consider next the 2-period problem of choosing  $\mathbf{x}_T$  and  $\mathbf{x}_{T-1}$ . Since the optimal  $\hat{\mathbf{x}}_T$  and  $\hat{\mathbf{V}}_T$  have already been obtained, we apply the principle of optimality in dynamic programming and minimize with respect to  $\mathbf{x}_{T-1}$  the expression

$$V_{T-1} = E_{T-2} (y_{T-1}^{\prime} K_{T-1} y_{T-1} - 2y_{T-1}^{\prime} K_{T-1} a_{T-1} + a_{T-1}^{\prime} K_{T-1} a_{T-1} + \hat{V}_{T})$$

$$= E_{T-2} (y_{T-1}^{\prime} H_{T-1} y_{T-1} - 2y_{T-1}^{\prime} h_{T-1} + c_{T-1})$$

where, after substitution of (1.15) for  $\hat{\vec{V}}_{\rm T}$  ,

$$c_{T-1} = E_{T-1}(b_T + C_T g_T) H_T(b_T + C_T g_T) - 2E_{T-1}(b_T + C_T g_T) h_T$$

$$+ a_{T-1}^{\prime} K_{T-1} a_{T-1} + E_{T-1} u_T^{\prime} H_T u_T + E_{T-1} c_T.$$

Since the second line of (1.16) has the same form as (1.4), we can repeat the steps in the solution for  $\mathbf{x}_T$  with T-1 replacing T , yielding an optimal  $\hat{\mathbf{x}}_{T-1}$  in the form (1.12) and the corresponding minimum 2-period loss  $\hat{\mathbf{v}}_{T-1}$  from (1.16). The process continues backward in time until  $\hat{\mathbf{x}}_1$  and  $\hat{\mathbf{v}}_1$  are obtained.

Computationally, we suggest the following steps for the T-period optimal control problem. (1) Start with initial guesses  $\tilde{x}_1$ ,  $\tilde{x}_2$ ,...,  $\tilde{x}_T$ , solve the system (1.2) with  $\varepsilon_t = 0$  for  $y_1^\circ$ ,  $y_2^\circ$ ,...,  $y_{T-1}^\circ$ , using the Gauss-Seidel method. (2) For t=T, T-1,..., 1, linearize the structural equations as in (1.6) and (1.7), noting that  $y_t^* = y_t^\circ$  has been computed in step 1. Compute the reduced form coefficients  $A_t$ ,  $C_t$  and  $b_t$  by (1.9). (3) Using (1.13) and (1.17) alternately, compute  $G_t$  and  $H_{t-1}$  for t=T, T-1,..., 1. Use (1.18) to compute  $h_{t-1}$  and (1.13) to compute  $h_t$  and the system (1.2) with  $h_t$  compute successively  $h_t$ ,  $h_$ 

Recall that by our linearization of the structure about  $y_t^*$  (rather than about  $\tilde{y}_t$  which depends on  $\varepsilon_t$ ), all the coefficients  $A_t$ ,  $C_t$  and  $b_t$  become constants, and the expectation signs in all calculations above can be dropped. We only retain the expectation  $E_{t-1}u_t^2H_tu_t = tr(H_tEu_tu_t^2)$  in the calculation

of  $c_{t-1}$  by (1.19), which, by virtue of (1.9), equals  $tr H_t (I - B_{lt})^{-1} V (I - B_{lt})^{-1}$ .

#### 2. Feedback Control with Unknown Parameters

The exposition of section 1 has paved the way for introducing randomness in the parameters  $\eta_{\bf t}$  in the system (1.2). In principle, random  $\eta_{\bf t}$  can be treated in the same way as random  $\varepsilon_{\bf t}$ . To obtain an exact solution to the last-period control problem by the method of section 1, it is necessary to linearize (1.2) about  $\tilde{\bf y}_{\bf T}$ , the solution value of  ${\bf y}_{\bf T}$  which depends on the random  $\varepsilon_{\bf t}$  and  ${\bf n}_{\bf t}$ . Accordingly, the coefficients  ${\bf B}_{1{\bf T}},\,{\bf B}_{2{\bf T}}$  and  ${\bf B}_{3{\bf T}}$  in (1.14) and  ${\bf A}_{\bf T},\,{\bf C}_{\bf T}$  and  ${\bf b}_{\bf T}$  in the resulting reduced-form are all random functions of  ${\bf n}_{\bf t}$ . The approximate method we propose to solve the multiperiod control problem with unknown parameters also follows the 5 steps described at the end of section 1, except that all the expectation signs have to be kept in the calculations.

To evaluate the expectations such as  $E_{t-1}(A_t^H t^A t)$  in (1.17), two approximations are made. First, all time subscripts of the expectation signs are replaced by zero. Thus information on the probability distribution of  $\varepsilon_t$  and  $\eta_t$  as of the beginning of the planning period is used for the calculation of the optimal  $\hat{x}_1$ ; possible future learning about the unknown parameters is ignored. Second, we linearize the structure about  $y_t^*$  which is the solution of (1.2) with  $\varepsilon_t = 0$  and  $\eta_t$  set equal to its mean  $\eta_t$ , obtaining the structural coefficients  $\overline{B}_{1t}$ ,  $\overline{B}_{2t}$  and  $\overline{B}_{3t}$ ; we then compute the i-j element of expectation  $E_0(A_t^* H_t A_t)$  by the identity

(2.1) 
$$E_0(A_t^{\prime}H_tA_t)_{ij} = (\overline{A}_t^{\prime}H_t\overline{A}_t)_{ij} + tr H_tE_0(a_{jt} - \overline{a}_{jt})(a_{it} - \overline{a}_{it})'$$

where  $\overline{A}_t = (I - \overline{B}_{lt})^{-l}\overline{B}_{2t}$ , and the covariance matrix for any two columns  $a_{jt}$  and  $a_{it}$  of  $A_t$  can be approximated by the appropriate submatrix in  $D_t Cov(\eta_t)D_t'$ ,  $D_t$  being the matrix of the partial derivatives of the columns of  $A_t$  with respect to  $\eta_t$ . Numerically, the  $k^{th}$  column of  $D_t$  is computed as the rates of change of the columns of  $A_t$  with respect to a small change in the  $k^{th}$  element of  $\eta_t$  from  $\eta_t$ . For a more thorough discussion of this method, the reader may refer to Chow (1975b).

#### 3. Usefulness of Feedback Control

If we treat the parameters  $n_{\rm t}$  as known constants and set  $\varepsilon_{\rm t}=0$ , the method of section 1 provides a solution to the optimal control of a nonlinear deterministic system. Currently, a popular way to solve such a deterministic control problem is to treat the multiperiod loss W as a function of  $x_1, \ldots, x_{\rm T}$  and minimize it by some gradient, conjugate-gradient or another standard computer algorithm, as in Fair (1974), Holbrook (1974), and Norman, Norman and Palash (1974). It may be useful to point out the possible advantages of the method of this paper as compared with this alternative approach.

1) From the very narrow viewpoint of computing the optimal policy under the assumption of a deterministic model, the method of section 1 compares favorably with the alternative method when the number of unknowns in the minimization problem is large. The number of unknowns equals the number T of planning periods times the number q of control variables. If we are dealing with 32 quarters and 4 control variables, there will be 128 variables, creating a formidable minimization problem. Our method, being based on the method of dynamic programming with a time structure, converts a problem involving T sets of control variables to T problems each involving only one set of control

variables. Its computing cost increases only linearly with T . For each period t , we solve a minimization problem involving q controls; the matrix  $C_{\mathsf{t}}^{\mathsf{H}} C_{\mathsf{t}}^{\mathsf{C}}$  to be inverted is q × q . Also, if q is increased from 4 to 8, we have to solve an 8-variable problem 32 times, whereas the alternative method has to deal with 256 variables simultaneously.

On the other hand, our method is perhaps more constrained than the alternative method by the number of simultaneous equations (the order of the matrix  $I - B_{1T}^*$  in equation 1.10) in the econometric system for our linearization requires the inversion of  $I - B_{1T}^*$ . However, by exploiting the bloc-diagonality and the sparseness of this matrix, it may be possible to deal with some 150 to 200 simultaneous equations. More computational experience is required to shed light on this question.

2) Once we leave the realm of purely deterministic control, the advantages of our approach are numerous. First, after incorporating the random disturbances  $\epsilon_t$  in an otherwise deterministic model, one can no longer regard as optimal the values of  $\mathbf{x}_2,\dots,\mathbf{x}_T$  obtained by solving the deterministic control problem. Only the value of  $\mathbf{x}_1$  for the first period constitutes an approximately optimal policy. In contrast with the alternative method of deterministic control, the method of section 1 provides the solution  $\hat{\mathbf{x}}_t$   $(t=2,\dots,T)$  as a function of the yet unobserved  $\mathbf{y}_{t-1}$ . It provides analytically an estimate  $\hat{\mathbf{v}}_1$  of the minimum expected loss associated with the optimal strategies. Using the alternative method, one would have to calculate  $\mathbf{y}_1$  from  $\hat{\mathbf{x}}_1$  and  $\epsilon_1$ , solve a multiperiod control problem from period 2 to T to obtain  $\hat{\mathbf{x}}_2$ , calculate  $\mathbf{y}_2$  from  $\hat{\mathbf{x}}_2$  and  $\epsilon_2$ , etc., and repeat the T-period simulations many times to estimate the expected loss from such a strategy. Such computations are extremely costly, if not prohibitive.

- 3) Our method yields a linearized reduced form at each period as a by-product. The reduced-form coefficients are extremely useful for computing the various dynamic multipliers of  $y_t$  with respect to current, delayed and cummulative changes of  $x_t$ , and for exhibiting how nonlinear the system is and how the various partial derivatives change through time.
- 4) The feedback control equations are useful as a basis of policy recommendations. They can be used to compare different econometric models. They can be incorporated into the econometric model to study the dynamic properties of the system under control. Once the model is linearized, its dynamic properties can be deduced by spectral and auto-covariance methods, as described in Chow (1975a, Ch. 3, 4, and 6). Not only the mean paths of the variables from periods one to T, but their variances, covariances, autocovariances and cross-covariances can be deduced.
- 5) The value of having improved information (a smaller covariance matrix) for a subset of parameters can be ascertained by comparing the minimum expected losses computed by varying the covariance matrix of  $\eta_t$  using the method of section 2. As a special case, the comparison of  $\hat{V}_1$  computed by varying the covariance matrix of  $\varepsilon_t$  using the method of section 1 helps to evaluate the importance of the stochastic disturbances in the expected welfare loss. In short, by our method, the rich theory of optimal control for linear systems can be applied to the control of nonlinear systems. Parts of this theory will be illustrated in section 4.
  - 4. A Numerical Example Using the Klein-Goldberger Model

To illustrate our method, the Klein-Goldberger model as adopted by Adelman and Adelman (1959, pp. 622-624) is used. The equations are listed below.

- (4.1) Consumer expenditures in 1939 dollars = C =  $y_1 = -22.26 + 0.55(y_6 + x_1 y_{19}) + 0.41(y_{14} y_{21} y_3) + 0.34(y_9 + x_3 y_{22}) + .26 y_{1.-1} + .072 y_{11,-1} + 0.26 z_2$
- (4.2) Gross private domestic capital formation in 1939 dollars = I =  $y_2 = -16.71 + .78(y_{14} y_{21} + y_9 + x_3 y_{22} + y_5)_{-1}$  .073  $y_{16,-1}$  + .14  $y_{12,-1}$
- (4.3) Corporate savings =  $s_p$  =  $y_3 = -3.53 + 0.72(y_4 y_{20}) .028 y_{17,-1}$
- (4.4) Corporate profits =  $P_c = Y_4 = -7.60 + 0.68 Y_{14}$
- (4.5) Capital consumption charges = D =  $y_5 = 7.25 + 0.05(y_{16} + y_{16,-1}) + 0.044(y_{13} x_1)$
- (4.6) Private employee compensation =  $W_1$  =  $y_6 = -1.40 + 0.24(y_{13} x_1) + 0.24(y_{13,-1} x_{1,-1}) + 0.29 z_6$
- (4.7) Number of wage-and-salary earners =  $N_W = y_7 = x_4 (z_4 + z_5) \div 1.062 + (26.08 + y_{13} x_1 .08 y_{16} .08 y_{16,-1} 2.05 z_6) \div (2.17 \times 1.062)$
- (4.8) Index of hourly wages = w =  $y_8 = y_{8,-1} + 4.11 0.74(z_3 y_7 z_4 z_5) + 0.52(y_{15,-1} y_{23,-1}) + .54 z_6$
- (4.9) Farm income =  $A_1$  =  $y_9 = .054(y_6 + x_1 y_{19} + y_{14} y_{21} y_3) + .012(z_1)(y_{10}) \div y_{15}$
- (4.10) Index of agricultural prices =  $p_A = y_{10} = 1.39 y_{15} + 32.0$
- (4.11) End-of-year liquid assets held by persons =  $L_1$  =  $y_{11} = 0.14(y_6 + x_1 y_{19} + y_{14} y_{21} y_3 + y_9 + x_3 y_{22}) + 76.03(1.5)^{-.84}$
- (4.12) End-of-year liquid assets held by businesses =  $L_2$  =  $y_{12}$  = .26  $y_6$  1.02(2.5) .26( $y_{15}$   $y_{15}$ ,-1) + .61  $y_{12}$ ,-1

- (4.13) Gross national product = Y + T + D =  $y_{13} = y_1 + y_2 + x_2$
- (4.14) Nonwage nonfarm income = P =  $y_{14} = y_{13} y_{18} y_5 y_6 x_1 y_9 x_3$
- (4.15) Price index of gross national product = p =  $y_{15} = 1.062 y_8 (y_7) \div (y_6 + x_1)$
- (4.16) End-of-year stock of private capital =  $K = y_{16} = y_{16,-1} + y_2 y_5$
- (4.17) End-of-year corporate surplus = B =  $y_{17} = y_{17,-1} + y_3$
- (4.18) Indirect taxes less subsidies =  $T = y_{18} = 0.0924 y_{13} 1.3607$
- (4.19) Personal and payroll taxes less transfers =  $T_W = y_{19} = 0.1549 y_6 + .131 x_1 6.9076$
- (4.20) Corporate income  $tax = T_c = y_{20} = .4497 y_4 + 2.7085$
- (4.21) Personal and corporate taxes less transfers =  $T_p = y_{21} = 0.248(y_{14} y_{20} y_3) + .2695(y_{15,-1} \div y_{15})(y_{14} y_{20} y_3) 1 + 0.4497 y_A 5.7416$
- (4.22) Taxes less transfers associated with farm income =  $T_A = y_{22} = 0.0512(y_9 + x_3)$
- (4.23)  $y_{23} = y_{15,-1}$

The control variables or instruments are

 $x_1 = W_2 = Government employee compensation$ 

 $x_2 = G$  = Government expenditures for goods and services

 $x_3 = A_2 = Government payments to farmers$ 

 $x_4 = N_G = Number of government employees.$ 

The exogenous variables not subject to control are

 $\mathbf{z}_1$  =  $\mathbf{F}_{\mathbf{A}}$  = Index of agricultural exports  $\mathbf{z}_2$  =  $\mathbf{N}_{\mathbf{p}}$  = Number of persons in the United States  $\mathbf{z}_3$  =  $\mathbf{N}$  = Number of persons in the labor force  $\mathbf{z}_4$  =  $\mathbf{N}_{\mathbf{E}}$  = Number of nonfarm entrepreneurs  $\mathbf{z}_5$  =  $\mathbf{N}_{\mathbf{F}}$  = Number of farm operators  $\mathbf{z}_6$  = time = 0 for 1929 (= 24 for 1953).

In the control experiments reported below, 1953 was chosen as the first year of the planning period. Initial values of the endogenous variables you and extrapolation formulas for the uncontrollable exogenous variables  $z_{+}$  (part of in the notation of section 1) are given by Adelman and Adelman (1959, p. 624). The four control variables have been listed in the last paragraph. When imbedded in the vector  $\mathbf{y}_{+}$  in the notation of equation (1.2), they become respectively  $y_{24}$  to  $y_{27}$  . Three runs have been tried. Run 1 uses endogenous variables 7 (number of wage-and-salary earners), 13 (real GNP), 14 (real nonwage nonfarm income) and 15 (price index of GNP) as targets, with the value 1 specified for each of the corresponding 4 diagonal elements of the matrix  $K_{+}$  in the welfare function. These target variables are steered to grow at 2, 5, 5 and 1 per cent per year respectively from their initial values at 1952. Run 2 uses variables 13, 15, 26 (government payments to farmers) and 27 (number of government employees) as target variables. The target for  $y_{26}$  is to remain at its historical 1952 value 0.1187, and for  $y_{27}$  is to grow 3 per cent annually from its estimated 1952 value 9.393. Run 3 uses variables 7, 15, 26 and 27 as target variables. In effect, runs 2 and 3 tie up two instruments and uses the remaining two instruments to control real GNP and the price index, or employment of wageand salary earners and the price index.

A major motivation behind the above experiments is to find out whether

the relationship between the general price index and real GNP (or employment) can be shifted at will by government policy according to the Klein-Goldberger model. The answer is definitely yes. The specified targets for the price index, real GNP, and/or employment of wage-and-salary earners are met exactly by the optimal control solutions of the above 3 runs, ignoring random disturbances. Thus the government can choose any price-GNP or price-employment combination at any period as it pleases by applying government employee compensation and government expenditures for goods and services as the control variables.

As pointed out by Chow (1975a, p. 167), "if the number of target variables (the number of nonzero elements in the  $p \times p$  diagonal matrix  $K_{+}$ ) equals the number  $q \leq p$  of control variables, the time path  $y_t$  generated by the deterministic system [obtained by ignoring the random disturbances in a linear econometric model] under optimal control will meet the targets exactly and the deterministic part W, of the minimum expected welfare loss will be zero, provided that Ct is of rank q." In the above three runs, the number of target variables equals the number of control variables, and the matrix  $C_{\downarrow}$  for all t in the linearized reduced form has rank 4. Thus the targets are met exactly. This illustrates the application of control theory for linear systems to nonlinear econometric systems by the approach of this paper. Note that, in the theory for controlling known linear systems, Chow (1975a, Chapters 7 and 8), it is useful to decompose the solution vector  $y_{+}$  into its deterministic part  $y_{+}$ (obtained by ignoring  $\varepsilon_t$ ) and its stochastic part  $y_t^* = y_t - y_t$  due to the random disturbances. The same decomposition can now be achieved by our method for nonlinear systems. The autocovariance matrix of  $y_{t}^{\star}$  provides the variances and covariances of the variables under control from their mean path  $\overline{y}_{t}$  . It can be derived analytically as in Chow (1975a) once the system is linearized

by the method of this paper.

To better appreciate the reason why government policy can shift the relationship between the general price index and real GNP (or employment), consider the "aggregate demand curve" and the "aggregate supply curve" implicit in the Klein-Goldberger model. The aggregate demand curve relating price to real GNP can be obtained by solving the aggregate demand sector consisting of 16 equations: (4.1)-(4.4), (4.9), (4.10), (4.13), (4.14), (4.17)-(4.22) of the IS sector and equations (4.11) and (4.12) of the LM sector. The aggregate supply curve is obtained by solving 6 equations: (4.5)-(4.8), (4.15) and (4.16). We refer to the short-run aggregate supply curve, holding all lagged dependent variables constant. (4.8) gives wage  $\,w\,$  as a linear function of employment  $\,N_{_{\hspace{-.1em}W}}^{}$  . (4.7) gives  $N_{t,j}$  as a function of real GNP, capital stock K , and government employee compensation  $W_2$  . Equations (4.16) and (4.5) explain K by capital consumption charges D (investment I being predetermined by equation 4.2) and D by K , GNP and  $W_2$  , yielding K as a function of GNP and  $W_2$  . Both w and  $^{N}_{W}$  thus become functions of GNP and  $^{W}_{2}$  . By (4.15) price p = 1.062  $^{W}N_{W}/(^{W}_{1}+^{W}_{2})$  , where the private employee compensation  $W_1$  is also a function of GNP and  $W_2$ by virtue of (4.6). Hence the resulting aggregate supply curve relating p to GNP and  $W_2$  can be shifted by manipulating the control variable  $W_2$  .

If the aggregate supply function relating price to real GNP or to employment contains no variables which are subject to government control, government policy can only shift aggregate demand and trace out the rigid relation between price and real GNP, but cannot achieve more real output or employment without inflation. A case in point is the relation between the wage rate and employment as given by (4.8). No government policy can shift this rigid relationship for the current period, given the predetermined variables. In terms of control

theory, no two instruments can steer wage and employment to specified target values as they are linearly related by (4.8). The matrix  $C_{t}$  has two linearly dependent rows and has rank smaller than the number of instruments.

We have computed the optimal control solutions for the three runs described above, and some other related runs, using T=5 and T=10 as the planning horizon. To start the iterations, we arbitrarily let the initial  $\tilde{x}_{it}$  be the 3 per cent annual growth path for each of the 4 control variables beginning from its historical value as of 1953; these initial paths are given in Table 1 for  $x_1$  and  $x_2$ . For the first period 1953, we use the values of the endogenous variables as of 1952 as starting values for the Gauss-Seidel iterations to solve for  $y_{1953}^{\circ}$ , given  $\tilde{x}_{1953}^{\circ}$ , and use  $y_{1953}^{\circ}$  as starting values to iterate for  $y_{1954}^{\circ}$ , given  $\tilde{x}_{1954}^{\circ}$ , etc. Table 1 shows the values of selected target and control variables for Run 1 at the three rounds of linearizations (three "passes" through step (1) of the method of section 1) required for the convergence of the target variables to five significant figures. Note how rapidly these variables converge to the solution, the first pass already near the optimum.

In terms of computing time using the IBM 360-91 computer at Princeton University, each pass took slightly less than 4 seconds, and the total computer time for three passes was about 12 seconds. When we ran the experiments for 10 periods instead of 5, the time merely doubled, taking about 24 seconds for three passes to convergence. These would be minimization problems involving 40 variables in the alternative approach to deterministic control. Imagine a 120-variable problem with 4 controls and 30 periods using a quarterly model of similar size. The alternative approach would be almost prohibitive, but out method would take about 3 × 24 or 72 seconds. By our method, increasing the number of control variables from 4 to 5 would not require much more computing

Table 1

Values of Selected Variables at Three Successive Passes for Control By the Klein-Goldberger Model--Run 1 (y<sub>7</sub>, y<sub>13</sub>, y<sub>14</sub>, y<sub>15</sub> as targets).

Variable	Pass	1953	1954	1955	1956	1957
x <sub>1</sub> (government employee compensation)	0 1 2 3	15.70 21.15 21.21 21.21	16.17 25.60 26.03 26.03	16.66 29.41 30.63 30.64	17.16 32.95 35.35 35.38	17.67 36.35 40.28 40.35
x <sub>2</sub> (government expenditures for goods & services)	0 1 2 3	33.50 39.96 39.95 39.95	34.50 45.42 45.40 45.40	35.54 49.68 49.74 49.74	36.61 53.59 53.85 53.85	37.70 57.60 58.11 58.11
y (real GNP)	1 2 3	180.60 180.60 180.60	189.64 189.63 189.63	199.13 199.11 199.11	209.10 209.07 209.07	219.58 219.52 219.52
Y <sub>15</sub> (price index)	1 2 3	204.32 204.42 204.42	206.47 206.47	208.55 208.53	210.66 210.62	212.82 212.72

time, since a  $5 \times 5$  C'H C matrix is still easy to invert and the hard computing work is performed in obtaining the linearized reduced form. By the alternative method, a 120-variable problem would become a 150-variable problem.

We next examine the coefficients  $G_t$  and  $g_t$  in the feedback control equations for the optimal solution of Run 1 with T=5. Of the 27 variables in  $Y_{t-1}$  (including 4 control variables), only 18 appear in the reduced form, the matrix  $A_t$  having 9 columns of zeros. Table 2 exhibits coefficients of selected lagged variables in the feedback control equations for government expenditures  $x_2$ . Note that the coefficients of the lagged expenditure, income and price variables are all negative, showing that government expenditures

Coefficients of Selected Lagged Variables in the Feedback Control
Equations for Government Expenditures--Run 1 (T = 5)

Table 2

		Lagged Variable							
Period	1	3	5	8	9	12	14	15_	<u>g</u>
1	260	109	768	053	768	138	659	015	124.4
3	260	109	<b></b> 768	054	768	138	659	014	137.0
5	260	109	<b></b> 768	<del>-</del> .055	768	138	<b></b> 659	014	151.0

should respond negatively to recent signs of economic expansion. The feedback coefficients are practically identical for periods 1 through 5 for two reasons. First, since the number of instruments equals the number of target variables ( $C_t$  having full rank), the matrice  $K_t(A_t + C_tG_t) = 0$  and  $H_t = K_t$ , as shown in Chow (1975a, pp. 168-9). This means that the matrix  $H_t$  in the quadratic loss function  $V_t$  to be minimized in each future period is identical. Second, since the linearized reduced form coefficients  $A_t$  and  $C_t$  vary only slightly through time, the solution  $G_t = (C_tH_tC_t)^{-1}C_tH_tA_t$  will also be stable through time. The intercept  $g_t$ , however, is increasing in order to meet the growing targets as we have specified.

It may be interesting to exhibit parts of the matrices  $A_t$ ,  $C_t$  and  $b_t$  for t=1, 3, 5 to show how time-varying they are. Table 3 shows selected coefficients of the reduced form equation for consumption expenditures  $y_1$  from the optimal control solution of run 1. Their stability through time is apparent. The last row of Table 3 reproduces the corresponding coefficients from the study by A. S. Goldberger (1959, pp. 40-41) on impact multipliers of the Klein-Goldberger model, although for numerous reasons, including the differences between the two

versions of the Klein-Goldberger model, the coefficients given by Goldberger should be different from ours.

Table 3

Reduced Form Coefficients for Consumption from the Optimal Solution-Run 1

Period	a <sub>ll</sub>	a 13	<sup>a</sup> 15	<sup>a</sup> 16	c <sub>11</sub>	c <sub>12</sub>	b <sub>1</sub>
1 3 5	.3305 .3311 .3315	.1425 .1428 .1429	.2036 .2053 .2064	0 0 0	.3005 .2997 .3005	.2712 .2736 .2750	33.84 35.58 37.42
Goldberger	.3219	.0297	.2834	.1027	.3355	.2380	

### 5. Concluding Remarks

If we were to pursue a dynamic policy analysis using the Klein-Goldberger model or any other nonlinear econometric model by the method of this paper, it would occupy a substantial volume. Once the model is linearized and the approximately optimal linear feedback control equations obtained, the methods of dynamic analysis as described in Goldberger (1959), Adelman and Adelman (1959), and Chow (1975a) can be applied to study numerous important and interesting questions of macroeconomic theory and policy. The main purpose of this paper has been to show that, using our method of feedback control, the theory and techniques for controlling linear econometric systems can be made applicable to nonlinear econometric systems.

This paper has been written as an invited paper for presentation before
the Third Econometric Society World Congress to be held in Toronto in August
1975 to survey the subject of stochastic control in economics. One would expect

in a survey discussions on such topics as the methods of feedback control versus open-loop control, control of linear versus nonlinear systems, control of deterministic versus stochastic systems, problem of parameter uncertainty, various computation methods, and important areas of applications. I have not written such a survey partly because a comparison of methods and a discussion of applications can be found respectively in Chapters 12 and 9 of Chow (1975a). The presentation of this paper has been biased towards the feedback approach, because it appears to be much more useful than the computation of optimal time paths for the deterministic version of a stochastic control problem and helps to tie together a significant part of stochastic control theory in economics.

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